

## **Stormwater Management Report**

Windsor Solar Project



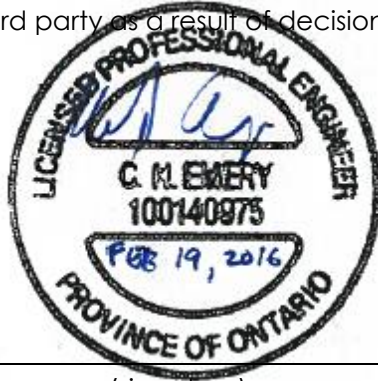
Prepared for:  
Windsor Solar LP

Prepared by:  
Stantec Consulting Ltd.  
171 Queens Avenue  
London, ON N6A 5J7  
Tel: 519-645-2007  
Fax: 519-645-6575

February 19, 2016

# Sign-off Sheet

This document entitled Stormwater Management Report was prepared by Stantec Consulting Ltd. ("Stantec") for the account of Windsor Solar LP (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.



Prepared by \_\_\_\_\_  
(signature)

**Nick Emery, P.Eng.**

Reviewed by \_\_\_\_\_  
(signature)

**Andy Sobchak, P.Eng.**

## Table of Contents

<b>1.0</b>	<b>INTRODUCTION .....</b>	<b>1.1</b>
1.1	BACKGROUND INFORMATION .....	1.1
<b>2.0</b>	<b>EXISTING CONDITIONS DRAINAGE .....</b>	<b>2.1</b>
2.1	TOPOGRAPHY .....	2.1
2.2	SOILS .....	2.1
2.3	SITE VISIT .....	2.1
2.4	WATER BODIES .....	2.1
<b>3.0</b>	<b>PROPOSED DEVELOPMENT.....</b>	<b>3.1</b>
<b>4.0</b>	<b>IMPACT ASSESSMENTS .....</b>	<b>4.1</b>
4.1	RUNOFF QUANTITY (PEAK FLOW) .....	4.1
4.2	RUNOFF QUALITY .....	4.2
<b>5.0</b>	<b>CONCLUSIONS &amp; RECOMMENDATIONS .....</b>	<b>5.1</b>

### LIST OF TABLES

Table 1	Calculated Peak Discharge Summary .....	4.2
---------	---	-----

### LIST OF FIGURES

FIGURE 1	SITE LOCATION PLAN
FIGURE 2	EXISTING CONDITIONS DRAINAGE PLAN
FIGURE 3	PROPOSED CONDITIONS DRAINAGE PLAN

### LIST OF APPENDICES

APPENDIX A	SITE PHOTOGRAPHS
APPENDIX B	ENGINEERING DRAWINGS
APPENDIX C	CULVERTS
APPENDIX D	RUNOFF QUANTITY (PEAK FLOWS)
APPENDIX E	RUNOFF QUALITY

# STORMWATER MANAGEMENT REPORT

Introduction  
February 19, 2016

## 1.0 INTRODUCTION

The Windsor Solar Project is a proposed 50 MW renewable energy project located on the Windsor International Airport property in the City of Windsor, Ontario. A stormwater management report was previously prepared by Dillon Consulting for the proposed project as part of the Renewable Energy Approval process. As part of the detailed design for the proposed facility, Stantec Consulting Ltd. has been retained to verify the conclusions of the Dillon report, prepare a proposed stormwater management strategy, and assess the potential impacts of this proposed development on local surface water. Our approach and the technical analyses undertaken to date are detailed in the following pages of this report.

### 1.1 BACKGROUND INFORMATION

The site stormwater management strategy was prepared based on the following background information:

- *Windsor Solar Project Geotechnical Engineering Report*, prepared by LVM, August 13, 2014;
- *Topographic Survey*, prepared by Verhaegen, Stubberfield, Hartley, Brewer, Bezaire Inc., May 20, 2015;
- *Topographic Survey*, prepared by Surveyors On Site Inc., December 2015;
- *Windsor Solar Project Preliminary Stormwater Management Report*, prepared by Dillon Consulting, February 2015; and
- *Proposed site plan*, prepared by PCL, January 2016.



## STORMWATER MANAGEMENT REPORT

Existing conditions drainage  
February 19, 2016

## 2.0 EXISTING CONDITIONS DRAINAGE

The subject site is located within the Windsor International Airport lands, and has historically been farmed for row crops. The existing site location is shown on Figure 1.

### 2.1 TOPOGRAPHY

Based on the results of the site topographic survey and available aerial photography, the existing site slopes very gently from west to east. The site slopes are nearly flat, with an average measured slope of approximately 0.2%. The slopes are interrupted by existing agricultural ditches and roadside ditches that intercept surface runoff and convey it to the Lappan Drain and the McGill Drain.

### 2.2 SOILS

Based on the information presented in the site geotechnical report, the site soils are comprised of a topsoil surface layer, measuring from 150 mm to 380 mm thick, overlying weathered silty clay till. Particle size distribution analysis results for the silty clay tills suggest these soils contain approximately 3% gravel, 26% – 29% sand, 35% - 38% silt, and 33% clay (LVM, 2014).

### 2.3 SITE VISIT

A site visit was completed on December 23, 2015 to identify the existing surface and drainage conditions prior to construction. A brief rainfall occurred immediately prior to the visit. Photographs presented in Appendix A reflect these conditions.

### 2.4 WATER BODIES

Runoff from most of the site is collected and conveyed by Municipal Drains - the Lappan Drain and the McGill Drain. As shown in the site visit photographs (Appendix A), both channels are heavily vegetated and standing water was observed in both during the December 23, 2015 site visit.

## STORMWATER MANAGEMENT REPORT

Proposed Development  
February 19, 2016

### 3.0 PROPOSED DEVELOPMENT

The Windsor Solar Project employs a low-impact approach to site development. The grading and civil engineering plans included in Appendix B show that the proposed grades will match existing grades wherever possible; existing drainage patterns are preserved wherever possible; roads will typically be constructed at grade to maintain existing drainage patterns; and site excavation will only occur to allow construction of the access road network and drainage features such as grassed swales.

Additionally, the proposed solar panel racking will be installed using helical piles, which means the invasive practices of coring, topsoil stripping and large-scale earthworks typically employed with rack and panel installation will not be required. Once the panels and racking are in place, all accessible areas will be scarified/aerated to alleviate soil compaction, and vegetation across the site will be promoted through drill seeding. The post-development hydrology will be significantly improved as the property transitions from active agricultural use with extended periods of bare soil to a permanent grassed meadow.

Runoff from the proposed development is conveyed to the Lappan Drain and McGill Drain by shallow grassed swales. The proposed swales are generally located on the upstream sides of the proposed access roads. Proposed access road culverts are designed to convey the design 5-year peak discharge. Entrance culverts are designed to convey the design 10-year peak discharge. The corresponding culvert design information is summarized in Appendix C.

## STORMWATER MANAGEMENT REPORT

Impact Assessments  
February 19, 2016

### 4.0 IMPACT ASSESSMENTS

As demonstrated from the analysis results described below, the land use change from agriculture to meadow is expected to 1) improve the site's infiltration regime, 2) reduce runoff peak flow, and 3) mitigate the risk of erosion and sediment migration off the site.

#### 4.1 RUNOFF QUANTITY (PEAK FLOW)

Hydrologic models were developed to calculate the peak runoff rates from the site under both existing and proposed conditions. The existing conditions drainage plan is shown on Figure 2 and the corresponding catchment areas were delineated based on available topographic mapping, aerial photography, site survey data, and site visit observations. The proposed conditions drainage plan is shown on Figure 3 and the corresponding catchment areas were delineated based on the proposed Windsor Solar Project grading plan.

The hydrologic models include the entire Lappan and McGill Drain catchment area upstream of the eastern Windsor Solar Project site boundary. Based on the site survey results, a secondary drainage outlet was also identified: A perched 600 mm diameter CSP culvert located approximately 400 m north of the 1600-mm-diameter CSP McGill Drain culvert at the eastern site boundary conveys stormwater from a small portion of the site to the neighboring agricultural land during severe storm events.

The Windsor Solar Project proposal increases site impervious coverage to approximately 5.65 ha, or 2.3% of the total site area, mainly in the form of roadways and substation platforms. As noted in *Hydrologic Response of Solar Farms* (Cook and McCuen; Journal of Hydrologic Engineering, May 2013), included in Appendix D for reference, solar panels suspended on racking above vegetated cover do not functionally contribute to site imperviousness and do not have "a significant effect on the runoff volumes, peaks or times to peak" of solar farm development sites.

Normally, increasing impervious coverage generates a corresponding increase in runoff peak flows. However, as the analysis in Appendix D details, existing bare soil/agricultural land use is being converted to grassed/vegetated land use under proposed conditions, which hydrologically improves the site and reduces expected peak runoff from existing pervious areas.

Comparing the existing and proposed condition hydrologic model results shows the impact of pervious cover change outweighs the impact of increasing the total impervious cover. The peak discharges at the two existing site outlets for the modelled design events are summarized in the following table. The results show that the post-development peak flows at the 1600 mm CSP culvert are less than the existing condition peak flows for all of the modelled design events. While the post-development peak flows are slightly higher than existing conditions at the 600 m diameter CSP culvert for three of the modelled design events, the calculated increase is negligible and unlikely to result in downstream negative impacts. Thus, formal quantity control measures for stormwater are not required.



## STORMWATER MANAGEMENT REPORT

Impact Assessments  
February 19, 2016

**Table 1 Calculated Peak Discharge Summary**

Design Event	Peak Discharge at Existing 600 mm Diameter Culvert (cms)		Peak Discharge at Existing 1600 mm Diameter McGill Drain Culvert (cms)	
	Existing Condition	Proposed Condition	Existing Condition	Proposed Condition
2-year	0.03	0.04	3.36	3.10
5-year	0.06	0.07	4.84	4.49
10-year	0.09	0.09	5.76	5.36
25-year	0.12	0.13	6.81	6.60
50-year	0.14	0.14	7.60	7.52
100-year	0.15	0.15	8.34	8.29

## 4.2 RUNOFF QUALITY

An added benefit of the Windsor Solar Project low-impact approach to site development is overland sheet flow drainage is largely maintained: concentration and channelization of runoff along roadsides is minimized and long, shallow-sloped flow paths over grass are promoted. This added contact with vegetation is expected to improve runoff quality draining from the site. As noted in *Control of Erosion – Fact Sheet* (Ontario Ministry of Agriculture and Food, October 1986) located in Appendix E, Moore, Fish and Arnold report, "Compared to continuous corn, hay or pasture crops reduce soil loss by about 90%." Table 3 of the fact sheet indicates hay-pasture and permanent pasture can provide an 87% and a 93% respective reduction in soil loss compared to corn and bean cultivation. Since the Windsor Solar Project site has been actively cultivated, implementation of the proposed drill seeding and vegetation program is expected to significantly improve its hydrologic characteristics, reduce erosion potential and achieve *Enhanced* water quality control.

Thus, formal quality control measures for stormwater are not required.

## STORMWATER MANAGEMENT REPORT

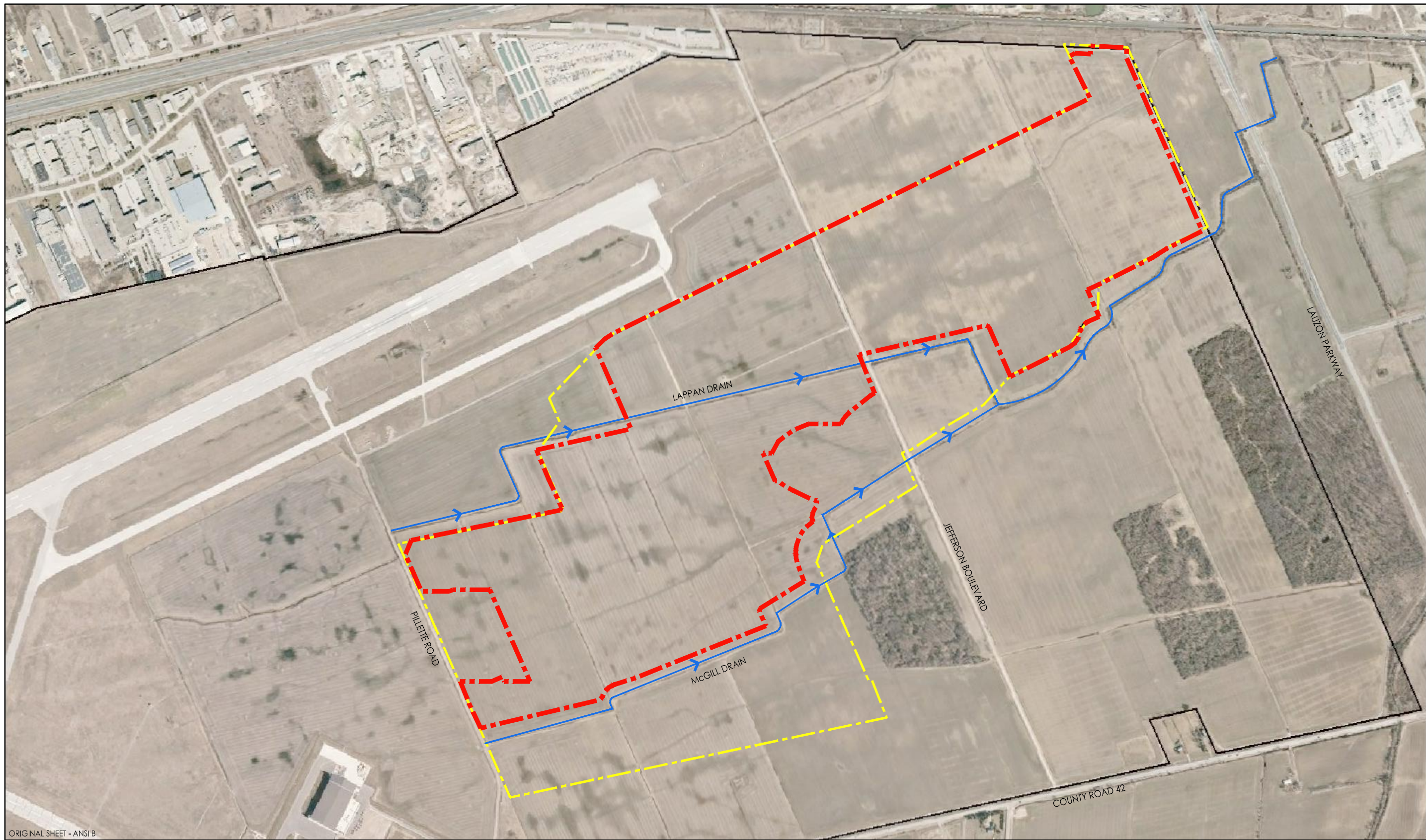
Conclusions & Recommendations  
February 19, 2016

### 5.0 CONCLUSIONS & RECOMMENDATIONS

The Windsor Solar Project development plan is simple and low-impact. Large-scale earthworks are not being proposed and localized post-development grading will generally match the existing topography. Fundamentally, the plan proposes to change land use of the property from active agriculture to grassed meadow. The analyses contained within this report demonstrate this land use change improves local hydrology and there are no anticipated negative impacts on the Lappan Drain or McGill Drain.

# FIGURES





ORIGINAL SHEET - ANSI B

February 2016  
133560106



600-171 Queens Avenue  
London ON N6A 5J7  
Tel. 519-645-2007  
www.stantec.com

Legend

- - - - - SITE BOUNDARY
- - - - - REA APPROVAL LIMIT

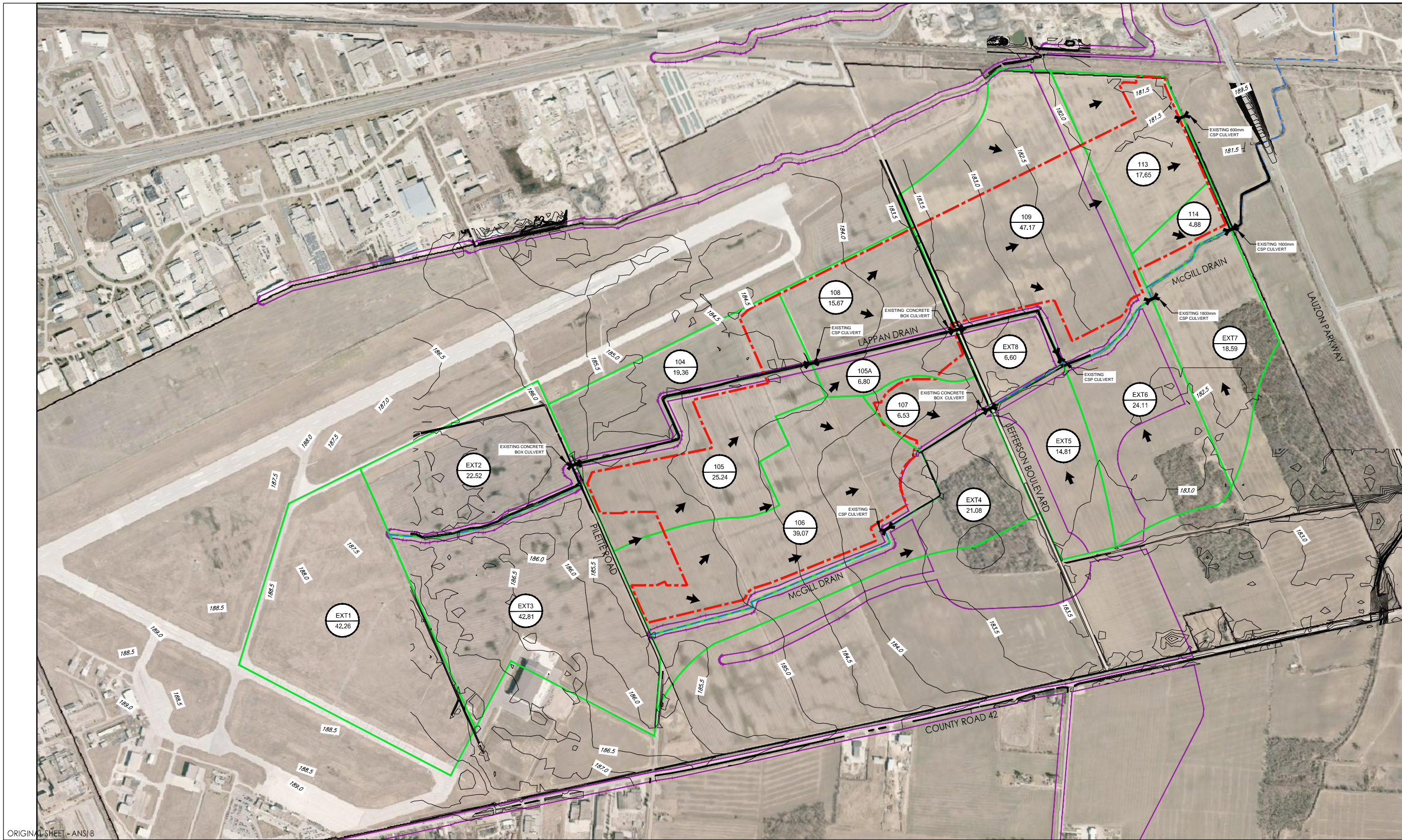


Client/Project  
WINDSOR SOLAR LP  
WINDSOR SOLAR ENERGY PROJECT

Figure No.  
1

Title  
SITE LOCATION





ORIGINAL SHEET - ANSI 8

February 2016  
133560106



600-171 Queens Avenue  
London ON N6A 5J7  
Tel. 519-645-2007  
www.stantec.com

Legend

- - - SITE BOUNDARY
- STORM DRAINAGE AREA
- ERCA REGULATION LIMITS

OVERLAND FLOW DIRECTION

- CATCHMENT ID
- CATCHMENT AREA (ha)

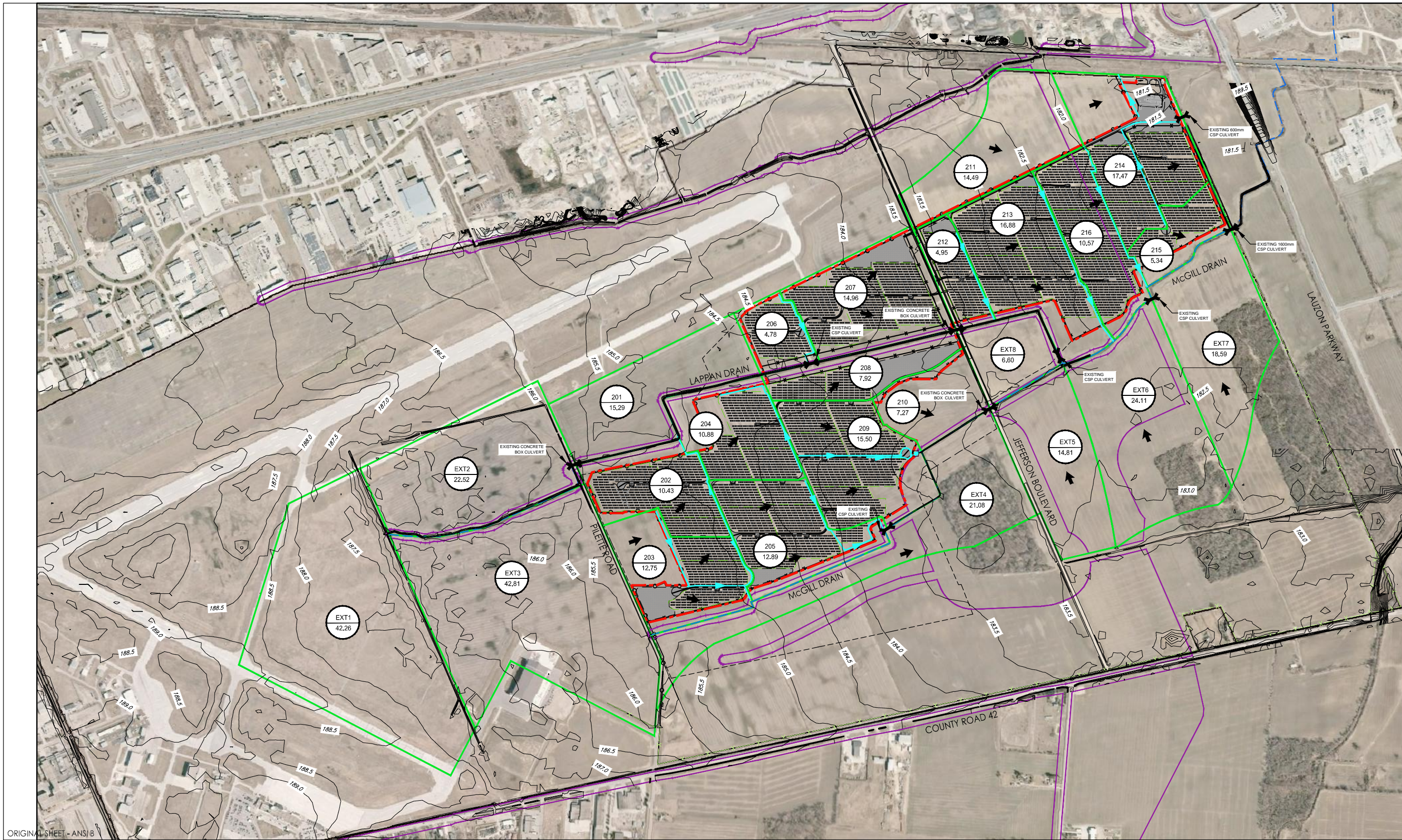


Client/Project  
WINDSOR SOLAR LP  
WINDSOR SOLAR ENERGY PROJECT

Figure No.  
2

Title  
**EXISTING CONDITIONS  
DRAINAGE PLAN**





ORIGINAL SHEET - ANSI 8

February 2016  
133560106

K:\01614\active\133560106\design\drawing\civil\sheet\_files\SWM\133560106\_Figure\_3.dwg  
2/9/2016 11:03 AM by:kenwell, Cynthia



600-171 Queens Avenue  
London ON N6A 5J7  
Tel. 519-645-2007  
www.stantec.com

Legend

- - - - - SITE BOUNDARY
- STORM DRAINAGE AREA
- ERCA REGULATION LIMITS
- ▶ PROPOSED GRASSED SWALE
- ▶ OVERLAND FLOW DIRECTION
- 205  
4.76 CATCHMENT ID  
CATCHMENT AREA (ha)



Client/Project  
WINDSOR SOLAR LP  
WINDSOR SOLAR ENERGY PROJECT

Figure No.  
**3**

Title  
**PROPOSED CONDITIONS  
DRAINAGE PLAN**



# **APPENDIX A SITE PHOTOGRAPHS**

**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 1 – McGill Drain at Pilette Road, Looking East**



**Photo 2 – Lappan Drain, Looking West to Pilette Road**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 3 – Lappan Drain, Looking East**



**Photo 4 – Looking South from Lappan Drain**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 5 – Drainage Swale to Lappan Drain, Looking South**



**Photo 6 – Typical Ditch, Looking South**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 7 – Lappan Drain, Looking West**



**Photo 8 – Looking Northeast from Lappan Drain**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 9 – Ditch South of Runway, Looking South**



**Photo 10 – Roadside Ditch South of Runway, Looking West**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 11 – Roadside Ditch South of Runway Looking East**



**Photo 12 – Jefferson Boulevard Roadside Ditch, Looking South**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



**Photo 13 – Lappan Drain, Looking North from McGill Drain**



**Photo 14 – Roadside Ditch at Eastern Site Boundary, Looking North**



**STORMWATER MANAGEMENT REPORT  
APPENDIX A – SITE PHOTOGRAPHS**



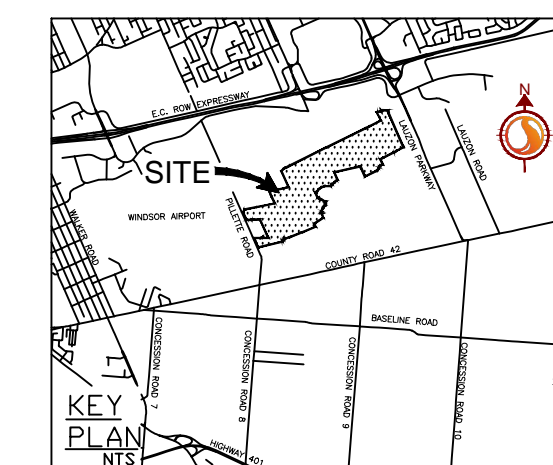
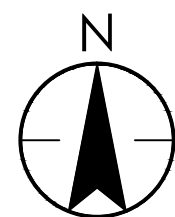
**Photo 15 – Sediment Deposition in Culvert Near East Site Limit**



**Photo 16 – Looking West from Jefferson Boulevard**

# **APPENDIX B ENGINEERING DRAWINGS**





The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

### Notes

1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS RECEIVED ON JANUARY 20, 2016. TOPOGRAPHIC SURVEY IS UTM 17 NAD83 CSRS, IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RTK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PC'S OFFICE AT 5255 COUNTY RD. 42.
2. LEGAL PLAN OF SURVEY BY VERNEKEN STUNNEFELD HARTLEY BROKER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016.
3. SETBACK INFORMATION PROVIDED BY DILLON CONSULTING LIMITED, AUGUST 2014.
4. THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
5. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
6. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
7. IF, FOR UNFORESEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENDOCHASE AND PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
8. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
9. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED EVERYWHERE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
10. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
11. CULVERTS ARE TO BE INSTALLED AS PER OPSD 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
12. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
13. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPSD 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPSD 577.
14. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPSD 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPSD 1011.
15. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPSD 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPSD 805.010.
16. RRPA SHALL BE IN ACCORDANCE WITH OPSD 810.010 SECTION B-B.
17. STOCKPILES TO BE LOCATED IN LATDOWN AREAS.

### Legend

PROPOSED	EXISTING
PROPERTY LINE	—————
PROJECT LOCATION BOUNDARY	—————
FENCE	—————
EX. CONTOUR	—————



B. ISSUED FOR TENDER	JBM	DS	16.02.17
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29
Revision	By	Appd.	YY.MM.DD
File Name: 133560106_CS-010SP.dwg	JBM	DS	JBM 14.01.28
	Dwn.	Chkd.	Dign.

Permit-Seal

PRELIMINARY  
NOT FOR CONSTRUCTION

Client/Project  
WINDSOR SOLAR LP

WINDSOR SOLAR ENERGY PROJECT  
50MW SOLAR FARM  
Windsor, ON

Title  
OVERALL SITE PLAN

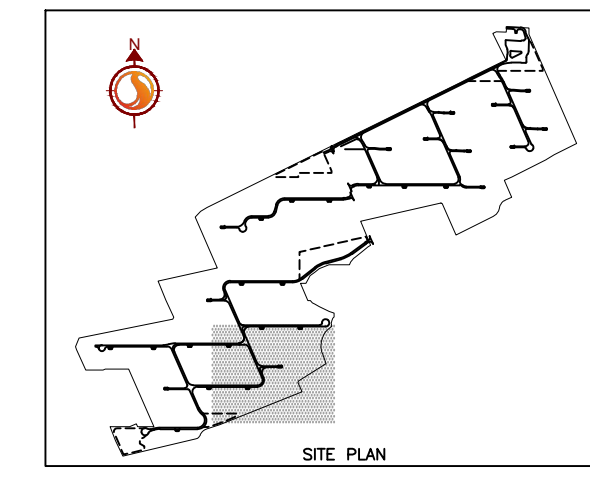
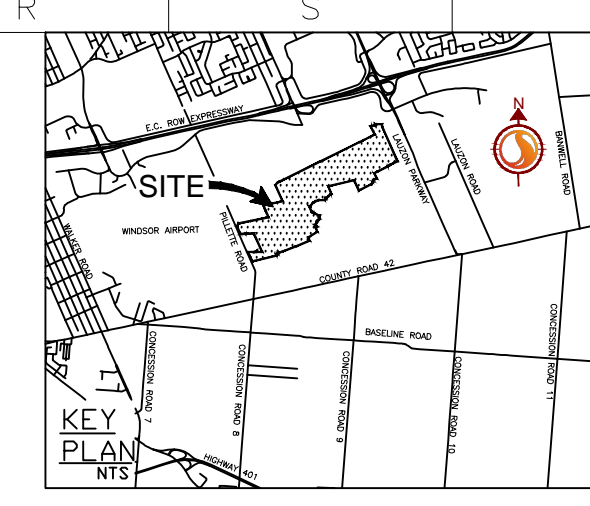
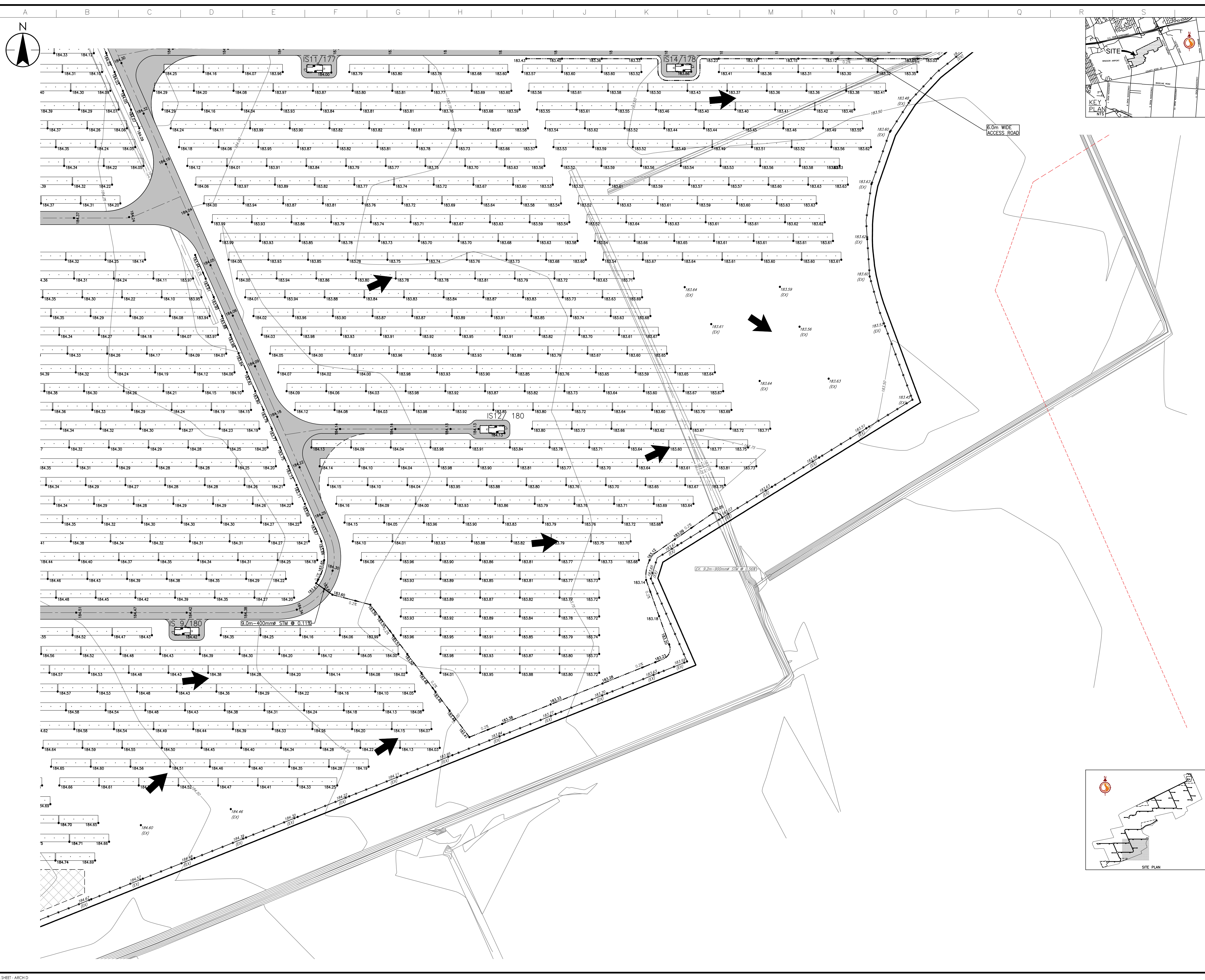
Project No. 133560106	Scale 1:4000	Sheet 	Revision B
--------------------------	-----------------	-----------	---------------

Drawing No. C-010









Copyright Reserved  
 The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
 The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

- Notes
1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS RECEIVED ON JANUARY 20, 2016. TOPOGRAPHICAL SURVEY IS WITH 17 NAD83 CGRS IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RPK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PCRS OFFICE AT 5255 COUNTY RD. 42.
  2. LEGAL PLAN OF SURVEY BY FERNANDEZ STUNNBERG HARTLEY BROKER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016. GEOTECHNICAL INFORMATION PROVIDED BY DELLORE CONSULTING LIMITED, AUGUST 2014.
  3. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
  4. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS; OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING STRUCTURES BEFORE PROCEEDING WITH ANY WORK.
  5. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
  6. IF, FOR UNFORESEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENDOCRASH AND/OR PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
  7. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
  8. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED EVERYWHERE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
  9. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
  10. CULVERTS ARE TO BE INSTALLED AS PER OPS 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
  11. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
  12. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPS 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPS 577.
  13. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPS 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPS 1019.
  14. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPS 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPS 805.010.
  15. RRPAF SHALL BE IN ACCORDANCE WITH OPS 810.010 SECTION B-B.
  16. STOCKPILES TO BE LOCATED IN LAYDOWN AREAS.

Legend		EXISTING	
● 187.00	ELEVATION	● 185.19 (EX)	ELEVATION
---	DITCH	---	CONTOUR (0.25m INTERVALS)
---	PROPERTY LINE	---	PROJECT LOCATION BOUNDARY
---	FENCE	---	OVERLAND FLOW DIRECTION

Revision	By	Appd.	YY.MM.DD
B. ISSUED FOR TENDER	JBM	DS	16.02.17
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29

File Name: 133560106\_C-400CP.dwg  
 Dwn. Chkd. Dign. YY.MM.DD

Permit-Seal

PRELIMINARY  
NOT FOR CONSTRUCTION

Client/Project  
**WINDSOR SOLAR LP**

**WINDSOR SOLAR ENERGY PROJECT**  
 50MW SOLAR FARM  
 Windsor, ON

Title  
**GRADING PLAN**

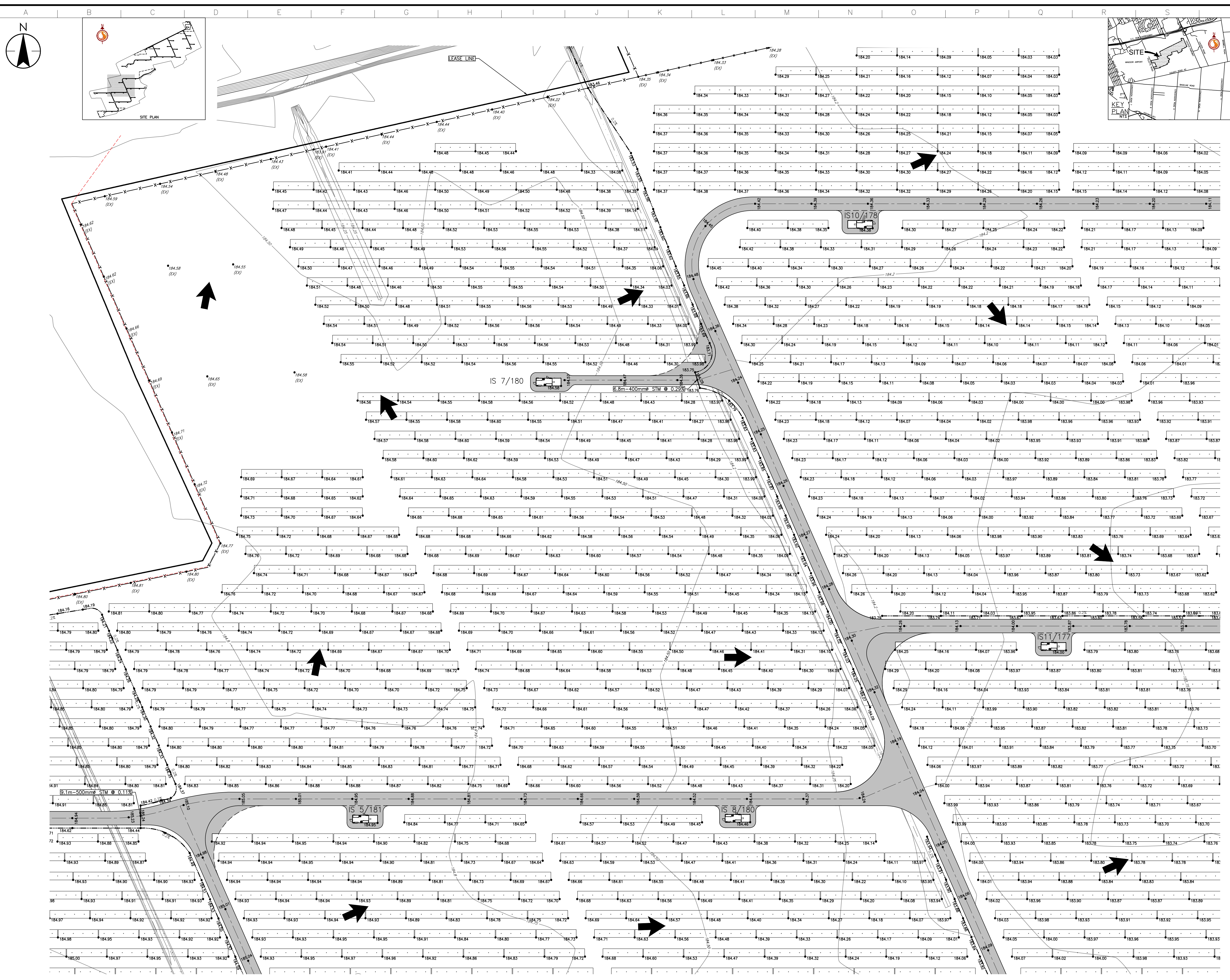
Project No. 133560106	Scale 1:750	Sheet C-401	Revision B
--------------------------	----------------	----------------	---------------

V:\016\A\active\133560106\design\drawing\civil\sheet\133560106\_C-400CP.dwg  
 2016/02/19 3:01 PM By: Miller, Jonathan









A B C D E F G H I J K L M N O P Q R S  
 1  
 2  
 3  
 4  
 5  
 6  
 7  
 8  
 9  
 10  
 11  
 12  
 13  
 14  
 15

49 Frederick Street  
 Kitchener, ON, N2H 6M7  
 Tel. 519.579.4410  
 www.stantec.com

**CONSTRUCTION LEADERS**

Copyright Reserved  
 The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
 The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

- Notes
1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS RECEIVED ON JANUARY 20, 2016. TOPOGRAPHICAL SURVEY IS WITH 17 NAD83 GBS, IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RISK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PC'S OFFICE AT 5255 COUNTY RD. 42.
  2. LEGAL PLAN OF SURVEY BY WILHELM STUMPFER HARLEY BREWER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016. GEOTECHNICAL INFORMATION PROVIDED BY DELLORE CONSULTING LIMITED, AUGUST 2014.
  3. THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
  4. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
  5. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
  6. IF, FOR UNFORESEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENDORSE OWN PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC. PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
  7. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
  8. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED OTHERWISE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
  9. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
  10. CULVERTS ARE TO BE INSTALLED AS PER OPS 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
  11. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
  12. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPS 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPS 577.
  13. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPS 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPS 1019.
  14. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPS 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPS 802.010.
  15. RIPRAP SHALL BE IN ACCORDANCE WITH OPS 810.010 SECTION B-B.
  16. STOCKPILES TO BE LOCATED IN LAYDOWN AREAS.

Legend

PROPOSED

- 187.00 ELEVATION
- DITCH
- CONTOUR (0.25m INTERVALS)
- PROPERTY LINE
- PROJECT LOCATION BOUNDARY
- FENCE
- OVERLAND FLOW DIRECTION

EXISTING

- 185.19 (EX) ELEVATION
- 184.5 CONTOUR (0.25m INTERVALS)

B. ISSUED FOR TENDER	JBM	DS	16.02.17
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29
Revision	By	Appd.	YY.MM.DD
File Name:	133560106_C-400CP.dwg		
	Dwn.	Chkd.	Dign.
			YY.MM.DD

Permit-Seal

PRELIMINARY  
NOT FOR CONSTRUCTION

Client/Project  
**WINDSOR SOLAR LP**

**WINDSOR SOLAR ENERGY PROJECT**  
 50MW SOLAR FARM  
 Windsor, ON

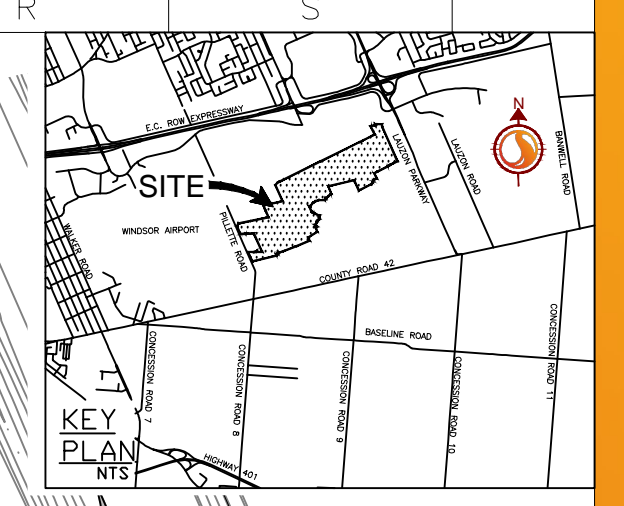
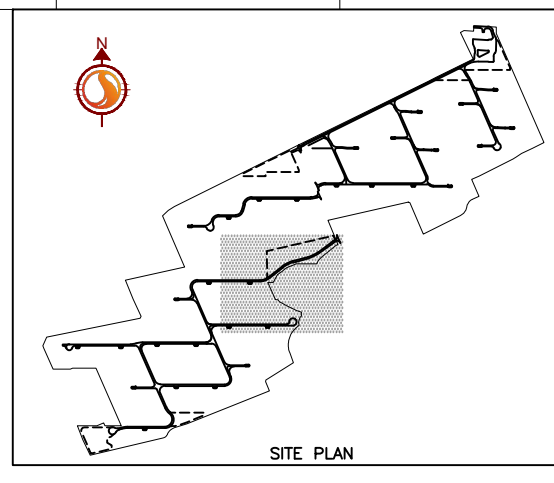
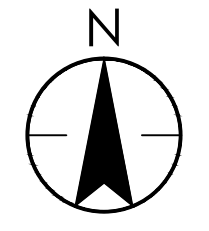
Title  
**GRADING PLAN**

Project No. 133560106  
 Scale 0 7.5 22.5 37.5m  
 1:750

Drawing No. Sheet  
 Revision

V:\016\A\active\133560106\design\drawing\civil\sheet\133560106\_C-400CP.dwg  
 2016/02/19 3:02 PM By: Miller, Jonathan





Copyright Reserved  
 CONSTRUCTION LEADERS  
 The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
 The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

- Notes
1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS RECEIVED ON JANUARY 20, 2016. TOPOGRAPHICAL SURVEY IS LTM 17 N4833 GRS, IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RPK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PC'S OFFICE AT 5255 COUNTY RD. 42.
  2. LEGAL PLAN OF SURVEY BY VERNEEN STUNTERFIELD HARLEY BROWER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016.
  3. GEOTECHNICAL INFORMATION PROVIDED BY DILLON CONSULTING LIMITED, AUGUST 2014.
  4. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
  5. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
  6. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
  7. IF, FOR UNFORSEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENCLOSED AND PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC. PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
  8. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
  9. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED EVERYWHERE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
  10. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
  11. CULVERTS ARE TO BE INSTALLED AS PER OPSD 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
  12. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
  13. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPSD 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPSD 577.
  14. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPSD 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPSD 1010.
  15. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPSD 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPSD 805.010.
  16. RRPA SHALL BE IN ACCORDANCE WITH OPSD 810.010 SECTION B-B.
  17. STOCKPILES TO BE LOCATED IN LAYDOWN AREAS.

Legend

	PROPOSED		EXISTING
187.00	ELEVATION	185.19	(EX)
	DITCH		184.5
	CONTOUR		PROPERTY LINE
	PROJECT LOCATION BOUNDARY		FENCE
	OVERLAND FLOW DIRECTION		

B. ISSUED FOR TENDER	JBM	DS	16.02.17
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29
Revision	By	Appd.	YY.MM.DD
File Name:	133560106_C-400CP.dwg		14.01.06
	Dwn.	Chkd.	Dign.
			YY.MM.DD

Permit-Seal

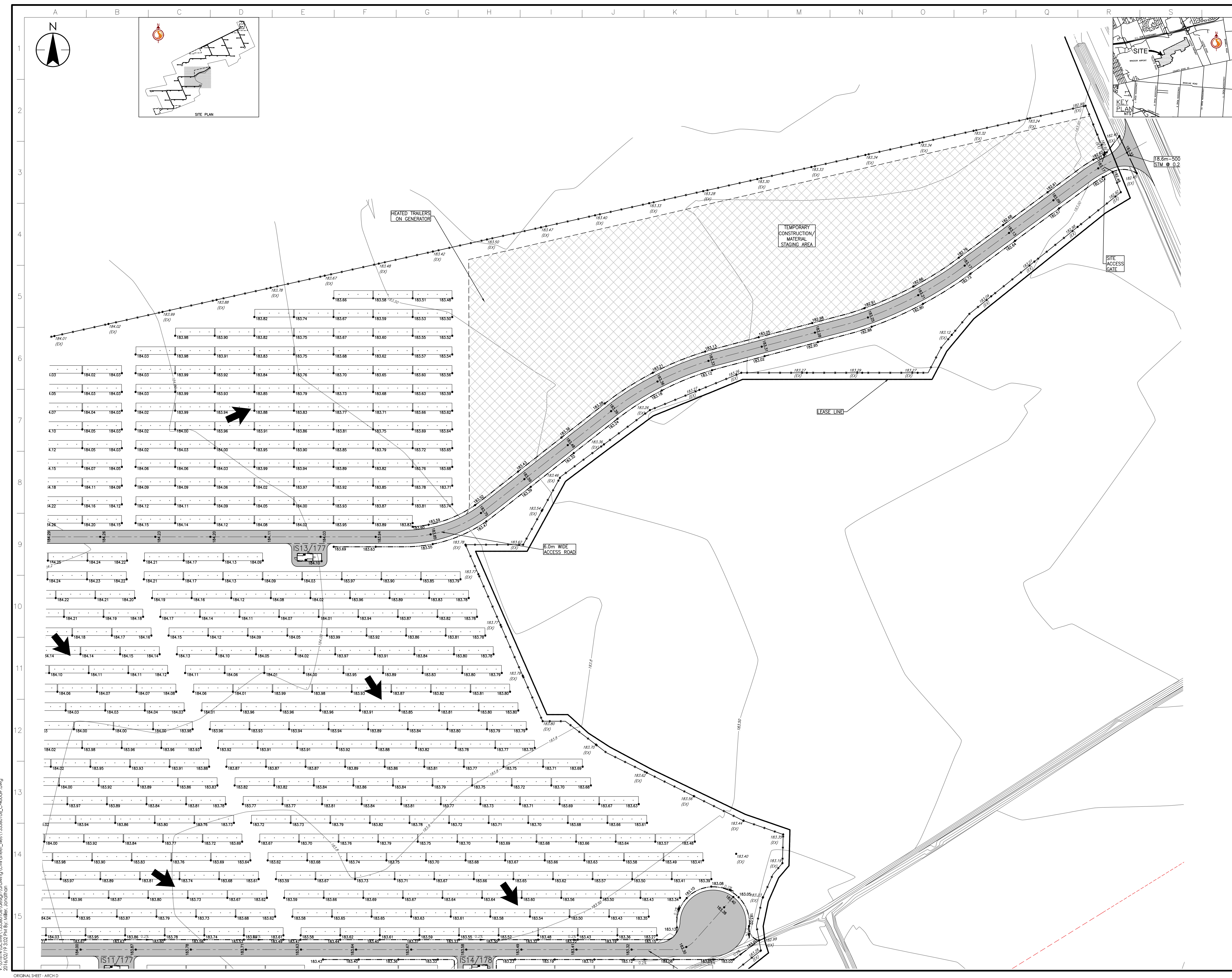
PRELIMINARY  
NOT FOR CONSTRUCTION

Client/Project  
**WINDSOR SOLAR LP**

**WINDSOR SOLAR ENERGY PROJECT**  
 50MW SOLAR FARM  
 Windsor, ON

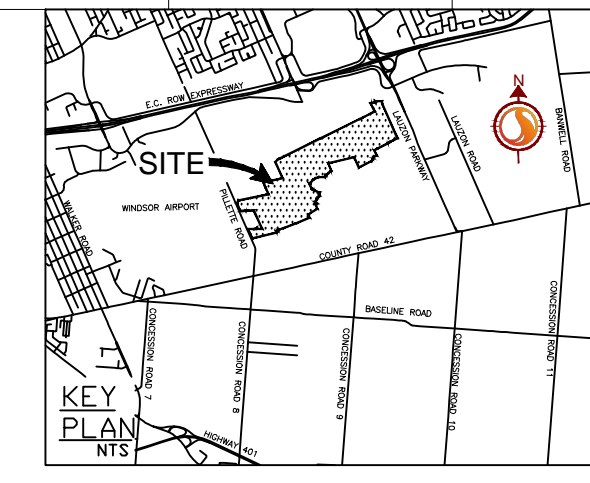
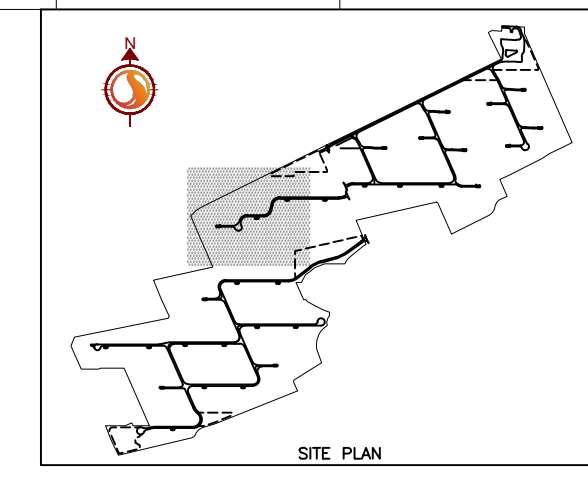
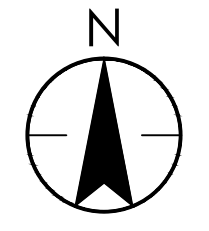
Title  
**GRADING PLAN**

Project No.	Scale	0	7.5	22.5	37.5m
133560106	1:750				
Drawing No.	Sheet			Revision	
C-404					



V:\016\A\active\133560106\design\drawing\civil\sheet\133560106\_C-400CP.dwg  
 2016/02/19 3:02 PM By: Miller, Jonathan





Copyright Reserved  
 The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
 The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

- Notes**
1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS RECEIVED ON JANUARY 20, 2016. TOPOGRAPHICAL SURVEY IS LTM 17 N483.58S IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RPK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PC'S OFFICE AT 5255 COUNTY RD. 42.
  2. LEGAL PLAN OF SURVEY BY VERNEGER STUNNBERG HARLEY BROKER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016. GEOTECHNICAL INFORMATION PROVIDED BY DELLOE CONSULTING LIMITED, AUGUST 2014.
  3. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
  4. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
  5. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
  6. IF, FOR UNFORSEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENDORSE AND/OR PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
  7. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
  8. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED EVERYWHERE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
  9. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
  10. CULVERTS ARE TO BE INSTALLED AS PER OPSD 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
  11. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
  12. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPSD 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPSD 577.
  13. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPSD 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPSD 1011.
  14. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPSD 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPSD 805.010.
  15. RIPRAP SHALL BE IN ACCORDANCE WITH OPSD 810.010 SECTION B-B.
  16. STOCKPILES TO BE LOCATED IN LATDOWM AREAS.

**Legend**

PROPOSED	EXISTING
● 187.00	● 185.19 (EX)
---	ELEVATION
---	DITCH
---	CONTOUR (0.25m INTERVALS)
---	PROPERTY LINE
---	PROJECT LOCATION BOUNDARY
---	FENCE
➔	OVERLAND FLOW DIRECTION

B. ISSUED FOR TENDER	JBM	DS	16.02.17		
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29		
Revision	By	Appd.	YY.MM.DD		
File Name:	133560106_C-400GP.dwg	Dwn.	Chkd.	Dign.	YY.MM.DD

Permit-Seal

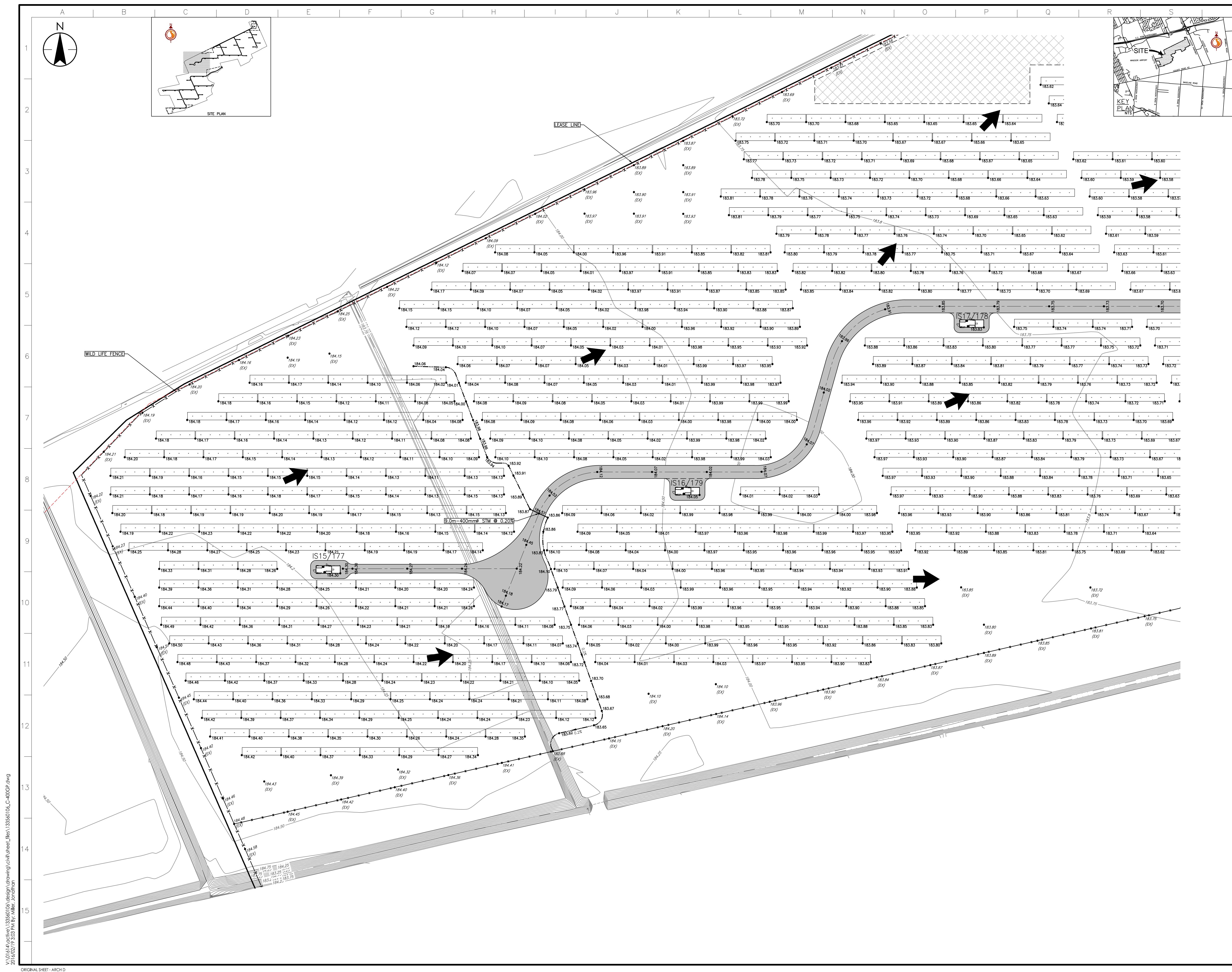
**PRELIMINARY  
NOT FOR CONSTRUCTION**

Client/Project  
**WINDSOR SOLAR LP**

**WINDSOR SOLAR ENERGY PROJECT  
 50MW SOLAR FARM**  
 Windsor, ON

Title  
**GRADING PLAN**

Project No.	133560106	Scale	0 7.5 22.5 37.5m 1:750
Drawing No.	C-410	Sheet	Revision



V:\016\A\active\133560106\design\drawing\civil\sheet\files\133560106\_C-400GP.dwg  
 2016/02/19 3:03 PM By: Miller, Jonathan  
 ORIGINAL SHEET - ARCHD

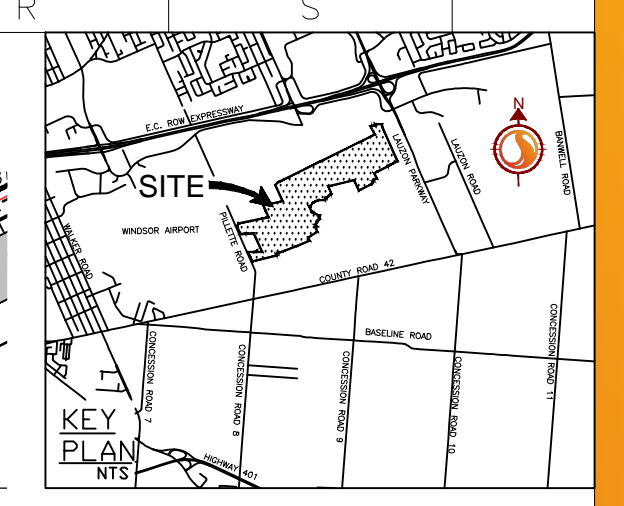
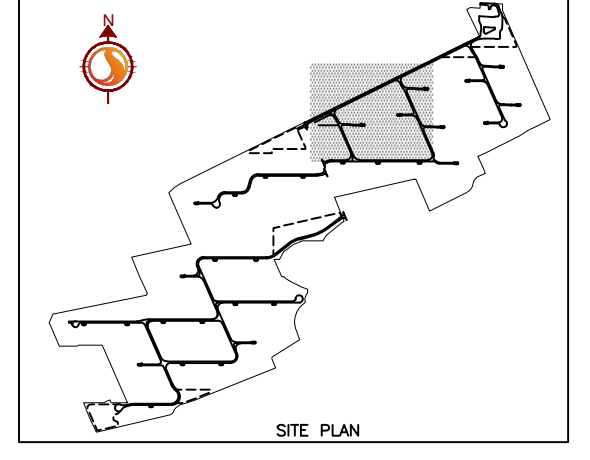
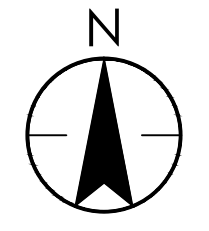












Copyright Reserved  
 The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.  
 The Copyrights to all designs and drawings are the property of Stantec. Reproduction or use for any purpose other than that authorized by Stantec is forbidden.

- Notes**
1. TOPOGRAPHICAL SURVEY CONDUCTED BY SURVEYORS ON SITE WAS COMPLETED ON JANUARY 20, 2016. TOPOGRAPHICAL SURVEY IS WITH 17 NAD83 CGRS. IN GRID WITH A SCALE FACTOR OF 0.999842435. HORIZONTAL AND VERTICAL CONTROL WAS PROVIDED USING SMARTNET RPK BASE STATION WHICH IS LOCATED LESS THAN 2 KM FROM THE SITE. THE BASE STATION IS LOCATED ON THE ROOF OF PCRS OFFICE AT 5255 COUNTY RD. 42.
  2. LEGAL PLAN OF SURVEY PROVIDED BY KENNEDY STUNTERFIELD HARLEY BROWER INC. MAY 20, 2015. SITE PLAN PROVIDED BY PCL CONSTRUCTION LEADERS, (REV. 15) JANUARY 29, 2016.
  3. SECTOPICAL INFORMATION PROVIDED BY DILLON CONSULTING LIMITED, AUGUST 2014.
  4. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
  5. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
  6. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
  7. IF, FOR UNFORESEEN REASONS, THE OWNER AND/OR HIS/HER REPRESENTATIVE MUST ENDOORSE AND/OR PRIVATE LANDS TO UNDERTAKE ANY WORKS, HE/SHE MUST OBTAIN WRITTEN PERMISSION FROM THE ADJACENT PROPERTY OWNERS PRIOR TO ENTERING UPON THE PRIVATE PROPERTY TO PERFORM ANY WORKS. COPIES OF THESE LETTERS OF CONSENT MUST BE SUBMITTED TO STANTEC. PRIOR TO ANY WORK BEING PERFORMED. FAILURE TO COMPLY WITH THE ABOVE IS AT THE PROPERTY OWNERS OWN RISK.
  8. THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY.
  9. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED EVERYWHERE PRIOR TO THE INSTALLATION OF SOLAR PANELS.
  10. CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
  11. CULVERTS ARE TO BE INSTALLED AS PER OPS 802.010. SOIL TYPE TO BE CONFIRMED ON SITE FOR DETERMINATION OF TRENCH WIDTH.
  12. ALL AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED. MIX AND APPLICATION RATE/METHOD TO BE SUBMITTED AND APPROVED BY OWNER PRIOR TO IMPLEMENTATION.
  13. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPS 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPS 577.
  14. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPS 206. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPS 1011.
  15. CULVERT TO BE CONSTRUCTED IN ACCORDANCE WITH OPS 421. HEIGHT OF FILL TABLE FOR CSP CULVERTS TO COMPLY WITH OPS 805.010.
  16. RIPRAP SHALL BE IN ACCORDANCE WITH OPS 810.010 SECTION B-B.
  17. STOCKPILES TO BE LOCATED IN LAYDOWN AREAS.

**Legend**

PROPOSED	EXISTING
● 187.00	● 185.19 (EX)
---	ELEVATION
---	DITCH
---	CONTOUR (0.25m INTERVALS)
---	PROPERTY LINE
---	PROJECT LOCATION BOUNDARY
---	FENCE
➔	OVERLAND FLOW DIRECTION

B. ISSUED FOR TENDER	JBM	DS	16.02.17
A. ISSUED FOR CLIENT REVIEW	JBM	DS	16.01.29
Revision	By	Appd.	YY.MM.DD
File Name:	133560106_C-400GP.dwg		
	Dwn.	Chkd.	Dign.
			YY.MM.DD

Permit-Seal

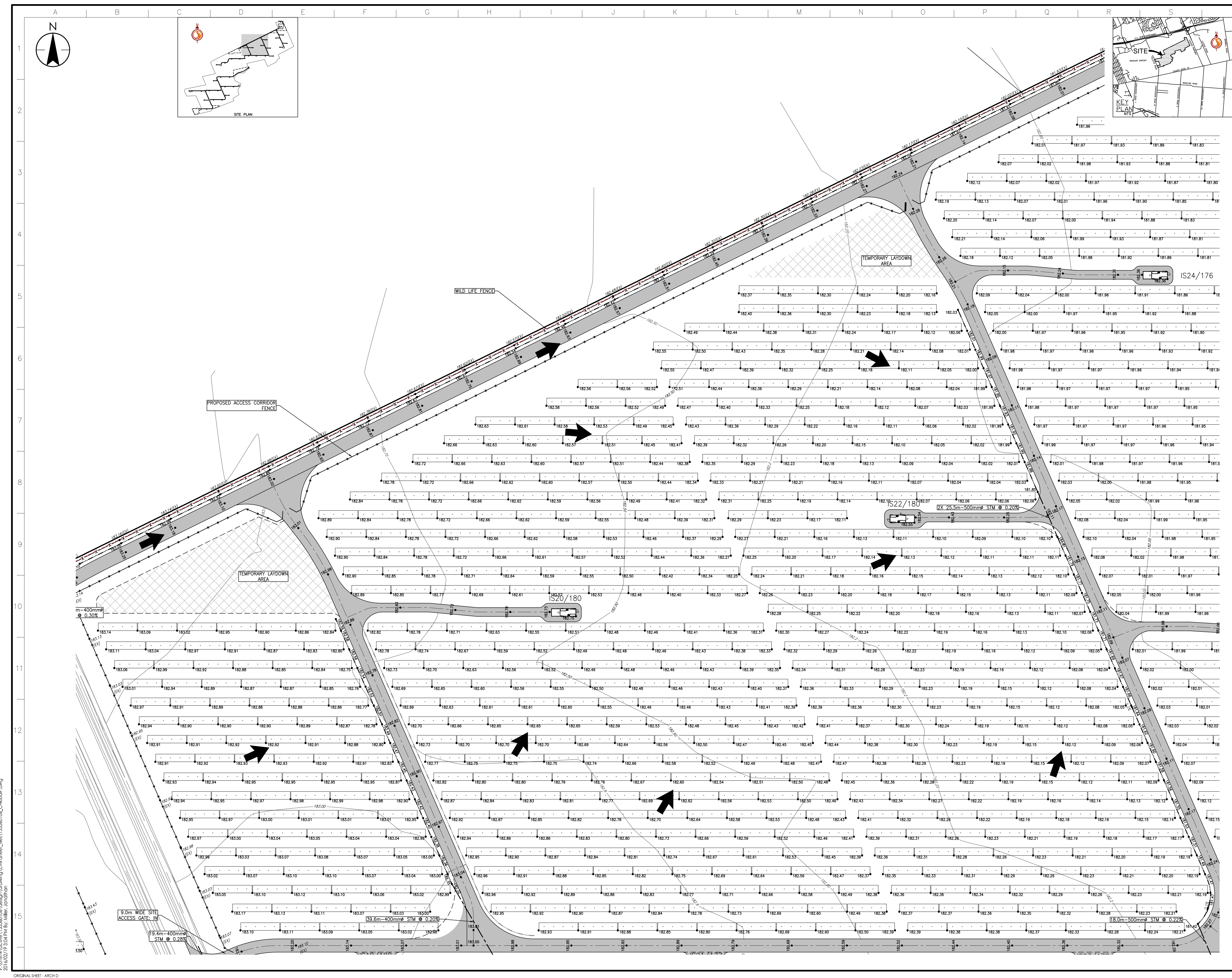
**PRELIMINARY**  
NOT FOR CONSTRUCTION

Client/Project  
**WINDSOR SOLAR LP**

**WINDSOR SOLAR ENERGY PROJECT**  
 50MW SOLAR FARM  
 Windsor, ON

Title  
**GRADING PLAN**

Project No.	Scale
133560106	0 7.5 22.5 37.5m 1:750
Drawing No.	Sheet
	Revision



V:\016\A\active\133560106\design\drawing\civil\sheet\133560106\_C-400GP.dwg  
 2016/02/19 3:04 PM By: Miller, Jonathan  
 ORIGINAL SHEET - ARCHD











# **APPENDIX C**

## **CULVERTS**



---

To:	Dan Santos	From:	Nick Emery
	Waterloo ON Office		London ON Office
File:	1335-60106	Date:	February 19, 2016

---

**Reference: Windsor Solar Project  
Proposed Culvert Sizing**

A hydrologic/hydraulic analysis was completed to select the proposed culvert diameters based on the available design information.

## **DESIGN FLOWS**

The proposed access road culverts are designed to convey the calculated 5-year peak discharges and the entrance culverts are designed to convey the calculated 10-year peak discharges. These rainfall events were selected for the proposed culverts for the following reasons:

- These storms have been used for access road and entrance culvert designs on previous solar farm projects in Ontario.
- Since most of the low points on the proposed access roads are not substantially higher than the downstream ground elevations, the risk of significant damage caused by road overtopping is likely low.
- The proposed site drainage system is likely subject to high tailwater elevations due to the limited capacities of the McGill and Lappan Drain channels. Designing the proposed culverts to accommodate more severe design events is unlikely to significantly reduce temporary ponding depths on the WSP site because of the anticipated high tailwater elevations.

The design flow for each culvert was calculated using the Rational Method. The corresponding calculation documentation is presented in the attached table.

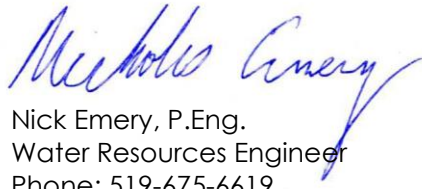
## **CULVERT DESIGN**

Hydraulic calculations were performed using the FHWA HY-8 culvert analysis software. The water surface elevation at the upstream face of each culvert was calculated based on the design flow and the proposed culvert geometry. The water surface elevation on the downstream side of each culvert was assumed to be equal to normal depth. The resulting calculated upstream water surface elevation at each culvert is less than both the local access road overtopping elevation and the culvert invert elevation.

**Reference: Windsor Solar Project  
Proposed Culvert Sizing**

To reduce the possibility of blockage caused by debris, the minimum allowable culvert diameter is 400 mm. The proposed culvert sizes and corresponding design information are summarized in the attached table.

**STANTEC CONSULTING LTD.**



Nick Emery, P.Eng.  
Water Resources Engineer  
Phone: 519-675-6619  
Fax: 519-645-6575  
nick.emery@stantec.com

Attachment: Culvert Design Summary Table  
HY-8 Culvert Analysis Report

c. Jonathan Miller (Stantec)  
Darren Scott (Stantec)



**Windsor Solar Project**  
**133560106**  
**Culvert Design Summary**

Culvert ID	Barrel Length <sup>1</sup> (m)	Upstream Invert	Downstream	Road	Approximate	Flow Path	Upstream Slope	Runoff	Time of	Design Storm	Rainfall	Peak Discharge <sup>6</sup> (cms)	Proposed	Proposed	No. of Culverts	Calculated	Freeboard <sup>8</sup> (m)	Pipe
		Elev. <sup>1</sup> (m)	Invert Elev. <sup>1</sup> (m)	Overtopping									Drainage Area <sup>2</sup> (ha)			Length <sup>2</sup> (m)		
15	39.31	182.33	182.24	183.00	2.15	110	0.2	0.2	0.87	5-year	34.2	0.041	400	CSP	1	182.61	0.12	-
16	25.48	181.75	181.70	182.12	6.18	300	0.2	0.2	1.44	5-year	23.9	0.082	500	CSP	2	182.08	0.04	EMBEDDED 0.1 m
17	9.44	180.95	180.94	181.48	4.29	150	0.2	0.2	1.02	5-year	30.6	0.073	500	CSP	1	181.34	0.11	EMBEDDED 0.1 m
18	17.97	181.42	181.39	182.26	9.82	300	0.2	0.2	1.44	5-year	23.9	0.131	500	CSP	1	181.87	0.05	-
19	9.11	184.43	184.42	184.92	7.44	360	0.2	0.2	1.58	5-year	22.4	0.093	500	CSP	1	184.79	0.13	-
20	9.00	183.62	183.60	184.23	5.82	290	0.2	0.2	1.42	5-year	24.2	0.078	400	CSP	1	183.98	0.04	-
21	9.72	184.55	184.53	185.08	6.73	380	0.2	0.2	1.62	5-year	22.0	0.082	400	CSP	1	184.92	0.03	-
22	7.30	183.63	183.61	-	4.35	290	0.2	0.2	1.42	5-year	24.2	0.059	400	CSP	1	183.94	0.09	-
23	9.30	183.87	183.85	-	2.39	200	0.2	0.2	1.18	5-year	27.6	0.037	400	CSP	1	184.11	0.16	-
24	23.70	181.28	181.23	-	3.00	150	0.2	0.2	1.02	5-year	30.6	0.051	400	CSP	1	181.60	0.08	-
25	14.00	181.50	181.28	181.86	14.49	600	0.2	0.2	2.04	5-year	18.7	0.151	500	CSP	2	181.86	0.00	EMBEDDED 0.1 m
26	12.60	182.84	182.81	183.52	0.13	125	0.2	0.55	0.57	10-year	53.3	0.010	400	CSP	1	182.96	0.28	-
28	13.90	182.91	182.89	183.49	7.48	450	0.2	0.2	1.76	10-year	23.9	0.099	500	CSP	1	183.38	0.03	EMBEDDED 0.1 m
29	19.40	182.85	182.79	183.46	0.33	325	0.2	0.55	0.92	10-year	38.0	0.019	400	CSP	1	183.02	0.23	-
30	19.90	182.64	182.61	183.59	7.48	450	0.2	0.2	1.76	10-year	23.9	0.099	500	CSP	1	183.12	0.02	EMBEDDED 0.1 m
31	18.60	182.45	182.40	183.33	14.96	450	0.2	0.2	1.76	10-year	23.9	0.199	500	CSP	1	182.84	0.11	-
33	19.00	180.63	180.62	-	5.27	270	0.2	0.24	1.31	10-year	29.6	0.104	500	CSP	1	181.08	0.05	-
34	18.50	180.61	180.60	-	5.74	310	0.2	0.29	1.32	10-year	29.4	0.136	500	CSP	2	180.96	0.15	-

Notes:  
<sup>1</sup> Value from proposed grading plans.  
<sup>2</sup> Measured from proposed grading plans.  
<sup>3</sup> Average site slope assumed for all drainage areas.  
<sup>4</sup> Time of concentration calculated using the Airport Equation.  
<sup>5</sup> Rainfall intensity calculated using the Environment Canada IDF curves for the Windsor Airport.  
<sup>6</sup> Peak discharge calculated using the Rational Method.  
<sup>7</sup> Headwater elevation calculated using the FHWA HY-8 culvert analysis software.  
<sup>8</sup> Freeboard calculated by subtracting the minimum of either the road overtopping elevation or the upstream pipe invert elevation from the calculated headwater elevation.  
<sup>9</sup> Depth of embedment below the proposed ditch bottom. The depth of embedment is included in the proposed culvert invert elevations.

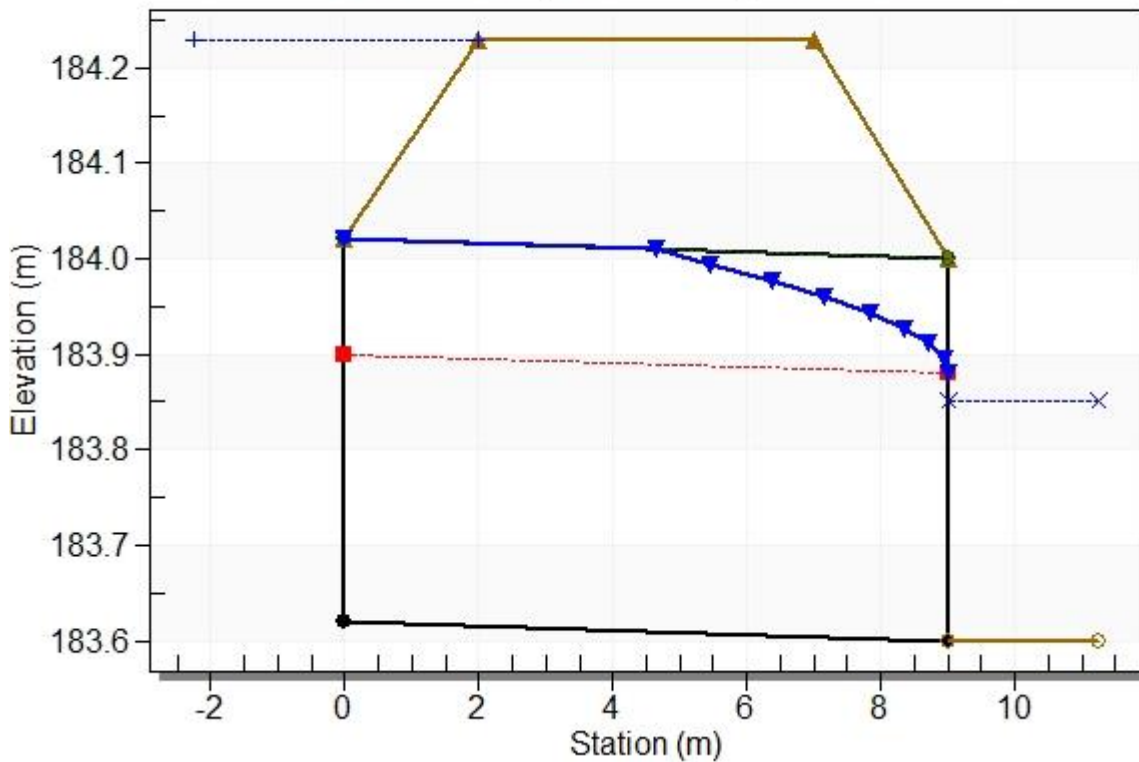
# HY-8 Culvert Analysis Report



## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 20, Design Discharge - 0.15 cms

Culvert - Culvert 2, Culvert Discharge - 0.15 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 183.62 m

Outlet Station: 9.00 m

Outlet Elevation: 183.60 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 1 - Downstream Channel Rating Curve (Crossing: Crossing 20)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.08	183.78	0.18	0.28	3.50	0.25
0.15	183.85	0.25	0.34	4.90	0.26

**Tailwater Channel Data - Crossing 20**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 183.60 m

**Roadway Data for Crossing: Crossing 20**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 184.23 m

Roadway Surface: Gravel

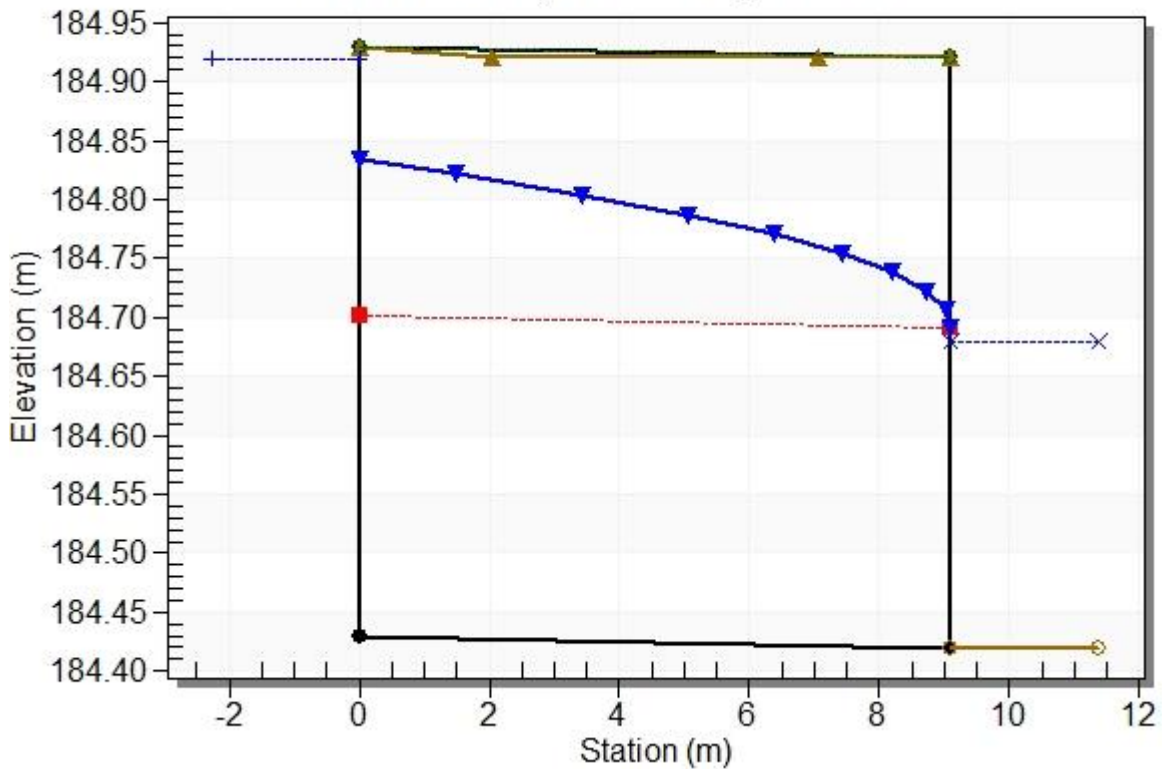
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 19, Design Discharge - 0.16 cms

Culvert - Culvert 2, Culvert Discharge - 0.16 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 184.43 m

Outlet Station: 9.11 m

Outlet Elevation: 184.42 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 2 - Downstream Channel Rating Curve (Crossing: Crossing 19)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.09	184.62	0.20	0.30	3.83	0.25
0.16	184.68	0.26	0.35	5.07	0.26

**Tailwater Channel Data - Crossing 19**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 184.42 m

**Roadway Data for Crossing: Crossing 19**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 184.92 m

Roadway Surface: Gravel

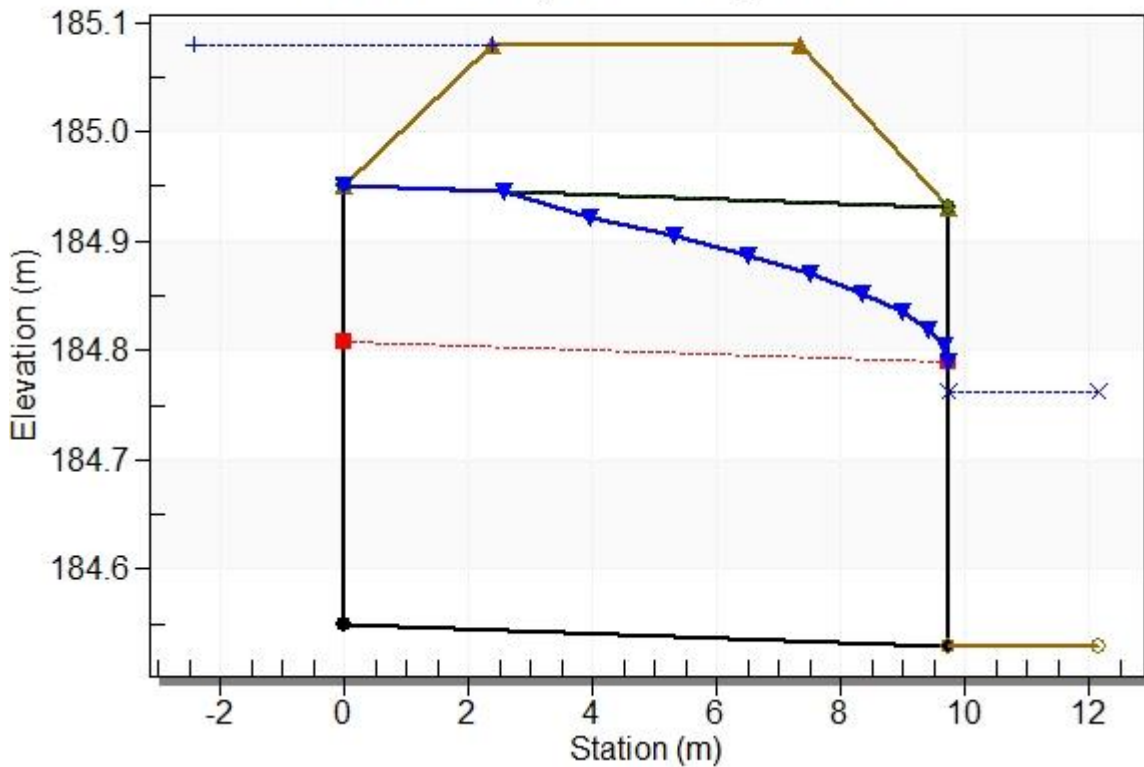
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 21, Design Discharge - 0.13 cms

Culvert - Culvert 2, Culvert Discharge - 0.13 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 184.55 m

Outlet Station: 9.72 m

Outlet Elevation: 184.53 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 3 - Downstream Channel Rating Curve (Crossing: Crossing 21)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.08	184.71	0.18	0.29	3.59	0.25
0.13	184.76	0.23	0.33	4.56	0.26

**Tailwater Channel Data - Crossing 21**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 184.53 m

**Roadway Data for Crossing: Crossing 21**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 185.08 m

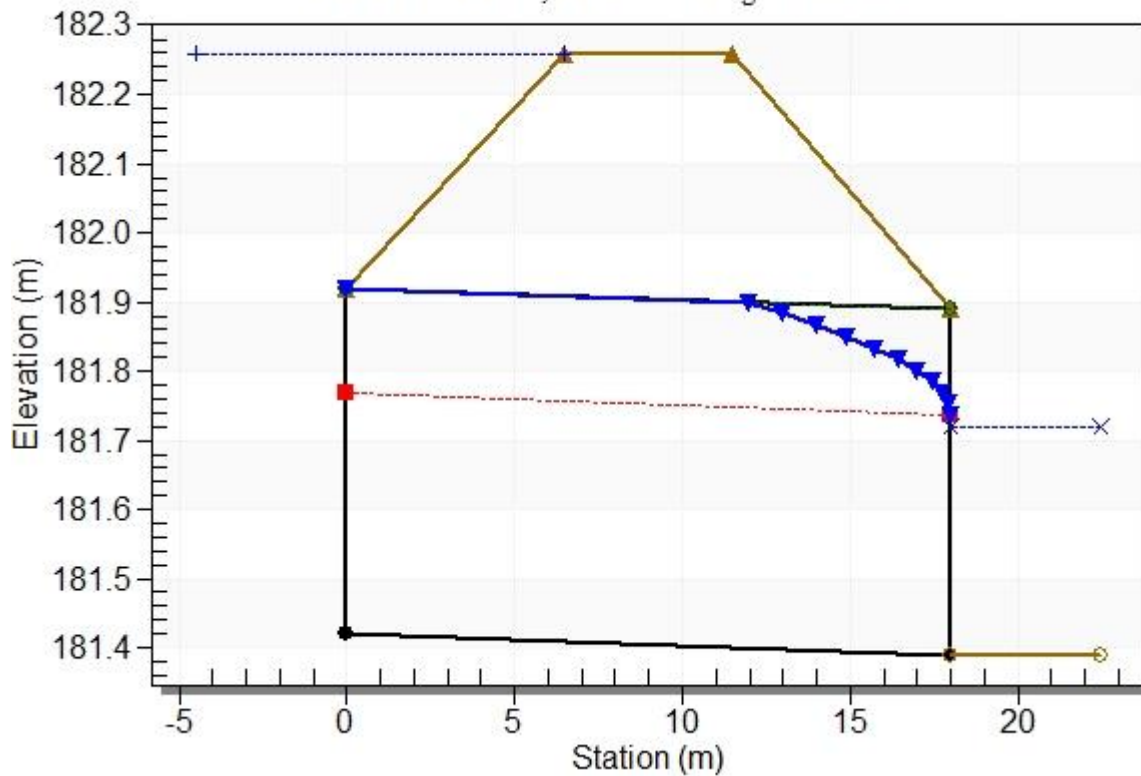
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 18, Design Discharge - 0.26 cms

Culvert - Culvert 2, Culvert Discharge - 0.26 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 181.42 m

Outlet Station: 17.97 m

Outlet Elevation: 181.39 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE



**Table 4 - Downstream Channel Rating Curve (Crossing: Crossing 18)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.13	181.62	0.23	0.33	4.58	0.26
0.26	181.72	0.33	0.40	6.45	0.27

**Tailwater Channel Data - Crossing 18**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 181.39 m

**Roadway Data for Crossing: Crossing 18**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 182.26 m

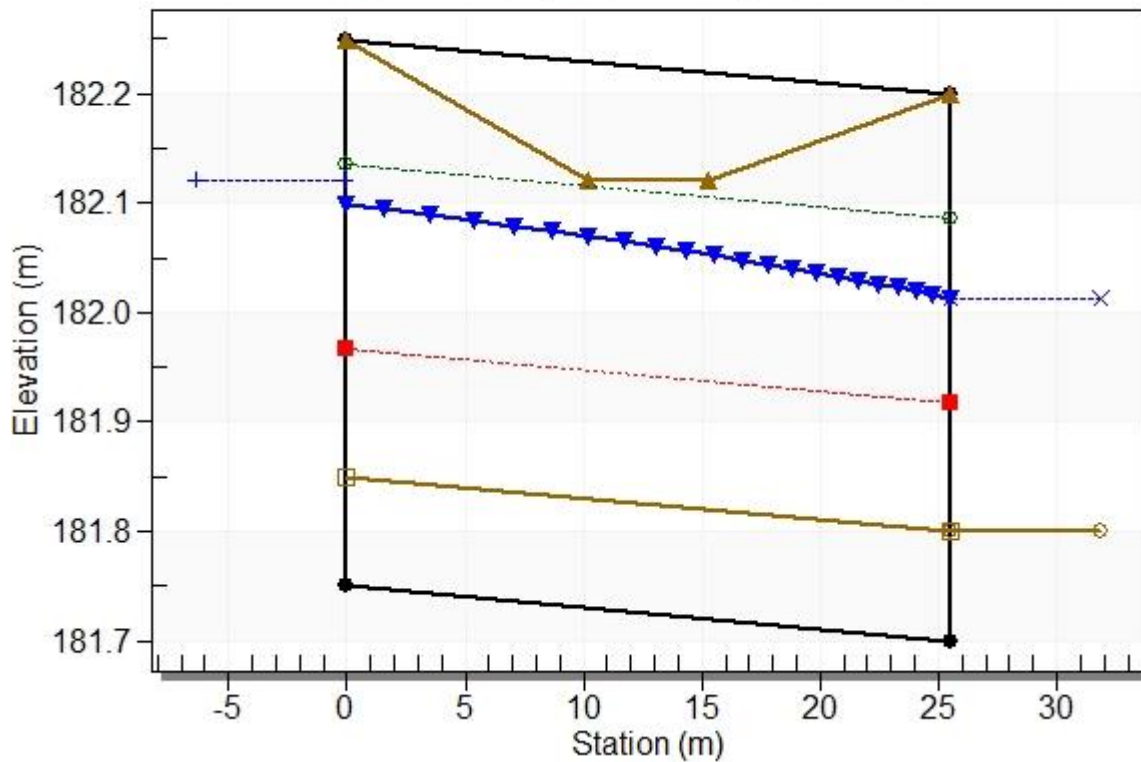
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 16, Design Discharge - 0.11 cms

Culvert - Culvert 2, Culvert Discharge - 0.11 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 181.75 m

Outlet Station: 25.48 m

Outlet Elevation: 181.70 m

Number of Barrels: 2

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 100.00 mm

Barrel Manning's n: 0.0240 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 5 - Downstream Channel Rating Curve (Crossing: Crossing 16)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.08	181.98	0.18	0.29	3.59	0.25
0.11	182.01	0.21	0.31	4.18	0.26

**Tailwater Channel Data - Crossing 16**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 181.80 m

**Roadway Data for Crossing: Crossing 16**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 182.12 m

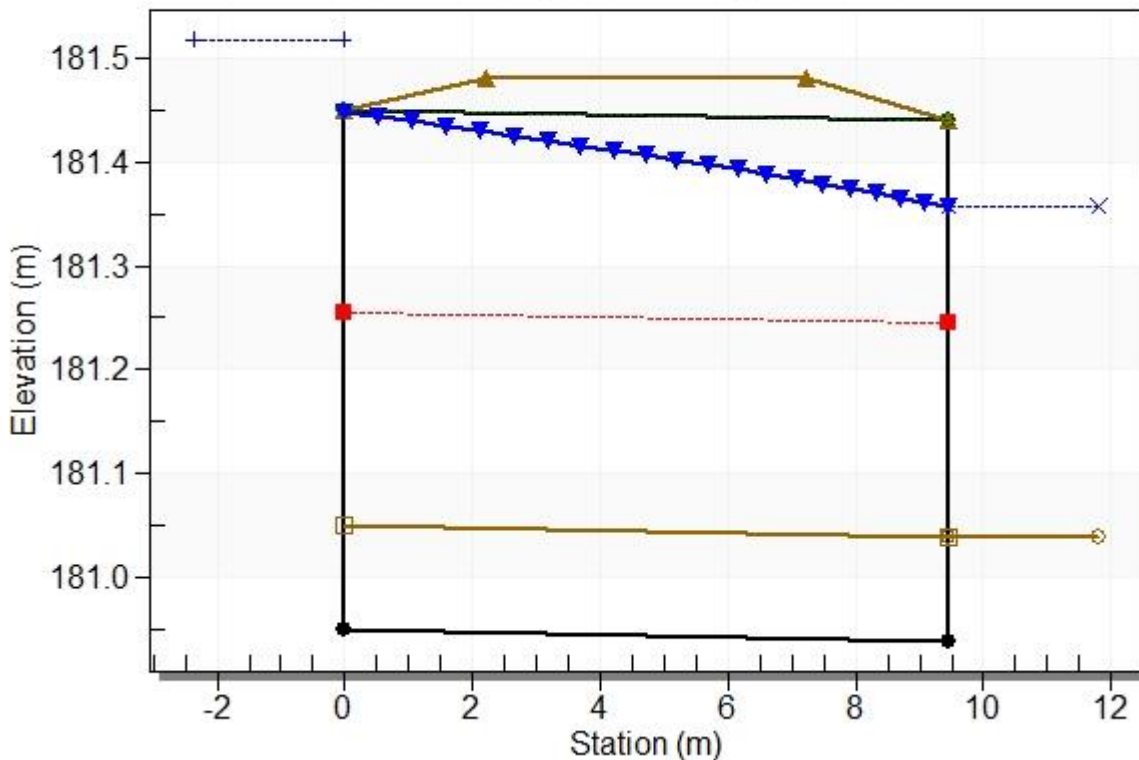
Roadway Surface: Gravel

Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 17, Design Discharge - 0.24 cms  
Culvert - Culvert 2, Culvert Discharge - 0.14 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 180.95 m

Outlet Station: 9.44 m

Outlet Elevation: 180.94 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 100.00 mm

Barrel Manning's n: 0.0240 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 6 - Downstream Channel Rating Curve (Crossing: Crossing 17)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.07	181.21	0.17	0.28	3.38	0.25
0.24	181.36	0.32	0.39	6.20	0.27

**Tailwater Channel Data - Crossing 17**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 181.04 m

**Roadway Data for Crossing: Crossing 17**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 181.48 m

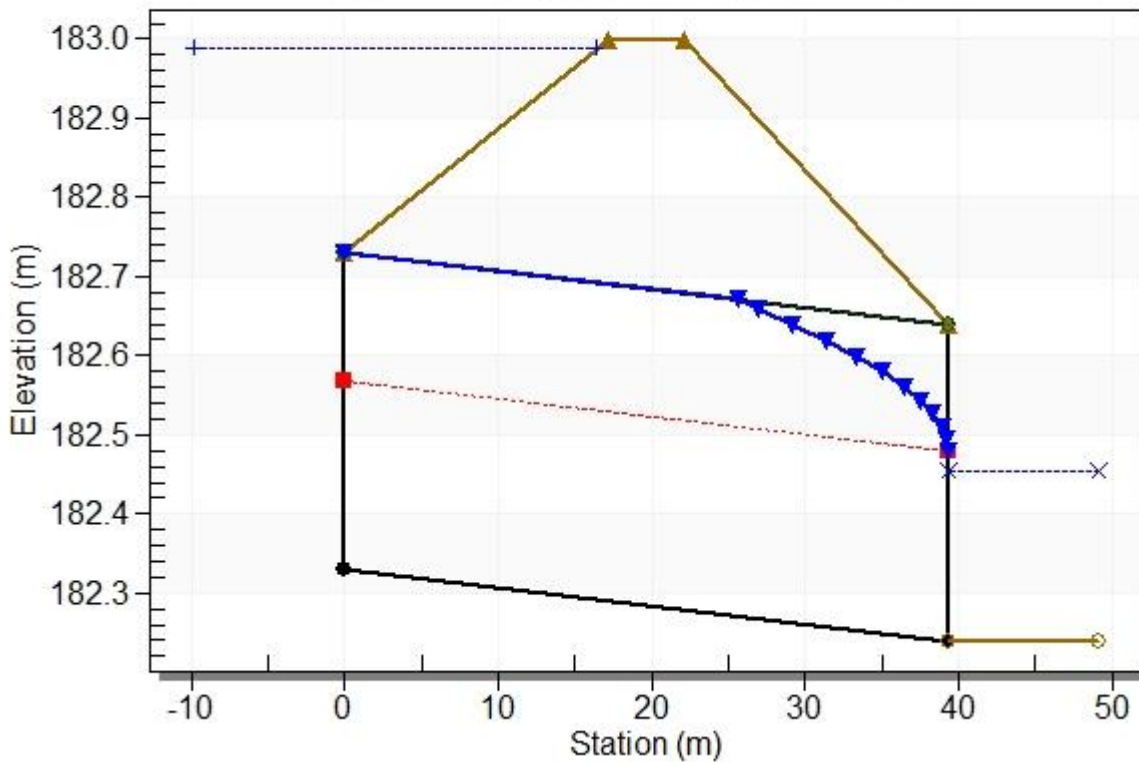
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

Crossing - Crossing 15, Design Discharge - 0.11 cms

Culvert - Culvert 2, Culvert Discharge - 0.11 cms



### Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.33 m

Outlet Station: 39.31 m

Outlet Elevation: 182.24 m

Number of Barrels: 1

### Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE



**Table 7 - Downstream Channel Rating Curve (Crossing: Crossing 15)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.04	182.37	0.13	0.24	2.47	0.24
0.11	182.45	0.21	0.31	4.18	0.26

**Tailwater Channel Data - Crossing 15**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.24 m

**Roadway Data for Crossing: Crossing 15**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.00 m

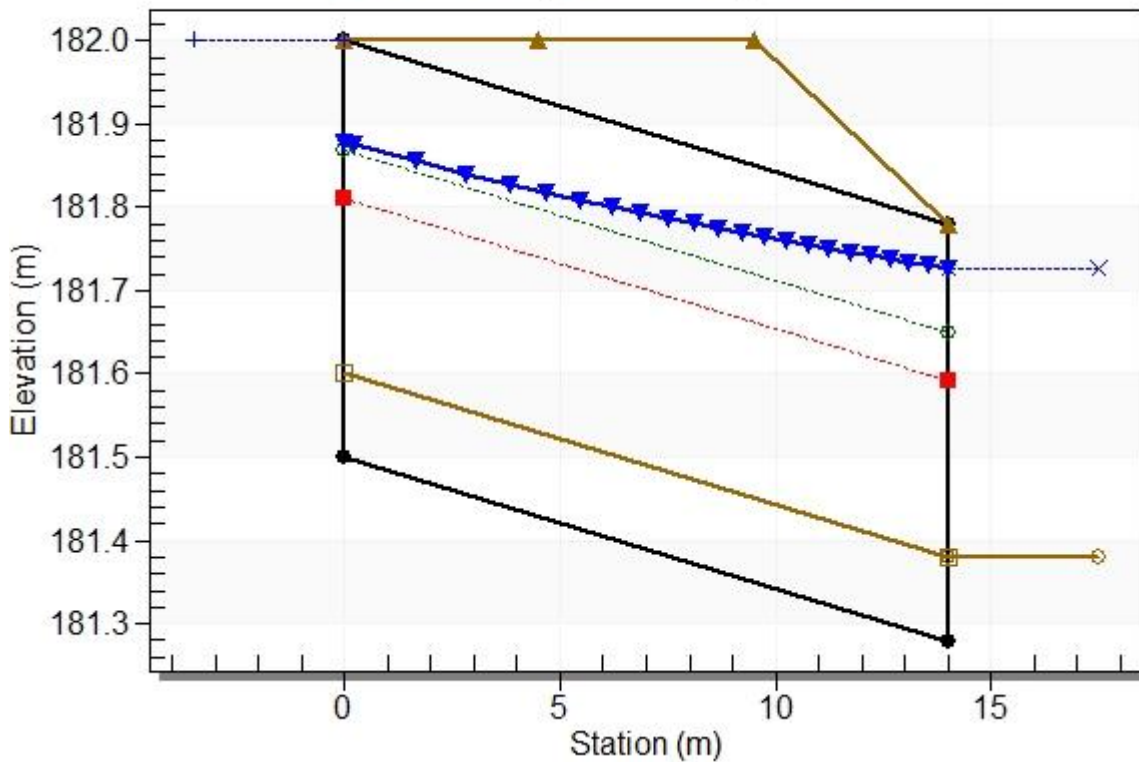
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 25, Design Discharge - 0.29 cms

Culvert - Culvert 2, Culvert Discharge - 0.29 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 181.50 m

Outlet Station: 14.00 m

Outlet Elevation: 181.28 m

Number of Barrels: 2

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 100.00 mm

Barrel Manning's n: 0.0240 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 8 - Downstream Channel Rating Curve (Crossing: Culvert 25)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.15	181.63	0.25	0.34	4.92	0.26
0.29	181.73	0.35	0.41	6.80	0.27

**Tailwater Channel Data - Culvert 25**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 181.38 m

**Roadway Data for Crossing: Culvert 25**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 182.00 m

Roadway Surface: Gravel

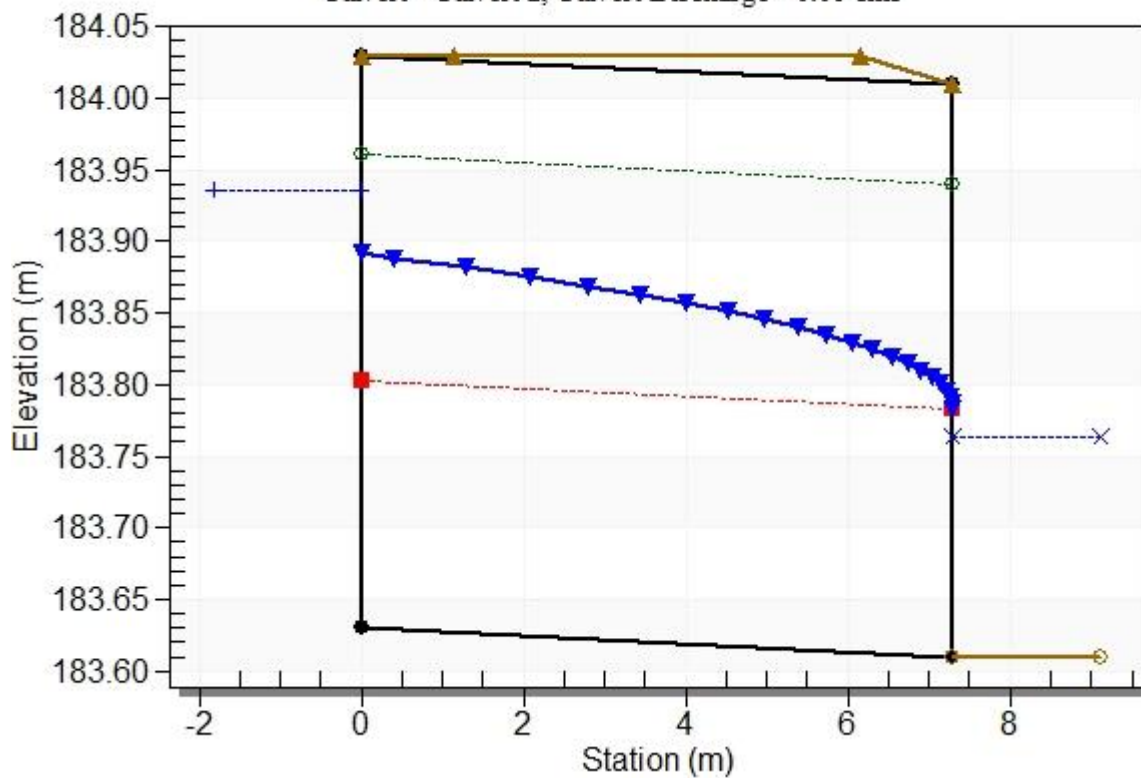
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 22, Design Discharge - 0.06 cms

Culvert - Culvert 2, Culvert Discharge - 0.06 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 183.63 m

Outlet Station: 7.30 m

Outlet Elevation: 183.61 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 9 - Downstream Channel Rating Curve (Crossing: Culvert 22)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.06	183.76	0.15	0.26	3.01	0.25
0.06	183.76	0.15	0.26	3.01	0.25

**Tailwater Channel Data - Culvert 22**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 3.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 183.61 m

**Roadway Data for Crossing: Culvert 22**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 184.03 m

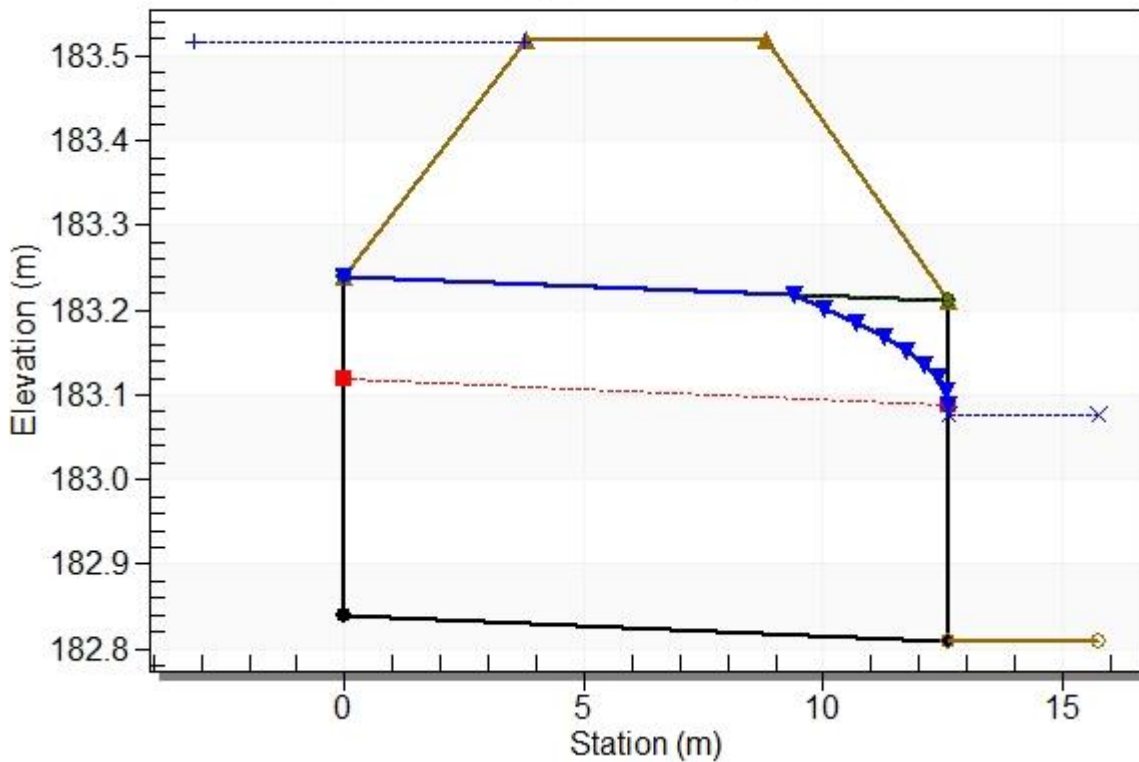
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 26, Design Discharge - 0.15 cms

Culvert - Culvert 2, Culvert Discharge - 0.15 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.84 m

Outlet Station: 12.60 m

Outlet Elevation: 182.81 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 10 - Downstream Channel Rating Curve (Crossing: Culvert 26)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.01	182.87	0.06	0.15	1.14	0.22
0.15	183.08	0.27	0.37	5.24	0.26

**Tailwater Channel Data - Culvert 26**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.81 m

**Roadway Data for Crossing: Culvert 26**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.52 m

Roadway Surface: Gravel

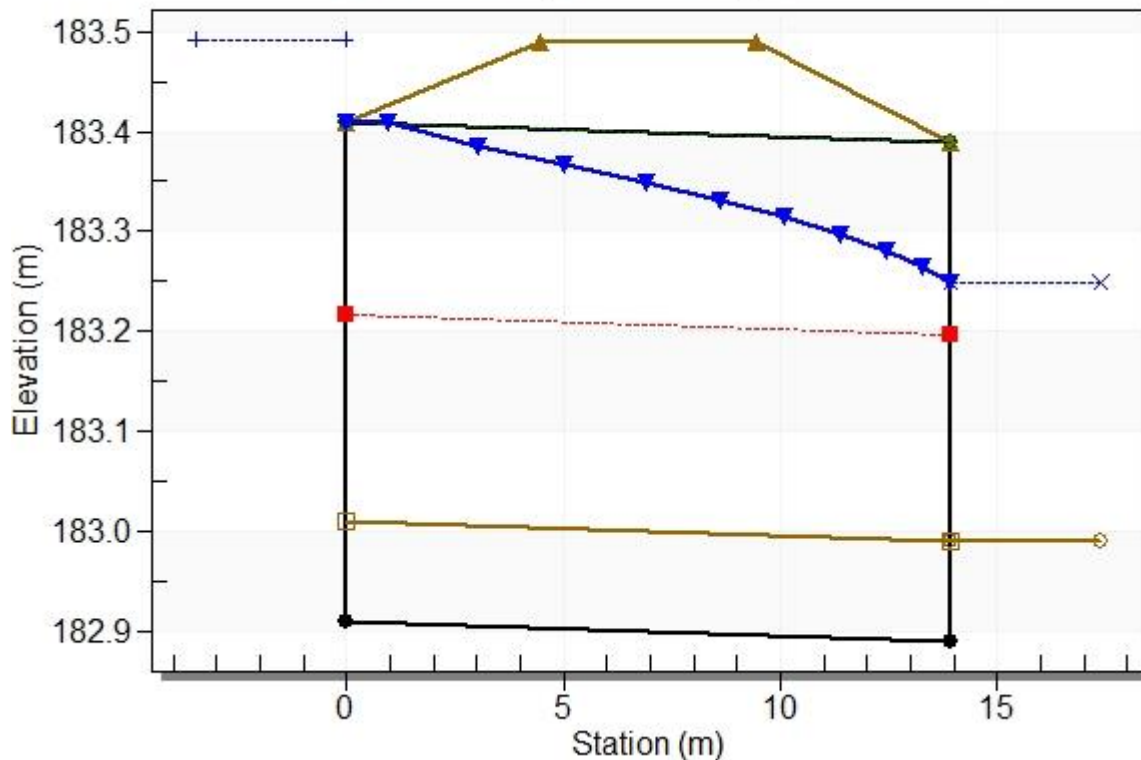
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 28, Design Discharge - 0.14 cms

Culvert - Culvert 2, Culvert Discharge - 0.14 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.91 m

Outlet Station: 13.90 m

Outlet Elevation: 182.89 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 100.00 mm

Barrel Manning's n: 0.0240 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 11 - Downstream Channel Rating Curve (Crossing: Culvert 28)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.10	183.20	0.21	0.32	4.19	0.26
0.14	183.25	0.26	0.36	5.05	0.26

**Tailwater Channel Data - Culvert 28**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.99 m

**Roadway Data for Crossing: Culvert 28**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.49 m

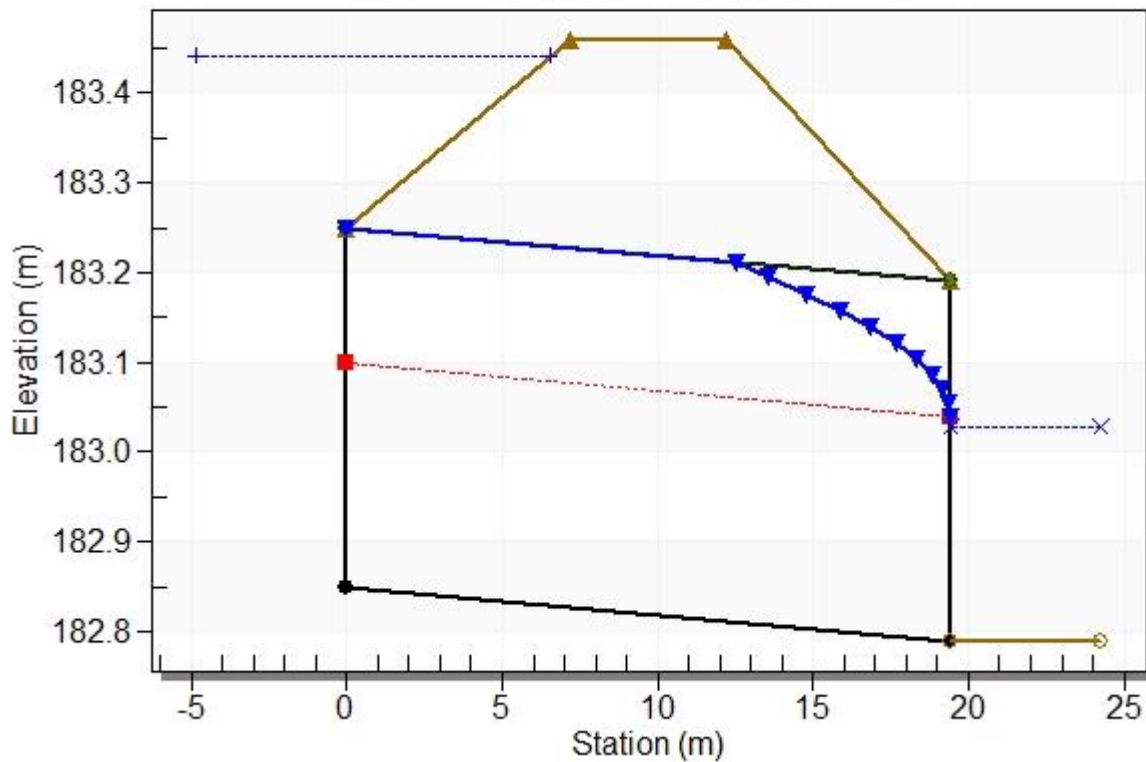
Roadway Surface: Gravel

Roadway Top Width: 5.00 m

## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 29, Design Discharge - 0.12 cms

Culvert - Culvert 2, Culvert Discharge - 0.12 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.85 m

Outlet Station: 19.40 m

Outlet Elevation: 182.79 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 12 - Downstream Channel Rating Curve (Crossing: Culvert 29)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.02	182.87	0.08	0.19	1.65	0.23
0.12	183.03	0.24	0.34	4.65	0.26

**Tailwater Channel Data - Culvert 29**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.79 m

**Roadway Data for Crossing: Culvert 29**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.46 m

Roadway Surface: Gravel

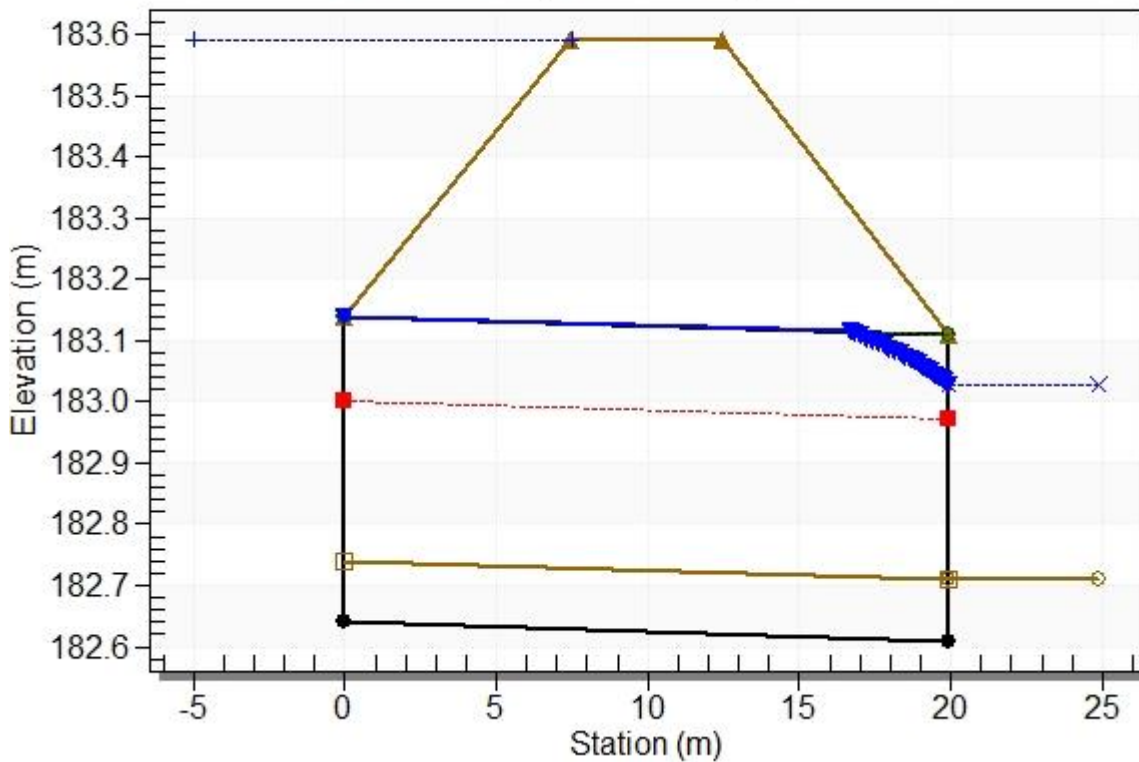
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 30, Design Discharge - 0.21 cms

Culvert - Culvert 2, Culvert Discharge - 0.21 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.64 m

Outlet Station: 19.90 m

Outlet Elevation: 182.61 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 100.00 mm

Barrel Manning's n: 0.0240 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 13 - Downstream Channel Rating Curve (Crossing: Culvert 30)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.10	182.92	0.21	0.32	4.19	0.26
0.21	183.03	0.32	0.40	6.26	0.27

**Tailwater Channel Data - Culvert 30**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.71 m

**Roadway Data for Crossing: Culvert 30**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.59 m

Roadway Surface: Gravel

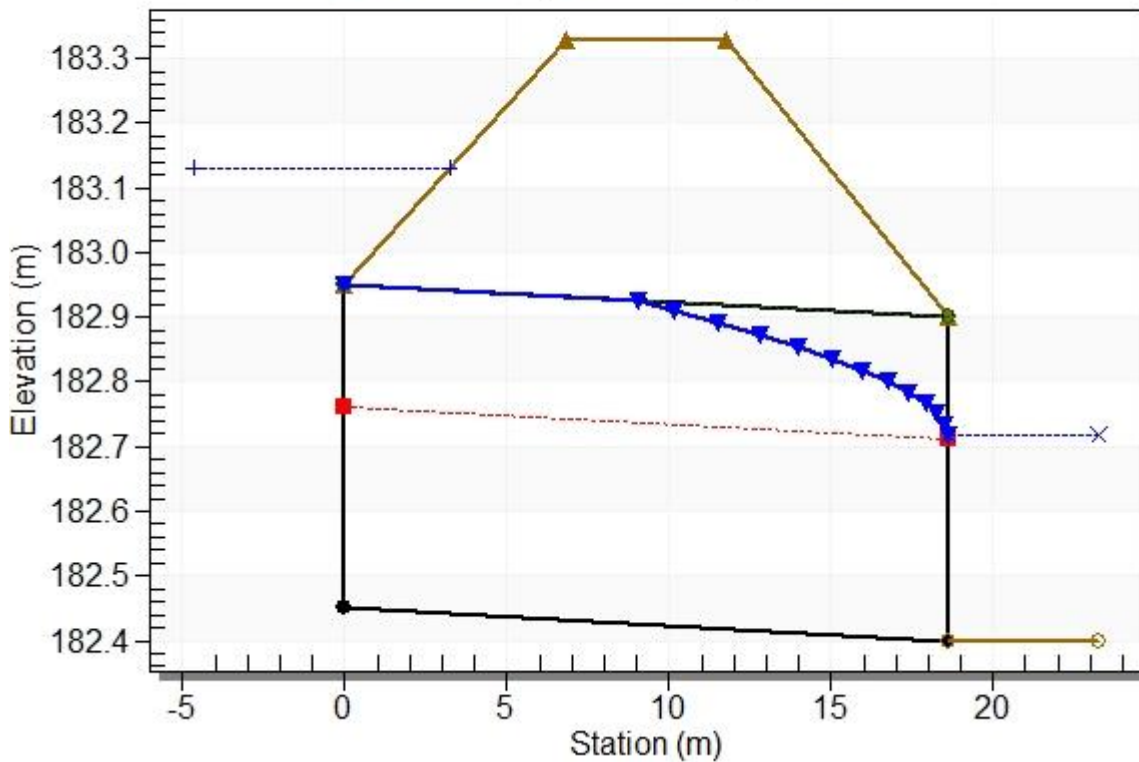
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 31, Design Discharge - 0.21 cms

Culvert - Culvert 2, Culvert Discharge - 0.21 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 182.45 m

Outlet Station: 18.60 m

Outlet Elevation: 182.40 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 14 - Downstream Channel Rating Curve (Crossing: Culvert 31)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.10	182.61	0.21	0.32	4.19	0.26
0.21	182.72	0.32	0.40	6.26	0.27

**Tailwater Channel Data - Culvert 31**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 182.40 m

**Roadway Data for Crossing: Culvert 31**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 183.33 m

Roadway Surface: Gravel

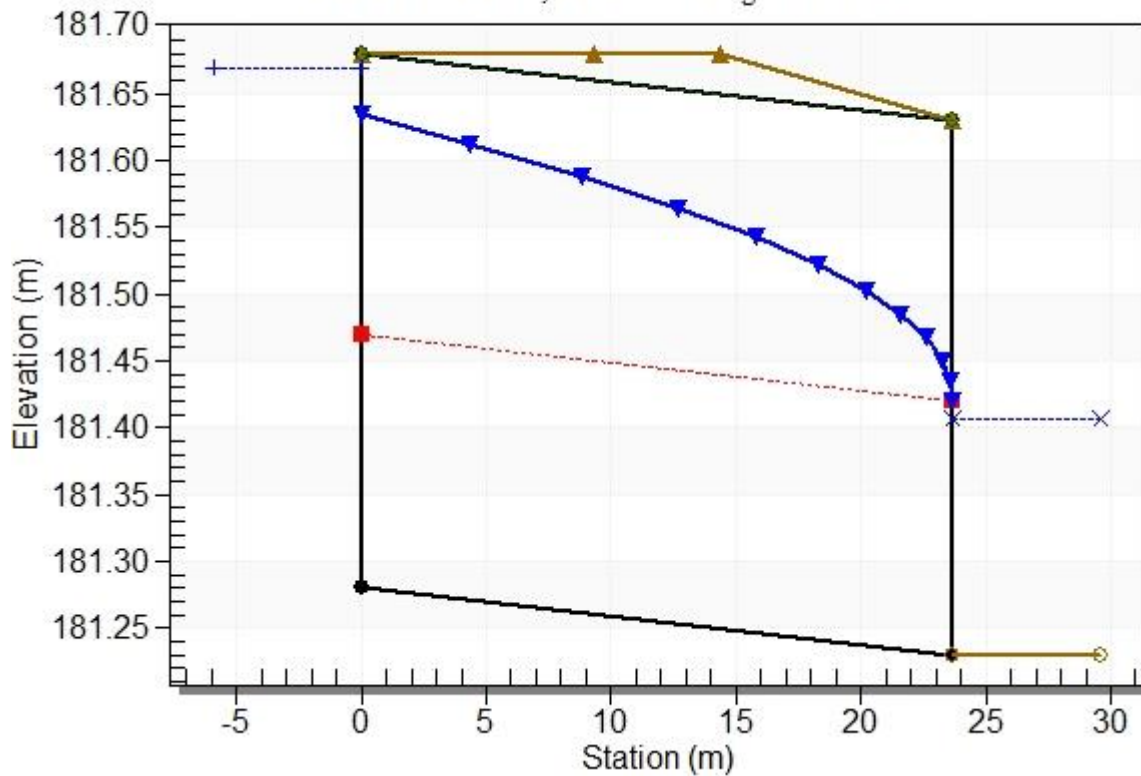
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 24, Design Discharge - 0.07 cms

Culvert - Culvert 2, Culvert Discharge - 0.07 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 181.28 m

Outlet Station: 23.70 m

Outlet Elevation: 181.23 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 15 - Downstream Channel Rating Curve (Crossing: Culvert 24)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.05	181.38	0.15	0.27	2.91	0.24
0.07	181.41	0.18	0.29	3.47	0.25

**Tailwater Channel Data - Culvert 24**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 181.23 m

**Roadway Data for Crossing: Culvert 24**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 181.68 m

Roadway Surface: Gravel

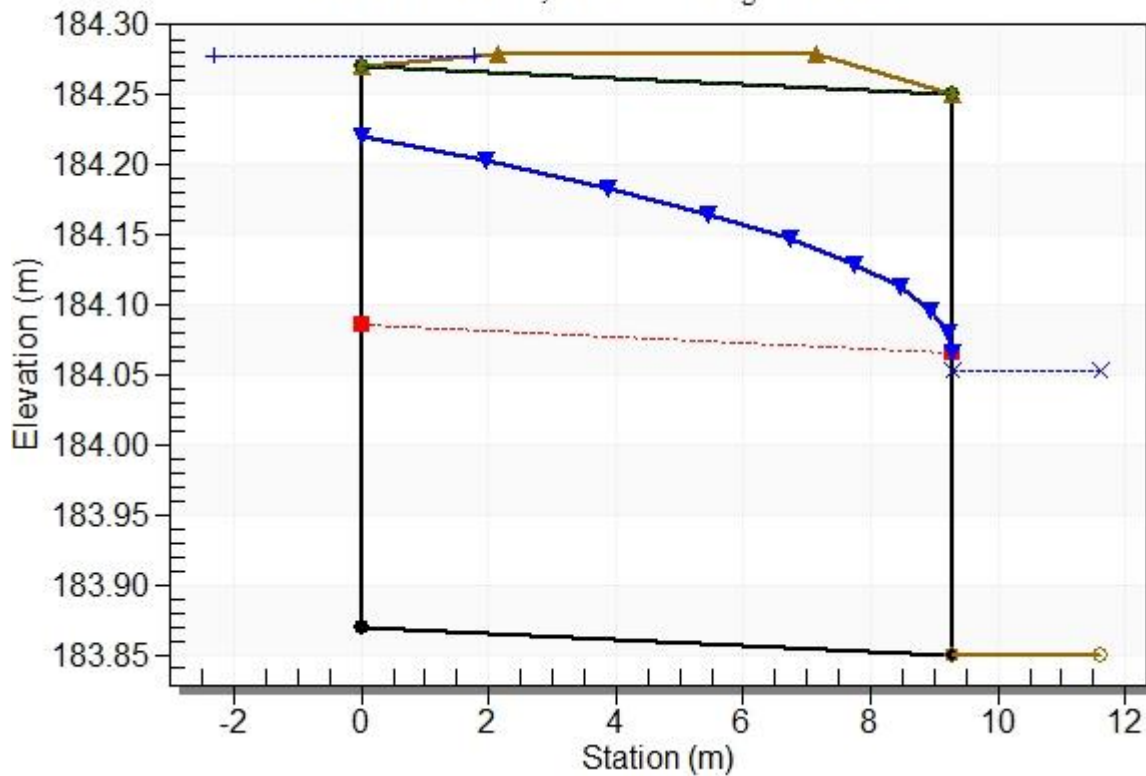
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 23, Design Discharge - 0.09 cms

Culvert - Culvert 2, Culvert Discharge - 0.09 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 183.87 m

Outlet Station: 9.30 m

Outlet Elevation: 183.85 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 400.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 16 - Downstream Channel Rating Curve (Crossing: Culvert 23)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.04	183.97	0.12	0.24	2.43	0.24
0.09	184.05	0.20	0.32	3.98	0.25

**Tailwater Channel Data - Culvert 23**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (2:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 183.85 m

**Roadway Data for Crossing: Culvert 23**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 184.28 m

Roadway Surface: Gravel

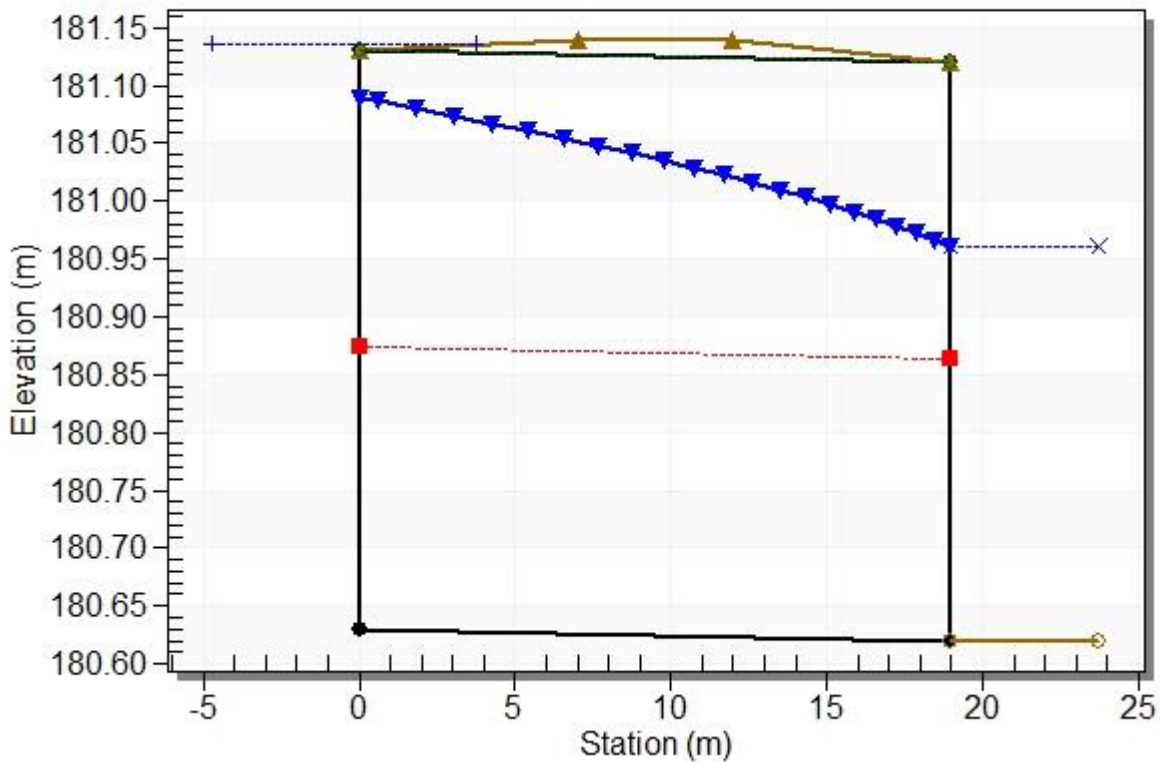
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 33, Design Discharge - 0.13 cms

Culvert - Culvert 2, Culvert Discharge - 0.13 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 180.63 m

Outlet Station: 19.00 m

Outlet Elevation: 180.62 m

Number of Barrels: 1

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 17 - Downstream Channel Rating Curve (Crossing: Culvert 33)**

Flow (cms)	Water Surface Elev (m)	Depth (m)
3.67	180.96	0.34
4.59	180.96	0.34

**Tailwater Channel Data - Culvert 33**

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 180.96 m

**Roadway Data for Crossing: Culvert 33**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 181.14 m

Roadway Surface: Gravel

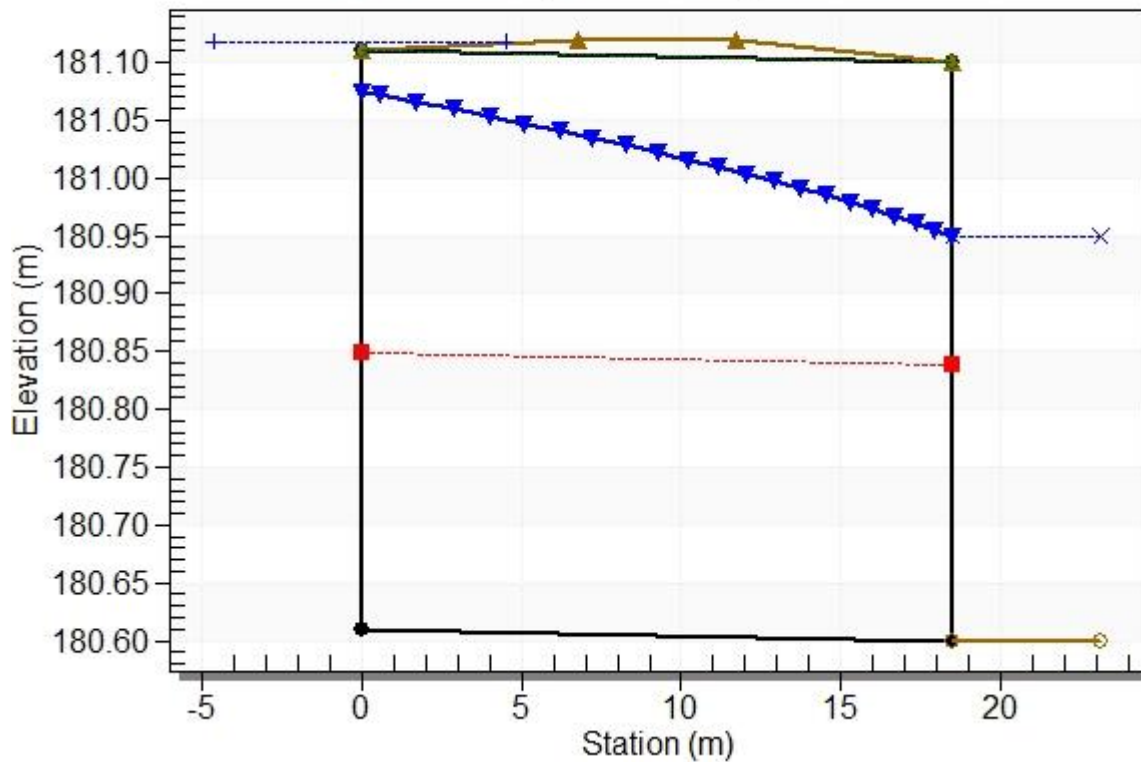
Roadway Top Width: 5.00 m



## Water Surface Profile Plot for Culvert: Culvert 2

### Crossing - Culvert 34, Design Discharge - 0.25 cms

Culvert - Culvert 2, Culvert Discharge - 0.25 cms



## Site Data - Culvert 2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 m

Inlet Elevation: 180.61 m

Outlet Station: 18.50 m

Outlet Elevation: 180.60 m

Number of Barrels: 2

## Culvert Data Summary - Culvert 2

Barrel Shape: Circular

Barrel Diameter: 500.00 mm

Barrel Material: Corrugated Steel

Embedment: 0.00 mm

Barrel Manning's n: 0.0240

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: NONE

**Table 18 - Downstream Channel Rating Curve (Crossing: Culvert 34)**

Flow (cms)	Water Surface Elev (m)	Depth (m)	Velocity (m/s)	Shear (Pa)	Froude Number
0.14	180.85	0.25	0.36	4.98	0.26
0.25	180.95	0.35	0.42	6.85	0.27

**Tailwater Channel Data - Culvert 34**

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 1.00 m

Side Slope (H:V): 2.00 (\_:1)

Channel Slope: 0.0020

Channel Manning's n: 0.0400

Channel Invert Elevation: 180.60 m

**Roadway Data for Crossing: Culvert 34**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 10.00 m

Crest Elevation: 181.12 m

Roadway Surface: Gravel

Roadway Top Width: 5.00 m



**APPENDIX D**  
**RUNOFF QUANTITY (PEAK FLOWS)**

**1335-60106 - Windsor Solar Project**  
**SWMHYMO Parameters**

**Existing Conditions**

Catchment Number	SWMHYMO Command	Comments	Area (ha)	CN	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
EXT1	DESIGN NASHYD	Airfield drainage to Lappan Drain upstream of Pilette Road	42.26	73	0.3	650	1.85	1.11
EXT2	DESIGN NASHYD	Cropped land drainage to Lappan Drain via roadside ditch	22.52	82	0.2	650	2.12	1.27
EXT3	DESIGN NASHYD	Cropped land drainage to Lappan Drain via roadside ditch	42.81	82	0.3	650	1.85	1.11
104	DESIGN NASHYD	Cropped land drainage to Lappan Drain via ditches	19.36	82	0.2	850	2.42	1.45
105	DESIGN NASHYD	Cropped land drainage to Lappan Drain via ditches	25.24	82	0.2	850	2.42	1.45
105A	DESIGN NASHYD	Cropped land drainage to Lappan Drain via shallow surface flow	6.80	82	0.3	480	1.59	0.96
106	DESIGN NASHYD	Cropped land drainage to McGill Drain via ditches	39.07	82	0.2	1070	2.72	1.63
EXT4	DESIGN NASHYD	Cropped land drainage to McGill Drain via ditches	21.08	80	0.2	1340	3.04	1.83
107	DESIGN NASHYD	Cropped land drainage to McGill Drain via ditches	6.53	82	0.3	350	1.36	0.82
108	DESIGN NASHYD	Cropped land drainage to McGill Drain via Jefferson Blvd ditch	15.67	82	0.2	480	1.82	1.09
109	DESIGN NASHYD	Cropped land drainage to McGill Drain via roadside ditch	47.17	82	0.3	630	1.83	1.10
EXT8	DESIGN NASHYD	Cropped land drainage to Lappan Drain via shallow surface flow	6.60	82	0.2	270	1.37	0.82
EXT5	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	14.81	82	0.1	590	2.54	1.52
EXT6	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	24.11	80	0.1	590	2.54	1.52
113	DESIGN NASHYD	Cropped land drainage to culvert via shallow surface flow	17.65	82	0.2	330	1.51	0.91
114	DESIGN NASHYD	Cropped land drainage to McGill Drain via roadside ditch	4.88	82	0.2	330	1.51	0.91
EXT7	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	18.59	82	0.1	550	2.45	1.47
<b>Total</b>			<b>375.15</b>					

**Proposed Conditions**

Catchment Number	SWMHYMO Command	Comments	Area (ha)	CN	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
EXT1	DESIGN NASHYD	Airfield drainage to Lappan Drain upstream of Pilette Road	42.26	73	0.3	650	1.85	1.11
EXT2	DESIGN NASHYD	Cropped land drainage to Lappan Drain via roadside ditch	22.52	82	0.2	650	2.12	1.27
EXT3	DESIGN NASHYD	Cropped land drainage to Lappan Drain via roadside ditch	42.81	82	0.3	650	1.85	1.11
EXT4	DESIGN NASHYD	Cropped land drainage to McGill Drain via ditches	21.08	80	0.2	1340	3.04	1.83
EXT5	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	14.81	82	0.1	590	2.54	1.52
EXT6	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	24.11	80	0.1	590	2.54	1.52
EXT7	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	18.59	82	0.1	550	2.45	1.47
EXT8	DESIGN NASHYD	Cropped land drainage to Lappan Drain via shallow surface flow	6.60	82	0.2	270	1.37	0.82
201	DESIGN NASHYD	Cropped land drainage to Lappan Drain via ditches	15.29	82	0.2	670	2.15	1.29
202	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via proposed grassed swale	10.43	72	0.2	380	1.62	0.97
203	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	12.75	72	0.2	380	1.62	0.97
204	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via proposed grassed swale	10.88	72	0.2	290	1.42	0.85
205	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	12.89	72	0.2	300	1.44	0.86
206	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via proposed grassed swale	4.78	72	0.1	200	1.48	0.89
207	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via proposed grassed swale	14.96	72	0.1	450	2.22	1.33
208	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via shallow surface flow	7.92	72	0.3	650	1.85	1.11
209	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	15.50	72	0.2	380	1.62	0.97
210	DESIGN NASHYD	Cropped land drainage to McGill Drain via shallow surface flow	7.27	82	0.3	350	1.36	0.82
211	DESIGN NASHYD	Cropped land drainage to McGill Drain via proposed grassed swale	14.49	82	0.3	600	1.78	1.07
212	DESIGN NASHYD	Proposed solar project drainage to Lappan Drain via proposed grassed swale	4.95	73	0.3	120	0.80	0.48
213	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	16.88	72	0.3	310	1.28	0.77
214	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	17.47	76	0.6	300	1.00	0.60
215	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via shallow surface flow	5.34	72	0.2	300	1.44	0.86
216	DESIGN NASHYD	Proposed solar project drainage to McGill Drain via proposed grassed swale	10.57	72	0.1	370	2.01	1.21
<b>Total</b>			<b>375.15</b>					

**Notes:**

Time of Concentration calculated using the Airport Method

$$T_c = [ 3.26 (1.1-C) L^{0.5} ] / S^{0.33}$$

Where:

C = Runoff Coefficient = 0.2 for undeveloped areas

L = Length of Overland Flow (m)

= (Area/1.5)<sup>0.5</sup>

S = Slope (%)

Time to Peak

$$T_p = 0.6T_c$$

1335-60106 - Windsor Solar Project  
 NRCS (SCS) Curve Number Determination  
 Existing Conditions

TABLE OF CURVE NUMBERS (CN's)									
Land Use		Hydrologic Soil Type						Source	
		A	AB	B	BC	C	CD		D
Meadow	"Good"	30	44	58	65	71	75	78	MTO
Woodlot	"Good"	25	40	55	63	70	74	77	MTO
Lawns	"Good"	39	50	61	68	74	77	80	USDA
Pasture/Range		58	62	65	71	76	79	81	MTO
Crop		66	70	74	78	82	84	86	MTO
Bare Soil (Fallow)		77	82	86	89	91	93	94	MTO
Wetland/Lake		50	50	50	50	50	50	50	MTO
Impervious		98	98	98	98	98	98	98	MTO

MTO - Ministry of Transportation Ontario Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers  
 USDA - United States Department of Agriculture (2004), National Engineering Handbook, Part 630 Hydrology, Chapter 9 Hydrologic Soil Cover Complexes

HYDROLOGIC SOIL TYPE (%) - Existing Conditions								
Catchment	Hydrologic Soil Type						TOTAL	
	A	AB	B	BC	C	CD		D
EXT1					100			100
EXT2					100			100
EXT3					100			100
104					100			100
105					100			100
105A					100			100
106					100			100
EXT4					100			100
107					100			100
108					100			100
109					100			100
110					100			100
EXT5					100			100
EXT6					100			100
113					100			100
114					100			100
EXT7					100			100

LAND USE (%) - Existing Conditions									
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Wetland	Impervious	Total
EXT1	94							6	100
EXT2					98			2	100
EXT3					97			3	100
104					99			1	100
105					99			1	100
105A					99			1	100
106					100				100
EXT4		18			81			1	100
107					99			1	100
108					98			2	100
109					99			1	100
110					98			2	100
EXT5					99			1	100
EXT6		19			80			1	100
113					98			2	100
114					98			2	100
EXT7					98			2	100

Note: Where STANDHYD command used (shaded), impervious fraction is not considered in CN determination, since %Imp directly input in STANDHYD command

CURVE NUMBER (CN) - Existing Conditions										
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Wetland/Lakes	Impervious	Weighted CN w/ imp area	Weighted CN w/o imp area
EXT1	67							6	73	71
EXT2					80			2	82	82
EXT3					80			3	82	82
104					81			1	82	82
105					81			1	82	82
105A					81			1	82	82
106					82				82	82
EXT4		13			66			1	80	80
107					81			1	82	82
108					80			2	82	82
109					81			1	82	82
110					80			2	82	82
EXT5					81			1	82	82
EXT6		13			66			1	80	80
113					80			2	82	82
114					80			2	82	82
EXT7					80			2	82	82

Notes:

AMC II assumed  
 Hydrological Soil Groups taken from MTO Drainage Manual



1335-60106 - Windsor Solar Project  
 NRCS (SCS) Curve Number Determination  
 Proposed Conditions

TABLE OF CURVE NUMBERS (CN's)									
Land Use		Hydrologic Soil Type						Source	
		A	AB	B	BC	C	CD		D
Meadow	"Good"	30	44	58	65	71	75	78	MTO
Woodlot	"Fair"	25	40	55	63	70	74	77	MTO
Lawns	"Good"	39	50	61	68	74	77	80	USDA
Pasture/Range		58	62	65	71	76	79	81	MTO
Crop		66	70	74	78	82	84	86	MTO
Bare Soil (Fallow)		77	82	86	89	91	93	94	MTO
Wetland/Lake		50	50	50	50	50	50	50	MTO
Impervious		98	98	98	98	98	98	98	MTO

MTO - Ministry of Transportation Ontario Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers  
 USDA - United States Department of Agriculture (2004), National Engineering Handbook, Part 630 Hydrology, Chapter 9 Hydrologic Soil Cover Complexes

HYDROLOGIC SOIL TYPE (%) - Proposed Conditions								
Catchment	Hydrologic Soil Type							TOTAL
	A	AB	B	BC	C	CD	D	
EXT1					100			100
EXT2					100			100
EXT3					100			100
EXT4					100			100
EXT5					100			100
EXT6					100			100
EXT7					100			100
EXT8					100			100
201					100			100
202					100			100
203					100			100
204					100			100
205					100			100
206					100			100
207					100			100
208					100			100
209					100			100
210					100			100
211					100			100
212					100			100
213					100			100
214					100			100
215					100			100
216					100			100

LAND USE (%) - Proposed Conditions									
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Wetland	Impervious	Total
EXT1	94							6	100
EXT2					98			2	100
EXT3					97			3	100
EXT4		18			81			1	100
EXT5					99			1	100
EXT6		19			80			1	100
EXT7					98			2	100
EXT8					98			2	100
201					99			1	100
202	98							2	100
203	98							2	100
204	98							2	100
205	97							3	100
206	98							2	100
207	98							2	100
208	98							2	100
209	97							3	100
210	5				92			3	100
211					98			2	100
212	93							7	100
213	97							3	100
214	67				23			10	100
215	98							2	100
216	97							3	100

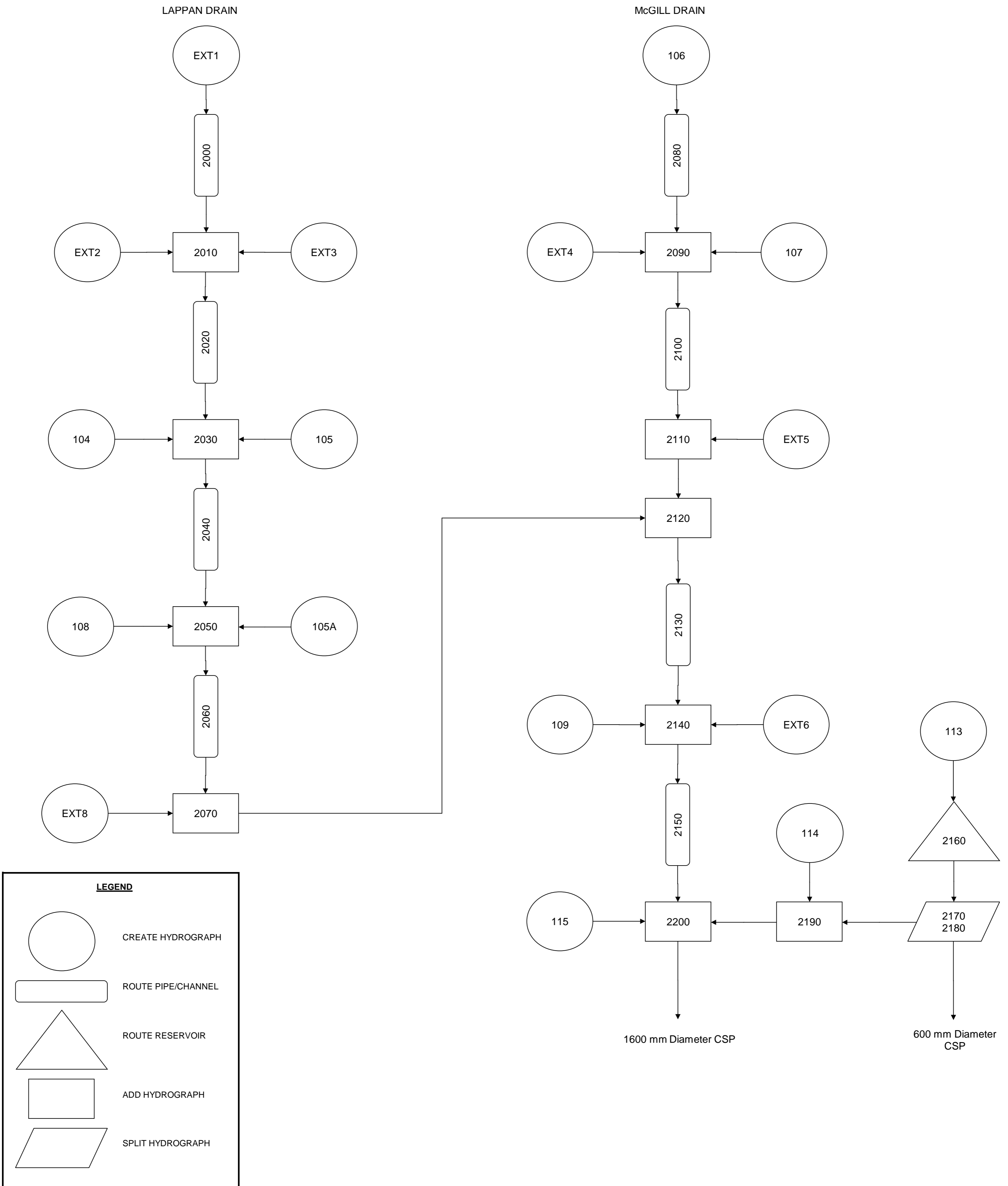
Note: Where STANDHYD command used (shaded), impervious fraction is not considered in CN determination, since %Imp directly input in STANDHYD command

CURVE NUMBER (CN) - Proposed Conditions										
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Wetland/Lakes	Impervious	Weighted CN w/ imp area	Weighted CN w/o imp area
EXT1	67							6	73	71
EXT2					80			2	82	82
EXT3					80			3	82	82
EXT4		13			66			1	80	80
EXT5					81			1	82	82
EXT6		13			66			1	80	80
EXT7					80			2	82	82
EXT8					80			2	82	82
201					81			1	82	82
202	70							2	72	71
203	70							2	72	71
204	70							2	72	71
205	69							3	72	71
206	70							2	72	71
207	70							2	72	71
208	70							2	72	71
209	69							3	72	71
210	4				75			3	82	81
211					80			2	82	82
212	66							7	73	71
213	69							3	72	71
214	48				19			10	76	74
215	70							2	72	71
216	69							3	72	71

Notes:

AMC II assumed  
 Hydrological Soil Groups taken from MTO Drainage Manual

Subject: Proposed Conditions SWMHYMO Schematic  
 Project: Windsor Solar Project  
 Project No.: 133560106  
 Client: Windsor Solar LP  
 Date: February 1, 2016







U.H. Tp(hrs)= 1.450

Unit Hyd Qpeak (cms)= .510

PEAK FLOW (cms)= .271 (i)

TIME TO PEAK (hrs)= 7.483

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0010-----

| DESIGN NASHYD | Area (ha)= 25.24 Curve Number (CN)=82.00

| 03:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

U.H. Tp(hrs)= 1.450

Unit Hyd Qpeak (cms)= .665

PEAK FLOW (cms)= .353 (i)

TIME TO PEAK (hrs)= 7.483

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0011-----

| ADD HYD ( 2030) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

----- (ha) (cms) (hrs) (mm) (cms)

ID1 01: 2020 107.59 1.188 7.93 17.74 .000

+ID2 02:104 19.36 .271 7.48 19.89 .000

+ID3 03:105 25.24 .353 7.48 19.89 .000

SUM 04: 2030 152.19 1.789 7.80 18.37 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0012-----

| ROUTE CHANNEL | Routing time step (min) = 1.00

| IN> 04:002030 | Number of SEGMENTS = 3

| OUT< 01:002060 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000

LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 3.0) ----->

Distance	Elevation	Manning
.00	2.20	.2000
200.00	1.80	.2000 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x V (m2/s)
.112	.112	.940E+02	.882E+01	.016	.087	95.91	.010
.225	.225	.187E+03	.389E+02	.054	.129	64.45	.029
.337	.337	.340E+03	.957E+02	.110	.161	51.67	.054
.450	.450	.492E+03	.185E+03	.185	.188	44.34	.085
.562	.562	.664E+03	.311E+03	.280	.211	39.43	.119
.675	.675	.854E+03	.481E+03	.397	.233	35.84	.157
.788	.788	.106E+04	.698E+03	.537	.252	33.06	.199
.900	.900	.129E+04	.970E+03	.700	.270	30.81	.243
1.013	1.013	.154E+04	.130E+04	.888	.288	28.95	.291
1.125	1.125	.181E+04	.170E+04	1.102	.304	27.37	.343
1.238	1.238	.210E+04	.216E+04	1.344	.320	26.01	.397
1.350	1.350	.240E+04	.271E+04	1.615	.336	24.81	.453
1.463	1.463	.272E+04	.333E+04	1.916	.351	23.76	.513
1.575	1.575	.308E+04	.404E+04	2.247	.365	22.82	.575
1.688	1.688	.344E+04	.484E+04	2.611	.379	21.97	.640
1.800	1.800	.382E+04	.574E+04	3.008	.393	21.19	.708
1.933	1.933	.424E+04	.674E+04	3.437	.407	20.52	.779
2.067	2.067	.470E+04	.788E+04	3.903	.422	19.94	.853
2.200	2.200	.520E+04	.920E+04	4.400	.437	19.44	.930

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.

S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4:002030 152.19	1.789	7.80	18.369	1.415	.344
OUTFLOW : ID= 1:002040 152.19	1.672	8.07	18.369	1.372	.339

002:0013-----

| DESIGN NASHYD | Area (ha)= 15.67 Curve Number (CN)=82.00

| 02:108 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

U.H. Tp(hrs)= 1.090

Unit Hyd Qpeak (cms)= .549

PEAK FLOW (cms)= .272 (i)

TIME TO PEAK (hrs)= 7.067

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0014-----

| DESIGN NASHYD | Area (ha)= 6.80 Curve Number (CN)=82.00

| 03:105A DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

U.H. Tp(hrs)= .960

Unit Hyd Qpeak (cms)= .271

PEAK FLOW (cms)= .130 (i)

TIME TO PEAK (hrs)= 6.917

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0015-----

| ADD HYD ( 2050) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

----- (ha) (cms) (hrs) (mm) (cms)

ID1 01: 2040 152.19 1.672 8.07 18.37 .000

+ID2 02:108 15.67 .272 7.07 19.89 .000

+ID3 03:105A 6.80 .130 6.92 19.89 .000

SUM 04: 2050 174.66 1.946 7.92 18.56 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0016-----

| ROUTE CHANNEL | Routing time step (min) = 1.00

| IN> 04:002050 | Number of SEGMENTS = 3

| OUT< 01:002060 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000

LENGTH = 450.00 (m)

<----- DATA FOR SECTION ( 4.0) ----->

Distance	Elevation	Manning
.00	2.20	.2000
200.00	1.80	.2000 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x V (m2/s)
.112	.112	.846E+02	.882E+01	.016	.087	86.32	.010
.225	.225	.187E+03	.389E+02	.054	.129	58.01	.029
.337	.337	.306E+03	.957E+02	.110	.161	46.50	.054
.450	.450	.443E+03	.185E+03	.185	.188	39.90	.085
.562	.562	.597E+03	.311E+03	.280	.211	35.49	.119
.675	.675	.769E+03	.481E+03	.397	.233	32.26	.157
.788	.788	.958E+03	.698E+03	.537	.252	29.75	.199
.900	.900	.116E+04	.970E+03	.700	.270	27.73	.243
1.013	1.013	.139E+04	.130E+04	.888	.288	26.06	.291
1.125	1.125	.163E+04	.170E+04	1.102	.304	24.63	.343
1.238	1.238	.192E+04	.216E+04	1.344	.320	23.41	.397
1.350	1.350	.216E+04	.271E+04	1.615	.336	22.33	.453
1.463	1.463	.246E+04	.333E+04	1.916	.351	21.38	.513
1.575	1.575	.277E+04	.404E+04	2.247	.365	20.53	.575
1.688	1.688	.310E+04	.484E+04	2.611	.379	19.77	.640
1.800	1.800	.344E+04	.574E+04	3.008	.393	19.07	.708
1.933	1.933	.382E+04	.674E+04	3.437	.407	18.43	.779
2.067	2.067	.424E+04	.788E+04	3.903	.422	17.84	.853
2.200	2.200	.470E+04	.920E+04	4.400	.437	17.30	.930

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.

S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4:002050 174.66	1.845	7.92	18.564	1.473	.347
OUTFLOW : ID= 1:002060 174.66	1.845	8.27	18.564	1.437	.347

002:0017-----

| DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00

| 02:EXTS DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

U.H. Tp(hrs)= .820

Unit Hyd Qpeak (cms)= .307

PEAK FLOW (cms)= .141 (i)

TIME TO PEAK (hrs)= 6.750

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0018-----

| ADD HYD ( 2070) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

----- (ha) (cms) (hrs) (mm) (cms)

ID1 01: 2060 174.66 1.845 8.27 18.56 .000

+ID2 02:EXTS 6.60 .141 6.75 19.89 .000

SUM 10: 2070 181.26 1.906 8.15 18.61 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0019-----

# MCGILL DRAIN

| DESIGN NASHYD | Area (ha)= 39.07 Curve Number (CN)=82.00

| 01:106 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

U.H. Tp(hrs)= 1.630

Unit Hyd Qpeak (cms)= .916

PEAK FLOW (cms)= .499 (i)

TIME TO PEAK (hrs)= 7.717

RUNOFF VOLUME (mm)= 19.890

TOTAL RAINFALL (mm)= 46.200

RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0020-----

| ROUTE CHANNEL | Routing time step (min) = 1.00

| IN> 01:106 | Number of SEGMENTS = 3

| OUT< 02:002080 | Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000

LENGTH = 250.00 (m)

<----- DATA FOR SECTION ( 5.0) ----->

Distance	Elevation	Manning
.00	1.40	.2000
200.00	1.00	.2000 / .1000 Main Channel
201.50	.00	.1000 Main Channel
205.00	1.00	.1000 / .2000 Main Channel
405.00	1.40	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x V (m2/s)
.071	.071	.376E+02	.358E+01	.010	.064	65.43	.005
.143	.143	.751E+02	.715E+01	.021	.097	47.56	.014
.214	.214	.124E+03	.355E+02	.061	.123	33.82	.026
.286	.286	.173E+03	.661E+02	.101	.145	28.74	.041
.357	.357	.226E+03	.108E+03	.148	.164	25.41	.059
.429	.429	.283E+03	.162E+03	.205	.181	23.02	.078
.500	.500	.344E+03	.229E+03	.270	.197	21.20	.098
.571	.571	.408E+03	.311E+03	.344	.211	19.75	.121
.643	.643	.476E+03	.408E+03	.428	.225	18.56	.144
.714	.714	.548E+03	.522E+03	.521	.237	17.56	.169
.786	.786	.624E+03	.654E+03	.623	.249	16.71	.196
.857	.857	.704E+03	.805E+03	.735	.261	15.96	.224
.929	.929	.788E+03	.975E+03	.858	.272	15.31	.253
1.000	1.000	.875E+03	.117E+04	.990	.283	14.73	.283
1.080	1.080	.974E+03	.142E+04	1.120	.297	14.20	.313
1.160	1.160	.107E+04	.172E+04	1.270	.313	13.73	.343
1.240	1.240	.118E+04	.208E+04	1.440	.328	13.33	.373
1.320	1.320	.130E+04	.248E+04	1.630	.343	13.00	.403
1.400	1.400	.144E+04	.292E+04	1.840	.357	12.73	.433

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for INFLOW and OUTFLOW at different IDs.

002:0021
DESIGN NASHYD | Area (ha)= 21.08 Curve Number (CN)=81.00
| 01:EXT4 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.830
Unit Hyd Qpeak (cms)= .440
PEAK FLOW (cms)= .237 (i)
TIME TO PEAK (hrs)= 7.967
RUNOFF VOLUME (mm)= 19.161
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .415
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0022
DESIGN NASHYD | Area (ha)= 6.53 Curve Number (CN)=82.00
| 03:107 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820
Unit Hyd Qpeak (cms)= .304
PEAK FLOW (cms)= .139 (i)
TIME TO PEAK (hrs)= 6.150
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0023
McGill Drain - Total Flow at Jefferson Boulevard
ADD HYD ( 2090 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01:EXT4 21.08 .237 7.97 19.16 .000
+ID2 02: 2080 39.07 .483 7.98 19.89 .000
+ID3 03:107 6.53 .139 6.75 19.89 .000
SUM 04: 2090 66.68 .795 7.82 19.66 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0024
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000
LENGTH = 280.00 (m)
DATA FOR SECTION ( 6.0 )
Distance Elevation Manning
200.00 1.00 .2000 / .1000 Main Channel
201.50 .00 .1000 Main Channel
203.50 .00 .1000 Main Channel
205.00 1.00 .1000 / .2000 Main Channel
405.00 1.40 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .421E+02 .179E+01 .014 .090 51.82 .006
.143 .143 .886E+02 .753E+01 .043 .138 33.94 .020
.214 .214 .139E+03 .178E+02 .087 .174 26.78 .037
.286 .286 .194E+03 .330E+02 .142 .205 22.76 .059
.357 .357 .254E+03 .539E+02 .210 .232 20.12 .083
.429 .429 .317E+03 .809E+02 .290 .256 18.23 .110
.500 .500 .385E+03 .115E+03 .382 .278 16.79 .139
.571 .571 .457E+03 .155E+03 .487 .298 15.64 .171
.643 .643 .534E+03 .204E+03 .605 .318 14.70 .204
.714 .714 .614E+03 .261E+03 .736 .336 13.91 .240
.786 .786 .699E+03 .327E+03 .881 .353 13.23 .277
.857 .857 .789E+03 .402E+03\* 1.040 .369 12.64 .316
.929 .929 .882E+03 .488E+03\* 1.213 .385 12.12 .357
1.000 1.000 .980E+03 .583E+03\* 1.401 .400 11.66 .400
1.080 1.080 .109E+04 .682E+03\* 1.761 .248 18.81 .268
1.160 1.160 .128E+04 .792E+04\* 2.505 .147 31.85 .170
1.240 1.240 .148E+04 .892E+04\* 3.856 .115 40.54 .143
1.320 1.320 .168E+05 .124E+05\* 5.997 .107 43.81 .141
1.400 1.400 .188E+05 .149E+05\* 9.093 .106 43.88 .149

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for INFLOW and OUTFLOW at different IDs.

002:0025
DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00
| 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .372
PEAK FLOW (cms)= .200 (i)
TIME TO PEAK (hrs)= 7.567
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0026
ADD HYD ( 2110 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2100 66.68 .785 7.98 19.66 .000
+ID2 02:EXT5 14.81 .200 7.57 19.89 .000
SUM 03: 2110 81.49 .978 7.87 19.70 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0027
DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00
| 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .372
PEAK FLOW (cms)= .200 (i)
TIME TO PEAK (hrs)= 7.567
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

McGill Drain - Total Flow at Lappan Drain Confluence

Table with columns: ADD HYD ( 2120 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF. Rows for ID1, ID2, and SUM.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0028
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:002120 | Number of SEGMENTS = 3
| OUT< 02:002130 | Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000
LENGTH = 370.00 (m)

DATA FOR SECTION ( 7.0 )
Distance Elevation Manning
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.093 .093 .681E+02 .573E+01 .016 .087 70.58 .008
.187 .187 .142E+03 .249E+02 .053 .131 46.93 .025
.280 .280 .240E+03 .606E+02 .107 .165 37.37 .046
.373 .373 .344E+03 .116E+03 .180 .193 31.94 .072
.467 .467 .460E+03 .194E+03 .271 .218 28.33 .102
.560 .560 .588E+03 .297E+03\* .382 .240 25.70 .134
.653 .653 .728E+03 .429E+03\* .513 .260 23.68 .170
.747 .747 .880E+03 .592E+03\* .665 .280 22.05 .209
.840 .840 .104E+04 .790E+03\* .840 .298 20.71 .250
.933 .933 .122E+04 .103E+04\* .1.039 .315 19.58 .294
1.027 1.027 .141E+04 .130E+04\* 1.262 .332 18.60 .340
1.120 1.120 .161E+04 .162E+04\* 1.510 .348 17.74 .389
1.213 1.213 .182E+04 .199E+04\* 1.785 .363 16.99 .440
1.307 1.307 .204E+04 .241E+04\* 2.087 .378 16.32 .494
1.400 1.400 .228E+04 .287E+04\* 2.418 .392 15.71 .549
1.500 1.500 .439E+04 .593E+04\* 3.044 .257 24.02 .385
1.600 1.600 .102E+05 .147E+05\* 4.365 .158 38.94 .253
1.700 1.700 .197E+05 .302E+05\* 6.783 .127 48.42 .217
1.800 1.800 .329E+05 .534E+05\* 10.633 .120 51.59 .215

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for INFLOW and OUTFLOW at different IDs.

002:0029
DESIGN NASHYD | Area (ha)= 47.17 Curve Number (CN)=82.00
| 03:109 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.100
Unit Hyd Qpeak (cms)= 1.638
PEAK FLOW (cms)= .812 (i)
TIME TO PEAK (hrs)= 7.083
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0030
DESIGN NASHYD | Area (ha)= 24.11 Curve Number (CN)=80.00
| 04:EXT6 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .606
PEAK FLOW (cms)= .300 (i)
TIME TO PEAK (hrs)= 7.583
RUNOFF VOLUME (mm)= 18.467
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .400
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0031
ADD HYD ( 2140 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 02: 2130 262.75 2.742 8.77 18.95 .000
+ID2 03:109 47.17 .812 7.08 19.89 .000
+ID3 04:EXT6 24.11 .300 7.58 18.47 .000
SUM 01: 2140 334.03 3.439 8.33 19.05 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0032
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:002140 | Number of SEGMENTS = 3
| OUT< 10:002150 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000
LENGTH = 370.00 (m)
DATA FOR SECTION ( 7.0 )
Distance Elevation Manning
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.093 .093 .681E+02 .107E+02 .012 .064 96.65 .006
.187 .187 .142E+03 .467E+02 .038 .096 64.26 .018
.280 .280 .240E+03 .114E+03 .078 .121 51.18 .034
.373 .373 .344E+03 .217E+03\* .131 .141 43.73 .053
.467 .467 .460E+03 .363E+03\* .198 .159 38.79 .074
.560 .560 .588E+03 .557E+03\* .279 .175 35.19 .098
.653 .653 .728E+03 .804E+03\* .374 .190 32.42 .124
.747 .747 .880E+03 .111E+04\* .486 .204 30.20 .152
.840 .840 .104E+04 .148E+04\* .614 .217 28.36 .183
.933 .933 .122E+04 .192E+04\* .759 .230 26.61 .215
1.027 1.027 .141E+04 .244E+04\* .921 .242 25.47 .249
1.120 1.120 .161E+04 .304E+04\* 1.103 .254 24.30 .284

# Windsor Solar Energy Project

# Existing Conditions SWMHYMO

1.213	1.213	.182E+04	.373E+04*	1.304	.265	23.27	.322
1.307	1.307	.204E+04	.451E+04*	1.524	.276	22.34	.361
1.400	1.400	.228E+04	.539E+04*	1.766	.287	21.51	.401
1.500	1.500	.439E+04	.111E+05*	2.264	.191	32.30	.286
1.600	1.600	.102E+05	.276E+05*	3.447	.125	49.30	.200
1.700	1.700	.197E+05	.566E+05*	5.720	.107	57.42	.183
1.800	1.800	.329E+05	.100E+06*	9.415	.106	58.27	.191

ID1 01:115	18.59	.257	7.52	19.89	.000
+ID2 02:	2190	21.71	.413	6.87	19.89
+ID3 03:	2150	334.03	3.075	9.43	19.05
SUM 05:	2200	374.33	3.358	9.18	19.14

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

		<--- hydrograph --->		<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH
	(ha)	(cms)	(hrs)	(mm)	(m)
INFLOW : ID= 1:002140	334.03	3.439	8.33	19.048	1.599
OUTFLOW: ID=10:002150	334.03	3.075	9.43	19.048	1.568
					MAX VEL
					(m/s)

```

002:0040-----
| DESIGN NASHYD | Area (ha)= 17.65 | Curve Number (CN)=82.00
| 01:113 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
+-----+
Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= .350 (l)
TIME TO PEAK (hrs)= 6.867
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0033-----
| DESIGN NASHYD | Area (ha)= 17.65 | Curve Number (CN)=82.00
| 01:113 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
+-----+
Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= .350 (l)
TIME TO PEAK (hrs)= 6.867
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0041-----
** END OF RUN : 4
    
```

```

002:0034-----
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| INID=01 (113 ) |
| OUF=02 (002160) |
+-----+
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .000E+00 | 1.130 .4600E+00
.150 .000E+00 | 5.470 .8100E+00
.450 .000E+00 | 83.090 .3400E+01
.820 .6500E-01 | .000 .0000E+00
    
```

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW >01: (113 )	17.65	.350	6.867	19.890
OUTFLOW<02: (002160)	17.65	.350	6.867	19.890

PEAK FLOW REDUCTION [Qout/Qin] (%) = 100.000  
 TIME SHIFT OF PEAK FLOW (min) = .00  
 MAXIMUM STORAGE USED (ha.m.) = .2593E-08

\*\*\* WARNING: Inflow peak was not reduced!  
 Check OUTFLOW/STORAGE table or reduce DT.

```

002:0035-----
| DIVERT HYD |
| INID=02 (002160) |
+-----+
Outflow / Inflow Relationships
Flow 03 + Flow 04 = Total
(cms) (cms) (cms)
.000 .000 .000
.150 .000 .150
.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090
    
```

	NHYD	AREA	QPEAK	TpeakDate	hh:mm	R.V.	NFE	Wetlres
	(ha)	(cms)	(hrs)			(mm)		(hrs)
IDin = 02:002160	17.65	.350	No_date	6:52	19.890	1	15.	
IDout= 03:002170	16.83	.316	No_date	6:52	19.890	1	15.	
IDout= 04:002180	.82	.033	No_date	6:52	19.890	1	2.	

```

002:0036-----
| DESIGN NASHYD | Area (ha)= 4.88 | Curve Number (CN)=82.00
| 01:114 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
+-----+
Unit Hyd Qpeak (cms)= .205
PEAK FLOW (cms)= .097 (l)
TIME TO PEAK (hrs)= 6.867
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0037-----
| ADD HYD ( 2190 ) | ID: NHYD | AREA QPEAK TPEAK R.V. DWF
| 01:114 | 4.88 .097 6.87 19.89 .000
| +ID2 03: 2170 | 16.83 .316 6.87 19.89 .000
| SUM 02: 2190 | 21.71 .413 6.87 19.89 .000
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0038-----
| DESIGN NASHYD | Area (ha)= 18.59 | Curve Number (CN)=82.00
| 01:115 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.470
+-----+
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .257 (l)
TIME TO PEAK (hrs)= 7.517
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0039-----
| ADD HYD ( 2200 ) | ID: NHYD | AREA QPEAK TPEAK R.V. DWF
| 01:115 | 18.59 .257 7.52 19.89 .000
| +ID2 03: 2150 | 334.03 3.075 9.43 19.05 .000
| SUM 01: 2210 | 375.15 3.358 9.18 19.14 .000
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0040-----
| DESIGN NASHYD | Area (ha)= 17.65 | Curve Number (CN)=82.00
| 01:113 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
+-----+
Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= .350 (l)
TIME TO PEAK (hrs)= 6.867
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0041-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:101 | Number of SEGMENTS = 3
| OUF< 02:002000 | Slopes (%), CHANNEL .1000 FLOODPLAIN= 2000
| LENGTH = 700.00 (m)
+-----+
<--- DATA FOR SECTION ( 1.0 ) --->
Distance Elevation Manning
.00 .00 1.40
100.00 1.20 .2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 .2000
    
```

```

| START | Project dir.: F:\WSP\
| Rainfall dir.: F:\WSP\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 005
NSTORM= 1
# l=12scs5.stm
    
```

```

005:0002-----
# Project Name: [Windsor Solar Project] Project Number: [1335-60106]
# Date : 02-02-2016
# Modeller : [NE]
# Company : Stantec Consulting Ltd. (London)
# License # : 4730904
# Existing Conditions
# 25 mm Water Quality Event
# 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
    
```

```

005:0002-----
| READ STORM | Filename: 5-yr scs 12 hr windsor
| Ptotal= 60.10 mm | Comments: 5-yr scs 12 hr windsor
+-----+
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.202 | 3.50 2.404 | 6.50 10.818 | 9.50 2.404
1.00 1.202 | 4.00 2.404 | 7.00 4.808 | 10.00 1.202
1.50 1.202 | 4.50 3.606 | 7.50 3.606 | 10.50 1.202
2.00 1.202 | 5.00 4.808 | 8.00 3.606 | 11.00 1.202
2.50 2.404 | 5.50 7.212 | 8.50 2.404 | 11.50 1.202
3.00 2.404 | 6.00 54.090 | 9.00 2.404 | 12.00 1.202
    
```

```

005:0003-----
# LAPPAN DRAIN
    
```

```

| DESIGN NASHYD | Area (ha)= 42.26 | Curve Number (CN)=73.00
| 01:101 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110
    
```

	Unit Hyd Qpeak	(cms)	= 1.454
	PEAK FLOW	(cms)	= .810 (l)
	TIME TO PEAK	(hrs)	= 7.101
	RUNOFF VOLUME	(mm)	= 22.511
	TOTAL RAINFALL	(mm)	= 60.100
	RUNOFF COEFFICIENT		= .375

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0004-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:101 | Number of SEGMENTS = 3
| OUF< 02:002000 | Slopes (%), CHANNEL .1000 FLOODPLAIN= 2000
| LENGTH = 700.00 (m)
+-----+
<--- DATA FOR SECTION ( 1.0 ) --->
Distance Elevation Manning
.00 .00 1.40
100.00 1.20 .2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 .2000
    
```

```

<--- TRAVEL TIME TABLE --->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .645E+02 .325E+01 .005 .059 197.27 .004
.141 .141 .140E+03 .141E+02 .018 .089 131.37 .013
.212 .212 .225E+03 .340E+02 .036 .111 104.80 .024
.282 .282 .321E+03 .647E+02 .060 .130 89.71 .037
.353 .353 .427E+03 .108E+03 .089 .146 79.68 .052
.424 .424 .548E+03 .165E+03 .125 .161 72.40 .068
.494 .494 .671E+03 .237E+03 .168 .175 66.79 .086
.565 .565 .809E+03 .326E+03 .217 .187 62.29 .106
.635 .635 .957E+03 .434E+03 .272 .199 58.56 .127
.706 .706 .112E+04 .563E+03 .336 .211 55.41 .149
.776 .776 .129E+04 .713E+03 .407 .221 52.69 .172
.847 .847 .146E+04 .886E+03 .485 .232 50.32 .196
.918 .918 .166E+04 .108E+04 .572 .242 48.22 .222
.988 .988 .186E+04 .131E+04 .667 .252 46.35 .249
1.059 1.059 .207E+04 .156E+04 .771 .261 44.66 .277
1.129 1.129 .229E+04 .185E+04 .884 .271 43.13 .306
1.200 1.200 .252E+04 .216E+04 .1006 .280 41.73 .335
1.306 1.306 .326E+04 .590E+04 .1392 .353 36.12 .499
1.400 1.400 .172E+05 .172E+05 .2456 .100 116.67 .140
    
```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

002:0039-----
| DESIGN NASHYD | Area (ha)= 18.59 | Curve Number (CN)=82.00
| 01:115 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.470
+-----+
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .257 (l)
TIME TO PEAK (hrs)= 7.517
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
    
```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0039-----
| McGill Drain - Total Flow at Eastern WSP
+-----+
| ADD HYD ( 2200 ) | ID: NHYD | AREA QPEAK TPEAK R.V. DWF
| 01:115 | 18.59 .257 7.52 19.89 .000
| +ID2 03: 2150 | 334.03 3.075 9.43 19.05 .000
| SUM 01: 2210 | 375.15 3.358 9.18 19.14 .000
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.





2.200 2.200 .407E+05 .829E+05\* 11.177 .124 60.70 .272
X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

TIME TO PEAK (hrs)= 6.751
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes data for INFLOW and OUTFLOW.

005:0023-----
# McGill Drain - Total Flow at Jefferson Boulevard

Table with columns: ADD HYD ( 2090 ) | ID: NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes data for ID1, ID2, ID3 and a summary row.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with columns: ROUTE CHANNEL, Routing time step (min) = 1.00, Number of SEGMENTS = 3, Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000, LENGTH = 280.00 (m)

<----- DATA FOR SECTION ( 6.0 ) ----->

Table with columns: Distance, Elevation, Manning. Includes data for various elevations and Manning coefficients.

<----- TRAVEL TIME TABLE ----->

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Includes a detailed data table for travel time.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

005:0017-----
| DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00
| 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .820
Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .215 (1)
TIME TO PEAK (hrs)= 6.751
RUNOFF VOLUME (mm)= 30.028
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0018-----
# Lappan Drain - Total Flow at McGill Drain
| ADD HYD ( 2070 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
+ID2 01: 2060 174.66 2.955 8.20 28.21 .000
+ID2 02:EXT8 6.60 .215 6.75 30.03 .000
SUM 10: 2070 181.26 3.044 8.13 28.28 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0019-----
# MCGILL DRAIN
| DESIGN NASHYD | Area (ha)= 39.07 Curve Number (CN)=82.00
| 01:106 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.630
Unit Hyd Qpeak (cms)= .916
PEAK FLOW (cms)= .760 (1)
TIME TO PEAK (hrs)= 7.684
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0020-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 01:106 | Number of SEGMENTS = 3
| OUT< 02:002080 | Slopes (%), CHANNEL= 1.500 FLOODPLAIN= .2000
| LENGTH = 250.00 (m)
<----- DATA FOR SECTION ( 5.0 ) ----->
Distance Elevation Manning
200.00 1.00 .2000 / .1000 Main Channel
201.50 .00 .1000 Main Channel
203.50 .00 .1000 Main Channel
205.00 1.00 .1000 / .2000 Main Channel
405.00 1.40 .2000

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Includes a detailed data table for travel time.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes data for INFLOW and OUTFLOW.

Table with columns: ADD HYD ( 2090 ) | ID: NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes data for ID1, ID2, ID3 and a summary row.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0025-----
| DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00
| 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .372
PEAK FLOW (cms)= .304 (1)
TIME TO PEAK (hrs)= 7.551
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0026-----
| ADD HYD ( 2110 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2100 66.68 1.203 7.90 29.72 .000
+ID2 02:EXT5 14.81 .304 7.55 30.03 .000
SUM 03: 2110 81.49 1.500 7.82 29.78 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0027-----
# McGill Drain - Total Flow at Lappan Drain Confluence
| ADD HYD ( 2120 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 03: 2110 81.49 1.500 7.82 29.78 .000
ID2 10: 2070 181.26 3.044 8.13 28.28 .000
SUM 01: 2120 262.75 4.517 8.13 28.74 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0021-----
| DESIGN NASHYD | Area (ha)= 21.08 Curve Number (CN)=81.00
| 01:EXT4 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.830
Unit Hyd Qpeak (cms)= .440
PEAK FLOW (cms)= .362 (1)
TIME TO PEAK (hrs)= 7.934
RUNOFF VOLUME (mm)= 29.057
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .483
(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0028-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 01:002120 | Number of SEGMENTS = 3
| OUT< 02:002130 | Slopes (%), CHANNEL= 1.500 FLOODPLAIN= .2000
| LENGTH = 370.00 (m)
<----- DATA FOR SECTION ( 7.0 ) ----->
Distance Elevation Manning
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

005:0022-----
| DESIGN NASHYD | Area (ha)= 6.53 Curve Number (CN)=82.00
| 03:107 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .820
Unit Hyd Qpeak (cms)= .304
PEAK FLOW (cms)= .212 (1)

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Includes a detailed data table for travel time.

Table with 10 columns of numerical data, likely representing flow or volume measurements at various points.

X-VOLUME = Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME = Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 10 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

005:0029-----
DESIGN NASHYD | Area (ha)= 47.17 Curve Number (CN)=82.00
| 03:109 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.100
Unit Hyd Qpeak (cms)= 1.638
PEAK FLOW (cms)= 1.237 (i)
TIME TO PEAK (hrs)= 7.068
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0030-----
DESIGN NASHYD | Area (ha)= 24.11 Curve Number (CN)=80.00
| 04:EXTA DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .606
PEAK FLOW (cms)= .461 (i)
TIME TO PEAK (hrs)= 7.568
RUNOFF VOLUME (mm)= 28.124
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .468
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0031-----
ADD HYD ( 2140) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 02: 2130 262.75 4.033 8.95 28.74 .000
+ID2 03:109 47.17 1.237 7.07 30.03 .000
+ID3 04:EXTA 24.11 .461 7.57 28.12 .000
SUM 01: 2140 334.03 4.960 8.53 28.88 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0032-----
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:002140 | Number of SEGMENTS = 3
| OUT< 10:002150 | Slopes (%), CHANNEL= .0800 FLOODPLAIN=.2000
LENGTH = 370.00 (m)
<----- DATA FOR SECTION ( 7.0) ----->
Distance Elevation Manning
1.80 .2000
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Includes a large data table with 10 columns.

X-VOLUME = Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME = Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 10 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

005:0033-----
DESIGN NASHYD | Area (ha)= 17.65 Curve Number (CN)=82.00
| 01:113 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= .533 (i)
TIME TO PEAK (hrs)= 6.851
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0034-----

\*\*\*\*\*
# Calculate culvert routing and flow split near eastern site boundary
# Storage volumes calculated based on site survey
# Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities
\*\*\*\*\*
ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>01:(113 ) |
| OUT<02:(002160) |
OUTFLOW STORAGE TABLE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | 1.130 .4600E+00
.150 .0000E+00 | 5.470 .8100E+00
.450 .0000E+00 | 83.090 .3400E+01
.820 .6500E-01 | .000 .0000E+00

ROUTING RESULTS table with columns: AREA, QPEAK, TPEAK, R.V. Includes INFLOW and OUTFLOW data.

005:0035-----
DIVERST HYD |
| INID=02 (002160) |
Outflow / Inflow Relationships
Flow 03 + Flow 04 = Total
(cms) (cms) (cms)
.000 .000 .000
.150 .000 .150
.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090

Table with 10 columns: NHYD, AREA, QPEAK, TpeakDate, R.V., NFE, WetHrs. Includes IDin, IDout, IDout data.

005:0036-----
DESIGN NASHYD | Area (ha)= 4.88 Curve Number (CN)=82.00
| 01:114 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .910
Unit Hyd Qpeak (cms)= .205
PEAK FLOW (cms)= .147 (i)
TIME TO PEAK (hrs)= 6.851
RUNOFF VOLUME (mm)= 30.028
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0037-----
ADD HYD ( 2190) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:114 4.88 .147 6.85 30.03 .000
+ID2 03: 2170 16.36 .439 7.15 30.03 .000
SUM 02: 2190 21.24 .580 7.03 30.03 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0038-----
DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
| 01:115 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.470
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .391 (i)
TIME TO PEAK (hrs)= 7.484
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0039-----
# McGill Drain - Total Flow at Eastern WSP
\*\*\*\*\*
ADD HYD ( 2200) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:115 18.59 .391 7.48 30.03 .000
+ID2 02: 2190 21.24 .580 7.03 30.03 .000
+ID3 10: 2150 334.03 4.438 9.62 28.88 .000
SUM 05: 2200 373.86 4.835 9.30 29.00 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0040-----
# AREA CHECK
\*\*\*\*\*
ADD HYD ( 2210) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 04: 2180 1.29 .062 7.15 30.03 .000
+ID2 05: 2200 373.86 4.835 9.30 29.00 .000
SUM 01: 2210 375.15 4.836 9.30 29.00 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0041-----
005:0002-----
\*\* END OF RUN : 9

START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
TRENO = .00 hrs on 0
METOUT= 2 (output = METRIC)



Windsor Solar Energy Project

Existing Conditions SWMHYMO

```

NRUN = 010
NSTORM= 1
# I=12accs10.stm
-----
010:0002-----
*****
# Project Name: [Windsor Solar Project] Project Number: [1335-60106]
# Date : 02-02-2016
# Modeller : [ME]
# Company : Stantec Consulting Ltd. (London)
# License # : 4730904
*****
# Existing Conditions
# 25 mm Water Quality Event
# 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
#
*****
010:0002-----
| READ STORM | Filename: 10-yr scs 12 hr windsor
| Pictal= 69.20 mm | Comments: 10-yr scs 12 hr windsor
-----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 1.384 | 3.50 2.768 | 7.00 5.536 | 10.00 1.384
1.50 1.384 | 4.50 4.152 | 7.50 4.152 | 10.50 1.384
2.00 1.384 | 5.00 5.536 | 8.00 4.152 | 11.00 1.384
2.50 2.768 | 5.50 8.304 | 8.50 2.768 | 11.50 1.384
3.00 2.768 | 6.00 6.280 | 9.00 2.768 | 12.00 1.384
-----
010:0003-----
# LAPPAN DRAIN
*****
| DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
| 01:101 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110
-----
Unit Hyd Qpeak (cms)= 1.454
PEAK FLOW (cms)= 1.025 (i)
TIME TO PEAK (hrs)= 7.101
RUNOFF VOLUME (mm)= 28.354
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .410
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
010:0004-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN= 01:101 | Number of SEGMENTS = 3
| OUT= 02:002000 | Slopes (%), CHANNEL= 1000 FLOODPLAIN= .2000
| LENGTH = 700.00 (m)
-----
<----- DATA FOR SECTION ( 1.0 ) ----->
Distance Elevation Manning
100.00 1.20 .2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 .00 .2000
-----
<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .645E+02 .325E+01 .005 .059 197.27 .004
.141 .141 .140E+03 .141E+02 .018 .089 131.37 .013
.212 .212 .225E+03 .237E+02 .036 .111 104.80 .024
.282 .282 .321E+03 .647E+02 .060 .130 89.71 .037
.353 .353 .427E+03 .108E+03 .089 .146 79.68 .052
.424 .424 .544E+03 .165E+03 .125 .161 72.40 .068
.494 .494 .671E+03 .237E+03 .168 .175 66.79 .086
.565 .565 .809E+03 .326E+03 .217 .187 62.29 .106
.635 .635 .957E+03 .434E+03 .272 .199 58.56 .127
.706 .706 .112E+04 .563E+03* .336 .211 55.41 .149
.776 .776 .129E+04 .713E+03* .407 .221 52.69 .172
.847 .847 .146E+04 .886E+03* .485 .232 50.32 .196
.918 .918 .166E+04 .108E+04* .572 .242 48.22 .222
.988 .988 .186E+04 .131E+04* .667 .252 46.35 .249
1.059 1.059 .207E+04 .156E+04* .771 .261 44.66 .277
1.129 1.129 .229E+04 .185E+04* .884 .271 43.13 .306
1.200 1.200 .252E+04 .216E+04* 1.006 .280 41.73 .335
1.300 1.300 .636E+04 .590E+04* 1.392 .153 76.12 .199
1.400 1.400 .172E+05 .172E+05* 2.456 .100 116.67 .140
-----
X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.
-----
010:0005-----
| DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00
| 01:102 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.270
-----
Unit Hyd Qpeak (cms)= .677
PEAK FLOW (cms)= .658 (i)
TIME TO PEAK (hrs)= 7.251
RUNOFF VOLUME (mm)= 37.125
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .536
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
010:0006-----
| DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110
-----
Unit Hyd Qpeak (cms)= 1.473
PEAK FLOW (cms)= 1.385 (i)
TIME TO PEAK (hrs)= 7.068
RUNOFF VOLUME (mm)= 37.125
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .536
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
010:0007-----
# Lappan Drain - Total Flow at Pilette Road
*****

```

```

| ADD HYD ( 2010 ) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:102 22.52 .658 7.25 37.12 .000
+ID2 02: 2000 42.26 .829 7.53 28.35 .000
+ID3 03:103 42.81 1.385 7.07 37.12 .000
SUM 04: 2010 107.59 2.808 7.28 33.68 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
-----
010:0008-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN= 04:002010 | Number of SEGMENTS = 3
| OUT= 01:002020 | Slopes (%), CHANNEL= 1.700 FLOODPLAIN= .2000
| LENGTH = 1000.00 (m)
-----
<----- DATA FOR SECTION ( 2.0 ) ----->
Distance Elevation Manning
100.00 2.00 .2000
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .2000 Main Channel
207.00 2.00 .2000
-----
<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .165E+03 486E+01 .016 .096 172.86 .010
.200 .200 .361E+03 212E+02 .052 .144 115.66 .029
.300 .300 .588E+03 518E+02 .106 .180 92.51 .054
.400 .400 .844E+03 938E+02 .177 .210 79.29 .084
.500 .500 .113E+04 1.66E+03 .268 .236 70.48 .118
.600 .600 .145E+04 2.56E+03 .377 .260 64.05 .156
.700 .700 .180E+04 3.70E+03 .507 .282 59.09 .197
.800 .800 .218E+04 5.12E+03 .659 .303 55.09 .242
.900 .900 .259E+04 6.85E+03 .833 .322 51.78 .290
1.000 1.000 .303E+04 8.91E+03 1.031 .340 48.97 .340
1.100 1.100 .350E+04 1.13E+04 1.253 .358 46.55 .394
1.200 1.200 .400E+04 1.41E+04 1.500 .375 44.43 .450
1.300 1.300 .453E+04 1.73E+04 1.775 .392 42.56 .509
1.400 1.400 .509E+04 2.10E+04 2.077 .408 40.88 .571
1.500 1.500 .569E+04 2.51E+04 2.407 .423 39.37 .635
1.600 1.600 .631E+04 2.97E+04 2.768 .439 38.01 .702
1.700 1.700 .697E+04 3.48E+04 3.158 .453 36.76 .771
1.800 1.800 .765E+04 4.05E+04* 3.580 .468 35.61 .842
2.000 2.000 .291E+05 .171E+05* 5.701 .196 84.93 .392
-----
X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.
-----
<----- hydrograph -----> <-pipe / channel->
AREA OPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002010 107.59 2.808 7.28 33.680 1.610 .440
OUTFLOW : ID= 1:002020 107.59 2.397 7.78 33.680 1.494 .422
-----
010:0009-----
| DESIGN NASHYD | Area (ha)= 19.36 Curve Number (CN)=82.00
| 02:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.450
-----
Unit Hyd Qpeak (cms)= .510
PEAK FLOW (cms)= .511 (i)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 37.125
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .536
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
010:0010-----
| DESIGN NASHYD | Area (ha)= 25.24 Curve Number (CN)=82.00
| 03:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.450
-----
Unit Hyd Qpeak (cms)= .665
PEAK FLOW (cms)= .667 (i)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 37.125
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .536
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
010:0011-----
| ADD HYD ( 2030 ) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01: 2020 107.59 2.397 7.78 33.68 .000
+ID2 02:104 19.36 .511 7.45 37.12 .000
+ID3 03:105 25.24 .667 7.45 37.12 .000
SUM 04: 2030 152.19 3.549 7.67 34.69 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
-----
010:0012-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN= 04:002030 | Number of SEGMENTS = 3
| OUT= 01:002040 | Slopes (%), CHANNEL= 1.200 FLOODPLAIN= .2000
| LENGTH = 500.00 (m)
-----
<----- DATA FOR SECTION ( 3.0 ) ----->
Distance Elevation Manning
100.00 2.20 .2000
200.00 1.80 .2000 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .2000 Main Channel
407.00 2.20 .2000
-----
<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .940E+02 882E+01 .016 .087 95.91 .010
.225 .225 .207E+03 3.89E+02 .054 .129 64.45 .029
.337 .337 .340E+03 9.57E+02 .110 .161 51.67 .054
.450 .450 .492E+03 1.85E+03 .185 .188 44.34 .085
.562 .562 .664E+03 3.11E+03 .280 .211 39.43 .119
.675 .675 .854E+03 4.81E+03* .397 .233 35.84 .157
.788 .788 .106E+04 6.98E+03* .537 .252 33.06 .199
.900 .900 .129E+04 9.70E+03* .700 .270 30.81 .243
1.013 1.013 .154E+04 1.30E+04* .898 .288 28.95 .291
1.125 1.125 .181E+04 1.70E+04* 1.102 .304 27.37 .343
1.238 1.238 .210E+04 2.16E+04* 1.344 .320 26.01 .397
1.350 1.350 .240E+04 2.71E+04* 1.615 .336 24.81 .453
1.463 1.463 .273E+04 3.33E+04* 1.916 .351 23.76 .513
1.575 1.575 .308E+04 4.04E+04* 2.247 .365 22.82 .575

```

1.688	1.688	.344E+04	.484E+04*	2.611	.379	21.97	.640
1.800	1.800	.382E+04	.574E+04*	3.008	.393	21.19	.708
1.933	1.933	.474E+04	.141E+05*	3.971	.227	36.67	.439
2.067	2.067	.225E+05	.388E+05*	6.403	.142	58.66	.294
2.200	2.200	.452E+05	.829E+05*	11.177	.124	67.44	.272

ID1 01:	2060	174.66	3.503	8.77	35.00	.000
+ID2 02:EXTS		6.60	.267	6.73	37.12	.000
SUM 10:	2070	181.26	3.576	8.77	35.08	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4:002030	152.19	3.549	7.67	34.689	1.875	.279
OUTFLOW: ID= 1:002040	152.19	3.293	8.55	34.689	1.840	.322

010:0019-----  
 #\*\*\*\*\*  
 # McGill Drain  
 #\*\*\*\*\*

DESIGN NASHYD	Area (ha)	39.07	Curve Number (CN)=82.00
01:106 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.630	

Unit Hyd Qpeak (cms)	= .916
PEAK FLOW (cms)	= .943 (i)
TIME TO PEAK (hrs)	= 7.668
RUNOFF VOLUME (mm)	= 37.125
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0013-----

DESIGN NASHYD	Area (ha)	15.67	Curve Number (CN)=82.00
02:108 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.090	

Unit Hyd Qpeak (cms)	= .549
PEAK FLOW (cms)	= .514 (i)
TIME TO PEAK (hrs)	= 7.051
RUNOFF VOLUME (mm)	= 37.125
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0014-----

DESIGN NASHYD	Area (ha)	6.80	Curve Number (CN)=82.00
03:105A DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	.960	

Unit Hyd Qpeak (cms)	= .271
PEAK FLOW (cms)	= .245 (i)
TIME TO PEAK (hrs)	= 6.901
RUNOFF VOLUME (mm)	= 37.125
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0015-----

*# Lappan Drain - Total Flow at Jefferson Boulevard						
ADD HYD ( 2050)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)

ID1 01:	2040	152.19	3.293	8.55	34.69	.000
+ID2 02:108		15.67	.514	7.05	37.12	.000
+ID3 03:105A		6.80	.245	6.90	37.12	.000
SUM 04:	2050	174.66	3.725	8.22	35.00	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0016-----

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN< 04:002050	Number of SEGMENTS	= 3
OUT< 01:002060	Slopes (%), CHANNEL= 1.200 FLOODPLAIN= .2000	
	LENGTH = 450.00 (m)	

Distance	Elevation	Manning
.00	2.20	.2000
200.00	1.80	.2000 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

<----- DATA FOR SECTION ( 4.0) ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x V (m2/s)
.112	.112	.646E+02	.602E+01	.016	.087	86.32	.010
.225	.225	.187E+03	.389E+02	.054	.129	58.01	.029
.337	.337	.306E+03	.957E+02	.110	.161	46.50	.054
.450	.450	.443E+03	.185E+03	.185	.188	39.90	.085
.562	.562	.597E+03	.311E+03*	.280	.211	35.49	.119
.675	.675	.769E+03	.481E+03*	.397	.233	32.26	.157
.788	.788	.958E+03	.698E+03*	.537	.252	29.75	.199
.900	.900	.116E+04	.970E+03*	.700	.270	27.73	.243
1.013	1.013	.139E+04	.130E+04*	.888	.288	26.06	.291
1.126	1.126	.163E+04	.170E+04*	1.102	.304	24.63	.343
1.238	1.238	.189E+04	.216E+04*	1.344	.320	23.41	.397
1.350	1.350	.216E+04	.271E+04*	1.615	.336	22.33	.453
1.463	1.463	.246E+04	.332E+04*	1.916	.351	21.38	.513
1.575	1.575	.278E+04	.404E+04*	2.247	.365	20.53	.575
1.688	1.688	.310E+04	.484E+04*	2.611	.379	19.77	.640
1.800	1.800	.344E+04	.574E+04*	3.008	.393	19.07	.708
1.933	1.933	.382E+04	.661E+04*	3.971	.227	33.00	.439
2.067	2.067	.423E+04	.754E+04*	4.943	.142	52.79	.294
2.200	2.200	.467E+04	.852E+04*	5.927	.124	60.70	.272

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4:002050	174.66	3.725	8.22	35.002	1.899	.255
OUTFLOW: ID= 1:002060	174.66	3.503	8.77	35.002	1.871	.284

010:0017-----

DESIGN NASHYD	Area (ha)	6.60	Curve Number (CN)=82.00
02:EXTS DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	.820	

Unit Hyd Qpeak (cms)	= .307
PEAK FLOW (cms)	= .267 (i)
TIME TO PEAK (hrs)	= 6.734
RUNOFF VOLUME (mm)	= 37.125
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0018-----

*# Lappan Drain - Total Flow at McGill Drain						
ADD HYD ( 2070)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)

ID1 01:	2070	174.66	3.503	8.77	35.00	.000
+ID2 02:EXTS		6.60	.267	6.73	37.12	.000
SUM 04:	2090	181.26	3.576	8.77	35.08	.000

010:0020-----

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN< 01:106	Number of SEGMENTS	= 3
OUT< 02:002080	Slopes (%), CHANNEL= 1.500 FLOODPLAIN= .2000	
	LENGTH = 250.00 (m)	

Distance	Elevation	Manning
.00	1.40	.2000
200.00	1.00	.2000 / 1000 Main Channel
201.50	.00	.1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / 2000 Main Channel
405.00	1.40	.2000

<----- DATA FOR SECTION ( 5.0) ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x V (m2/s)
.071	.071	.378E+02	.358E+01	.010	.064	65.43	.005
.143	.143	.791E+02	.151E+02	.031	.097	42.85	.014
.214	.214	.124E+03	.355E+02	.061	.123	33.82	.026
.286	.286	.173E+03	.661E+02	.101	.145	28.74	.041
.357	.357	.228E+03	.109E+03	.148	.164	25.41	.059
.429	.429	.283E+03	.162E+03*	.205	.181	23.02	.078
.500	.500	.344E+03	.229E+03*	.270	.197	21.20	.098
.571	.571	.408E+03	.311E+03*	.344	.211	19.75	.121
.643	.643	.474E+03	.408E+03*	.428	.225	18.56	.144
.714	.714	.548E+03	.522E+03*	.521	.237	17.56	.169
.786	.786	.624E+03	.654E+03*	.623	.249	16.71	.196
.857	.857	.704E+03	.805E+03*	.735	.261	15.96	.224
.929	.929	.788E+03	.975E+03*	.858	.272	15.31	.253
1.000	1.000	.875E+03	.117E+04*	.990	.283	14.73	.283
1.080	1.080	.100E+04	.150E+04*	1.270	.197	23.30	.193
1.160	1.160	.116E+04	.196E+04*	1.927	.113	36.97	.131
1.240	1.240	.132E+04	.250E+04*	3.185	.095	43.82	.118
1.320	1.320	.141E+05	.248E+05*	5.229	.093	44.86	.123
1.400	1.400	.154E+05	.399E+05*	8.222	.096	43.33	.135

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 1:106	39.07	.943	7.67	37.125	.975	.279
OUTFLOW: ID= 2:002080	39.07	.917	7.78	37.125	.961	.277

010:0021-----

DESIGN NASHYD	Area (ha)	21.08	Curve Number (CN)=81.00
01:EXT4 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.830	

Unit Hyd Qpeak (cms)	= .440
PEAK FLOW (cms)	= .451 (i)
TIME TO PEAK (hrs)	= 7.918
RUNOFF VOLUME (mm)	= 36.009
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .520

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0022-----

DESIGN NASHYD	Area (ha)	6.53	Curve Number (CN)=82.00
03:107 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	.820	

Unit Hyd Qpeak (cms)	= .304
PEAK FLOW (cms)	= .264 (i)
TIME TO PEAK (hrs)	= 6.734
RUNOFF VOLUME (mm)	= 37.125
TOTAL RAINFALL (mm)	= 69.200
RUNOFF COEFFICIENT	= .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0023-----

*# McGill Drain - Total Flow at Jefferson Boulevard						
ADD HYD ( 2090)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)

ID1 01:EXT4	2080	39.07	.917	7.78	37.12	.000
+ID2 02:		6.53	.264	6.73	37.12	.000
+ID3 03:107		6.53	.264	6.73	37.12	.000
SUM 04:	2090	66.68	1.514	7.75	36.77	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0024-----

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN< 04:002090	Number of SEGMENTS	= 3
OUT< 01:002100	Slopes (%), CHANNEL= 3.000 FLOODPLAIN= .2000	
	LENGTH = 280.00 (m)	

Distance	Elevation	Manning
.00	1.40	.2000
200.00	1.00	.2000 / 1000 Main Channel
201.50	.00	.1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / 2000 Main Channel

405.00 1.40 2000

----- TRAVEL TIME TABLE -----

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.071	.071	.421E+02	.179E+01	.014	.090	51.82	.006
.143	.143	.886E+02	.733E+01	.043	.138	33.94	.020
.214	.214	.139E+03	.178E+02	.087	.174	26.78	.037
.286	.286	.194E+03	.330E+02	.142	.205	22.76	.059
.357	.357	.254E+03	.539E+02	.210	.232	20.12	.083
.429	.429	.317E+03	.809E+02	.290	.256	18.23	.110
.500	.500	.385E+03	.115E+03	.382	.278	16.79	.139
.571	.571	.457E+03	.155E+03	.487	.298	15.64	.171
.643	.643	.534E+03	.204E+03	.605	.318	14.70	.204
.714	.714	.614E+03	.261E+03	.736	.336	13.91	.240
.786	.786	.699E+03	.327E+03	.881	.353	13.23	.277
.857	.857	.789E+03	.402E+03*	1.040	.369	12.64	.316
.929	.929	.882E+03	.488E+03*	1.213	.385	12.12	.357
1.000	1.000	.980E+03	.586E+03*	1.401	.400	11.66	.400
1.080	1.080	.109E+04	.692E+03*	1.761	.248	18.81	.268
1.160	1.160	.120E+04	.811E+03*	2.505	.147	31.85	.170
1.240	1.240	.132E+04	.938E+03*	3.856	.115	40.54	.143
1.320	1.320	.148E+04	.107E+04*	5.997	.107	43.81	.141
1.400	1.400	.169E+04	.123E+04*	9.093	.106	43.88	.149

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

----- hydrograph ----- <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
66.68	1.514	7.75	36.772	1.025	.335
66.68	1.489	8.22	36.772	1.020	.348

INFLOW : ID= 4:002090  
 OUTFLOW : ID= 1:002100

010:0025-----

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:EXT5 DT= 1.00	14.81	#2.00

U.H. Tp(hrs)= 1.520

Unit Hyd Qpeak (cms)= .372

PEAK FLOW (cms)= .377 (i)  
 TIME TO PEAK (hrs)= 7.534  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0026-----

ADD HYD ( 2110 )	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:	2100	66.68	1.489	8.22	36.77	.000
+ID2 02:EXT5		14.81	.377	7.53	37.12	.000
SUM 03:	2110	81.49	1.835	8.17	36.84	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0027-----

\*# McGill Drain - Total Flow at Lappan Drain Confluence

ADD HYD ( 2120 )	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 03:	2110	81.49	1.835	8.17	36.84	.000
+ID2 10:	2070	181.26	3.576	8.77	35.08	.000
SUM 01:	2120	262.75	5.282	8.52	35.62	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0028-----

ROUTE CHANNEL	Routing time step (min)	Number of SEGMENTS	Slopes (%)	CHANNEL LENGTH (m)	FLOODPLAIN=
01:002120	1.00	3	.1500	370.00	.2000
02:002130					

----- DATA FOR SECTION ( 7.0 ) -----

Distance	Elevation	Manning
.00	1.80	.2000
1.40	1.40	.2000 / .0850 Main Channel
202.60	.00	.0850 Main Channel
204.40	.00	.0850 Main Channel
207.00	1.40	.0850 / .2000 Main Channel
407.00	1.80	.2000

----- TRAVEL TIME TABLE -----

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.071	.071	.421E+02	.179E+01	.016	.087	70.58	.008
.187	.187	.148E+03	.249E+02	.053	.131	46.93	.025
.280	.280	.240E+03	.406E+02	.107	.165	37.37	.046
.373	.373	.344E+03	.616E+03	.180	.193	31.94	.072
.467	.467	.460E+03	.894E+03	.271	.218	28.33	.102
.560	.560	.588E+03	.129E+04	.382	.240	25.70	.134
.653	.653	.728E+03	.182E+04*	.513	.260	23.68	.170
.747	.747	.880E+03	.252E+04*	.665	.280	22.05	.209
.840	.840	.104E+04	.330E+04*	.840	.298	20.71	.250
.933	.933	.122E+04	.413E+04*	1.039	.315	19.58	.294
1.027	1.027	.141E+04	.500E+04*	1.262	.332	18.60	.340
1.120	1.120	.161E+04	.592E+04*	1.510	.348	17.74	.389
1.213	1.213	.182E+04	.690E+04*	1.785	.363	16.99	.440
1.307	1.307	.204E+04	.794E+04*	2.087	.378	16.32	.494
1.400	1.400	.228E+04	.904E+04*	2.418	.392	15.71	.549
1.500	1.500	.254E+04	.102E+05*	3.044	.257	24.02	.385
1.600	1.600	.282E+04	.117E+05*	4.365	.158	38.94	.253
1.700	1.700	.312E+04	.134E+05*	6.783	.127	48.42	.217
1.800	1.800	.342E+04	.154E+05*	10.633	.120	51.59	.215

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

----- hydrograph ----- <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
262.75	5.282	8.52	35.624	1.638	.145
262.75	4.823	9.25	35.624	1.619	.151

INFLOW : ID= 1:002120  
 OUTFLOW : ID= 2:002130

010:0029-----

DESIGN NASHYD	Area (ha)	Curve Number (CN)
03:109 DT= 1.00	47.17	#2.00

U.H. Tp(hrs)= 1.100

Unit Hyd Qpeak (cms)= 1.638

PEAK FLOW (cms)= 1.536 (i)  
 TIME TO PEAK (hrs)= 7.051  
 RUNOFF VOLUME (mm)= 37.125

TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0030-----

DESIGN NASHYD	Area (ha)	Curve Number (CN)
04:EXT6 DT= 1.00	24.11	#2.00

U.H. Tp(hrs)= 1.520

Unit Hyd Qpeak (cms)= .606

PEAK FLOW (cms)= .576 (i)  
 TIME TO PEAK (hrs)= 7.551  
 RUNOFF VOLUME (mm)= 34.934  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .505

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0031-----

ADD HYD ( 2140 )	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 02:	2130	262.75	4.823	9.25	35.62	.000
+ID2 03:109		47.17	1.536	7.05	37.12	.000
+ID3 04:EXT6		24.11	.576	7.55	34.93	.000
SUM 01:	2140	334.03	5.811	8.80	35.79	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0032-----

ROUTE CHANNEL	Routing time step (min)	Number of SEGMENTS	Slopes (%)	CHANNEL LENGTH (m)	FLOODPLAIN=
01:002140	1.00	3	.0800	370.00	.2000
02:002150					

----- DATA FOR SECTION ( 7.0 ) -----

Distance	Elevation	Manning
.00	1.80	.2000
200.00	1.40	.2000 / .0850 Main Channel
202.60	.00	.0850 Main Channel
204.40	.00	.0850 Main Channel
207.00	1.40	.0850 / .2000 Main Channel
407.00	1.80	.2000

----- TRAVEL TIME TABLE -----

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.093	.093	.681E+02	.107E+02	.012	.064	96.65	.006
.187	.187	.148E+03	.249E+02	.038	.096	64.26	.018
.280	.280	.240E+03	.406E+02	.078	.121	51.18	.034
.373	.373	.344E+03	.616E+03	.131	.141	43.73	.053
.467	.467	.460E+03	.894E+03	.198	.159	38.79	.074
.560	.560	.588E+03	.129E+04	.279	.175	35.19	.098
.653	.653	.728E+03	.182E+04*	.374	.190	32.42	.124
.747	.747	.880E+03	.252E+04*	.486	.204	30.20	.152
.840	.840	.104E+04	.330E+04*	.614	.217	28.36	.183
.933	.933	.122E+04	.413E+04*	.759	.230	26.81	.215
1.027	1.027	.141E+04	.500E+04*	.921	.242	25.47	.249
1.120	1.120	.161E+04	.592E+04*	1.103	.254	24.30	.284
1.213	1.213	.182E+04	.690E+04*	1.304	.265	23.27	.322
1.307	1.307	.204E+04	.794E+04*	1.524	.276	22.34	.361
1.400	1.400	.228E+04	.904E+04*	1.766	.287	21.51	.401
1.500	1.500	.254E+04	.102E+05*	2.264	.191	32.30	.286
1.600	1.600	.282E+04	.117E+05*	3.447	.125	49.30	.200
1.700	1.700	.312E+04	.134E+05*	5.720	.107	57.42	.183
1.800	1.800	.342E+04	.154E+05*	9.415	.106	58.27	.191

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

----- hydrograph ----- <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
334.03	5.811	8.80	35.786	1.702	.107
334.03	5.284	9.83	35.786	1.679	.111

INFLOW : ID= 1:002140  
 OUTFLOW : ID= 10:002150

010:0033-----

DESIGN NASHYD	Area (ha)	Curve Number (CN)
01:113 DT= 1.00	17.65	#2.00

U.H. Tp(hrs)= .910

Unit Hyd Qpeak (cms)= .741

PEAK FLOW (cms)= .661 (i)  
 TIME TO PEAK (hrs)= 6.834  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0034-----

\*# Calculate culvert routing and flow split near eastern site boundary  
 \*# Storage volumes calculated based on site survey  
 \*# Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities

ROUTE RESERVOIR	Requested routing time step =
IN:01: (113 )	1.0 min.
OUT:02: (002160)	

----- OUTFLOW STORAGE TABLE -----

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.000	.000E+00	1.130	.4600E+00
.150	.0000E+00	5.470	.8100E+00
.450	.0000E+00	83.090	.3400E+01
.820	.6500E-01	.000	.0000E+00

ROUTING RESULTS

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
17.65	.661	6.834	37.125
17.65	.603	7.218	37.136

PEAK FLOW REDUCTION [Out/(In)] (%)= 91.100  
 TIME SHIFT OF PEAK FLOW (min)= 23.00  
 MAXIMUM STORAGE USED (ha.m.)= 2680E-01

010:0035-----

DIVERT HYD	Flow 03 + Flow 04 = Total
INID=02 (002160)	

----- Outflow / Inflow Relationships -----

(cms)	(cms)	(cms)
.000	.000	.000
.150	.000	.150
.400	.050	.450



.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090

NHYD AREA OPEAK TpeakDate\_hh:mm R.V. NFE WetHrs
IDin = 02:002160 17.65 .603 No\_date 7:13 37.136 156 13.

010:0036

DESIGN NASHYD | Area (ha) = 4.88 Curve Number (CN)=82.00
| 01:114 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = .205

PEAK FLOW (cms) = .183 (I)
TIME TO PEAK (hrs) = 6.834
RUNOFF VOLUME (mm) = 37.125
TOTAL RAINFALL (mm) = 69.200
RUNOFF COEFFICIENT = .536

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0037

ADD HYD ( 2190) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
ID1 01:114 (ha) (cms) (hrs) (mm) (cms)
+ID2 03: 2170 16.03 .515 7.22 37.14 .000
SUM 02: 2190 20.91 .687 7.08 37.13 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0038

DESIGN NASHYD | Area (ha) = 18.59 Curve Number (CN)=82.00
| 01:115 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = .483

PEAK FLOW (cms) = .486 (I)
TIME TO PEAK (hrs) = 7.484
RUNOFF VOLUME (mm) = 37.125
TOTAL RAINFALL (mm) = 69.200
RUNOFF COEFFICIENT = .536

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0039

McGill Drain - Total Flow at Eastern WSP
ADD HYD ( 2200) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
ID1 01:115 (ha) (cms) (hrs) (mm) (cms)
+ID2 02: 2190 20.91 .687 7.08 37.13 .000
+ID3 10: 2150 334.03 5.284 9.83 35.79 .000
SUM 05: 2200 373.53 5.750 9.42 35.93 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0040

AREA CHECK
ADD HYD ( 2180) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
ID1 04: 2180 1.62 .087 7.22 37.14 .000
+ID2 05: 2200 373.53 5.750 9.42 35.93 .000
SUM 01: 2210 375.15 5.762 9.42 35.93 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0041

DESIGN NASHYD | Area (ha) = 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

010:0002

DESIGN NASHYD | Area (ha) = 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

010:0002

DESIGN NASHYD | Area (ha) = 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = 1.473

PEAK FLOW (cms) = 1.744 (I)
TIME TO PEAK (hrs) = 7.051
RUNOFF VOLUME (mm) = 46.563
TOTAL RAINFALL (mm) = 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0002

READ STORM | Filename: 25-yr scs 12 hr windsor
| Ptotal= 80.80 mm | Comments: 25-yr scs 12 hr windsor

Project Name: [Windsor Solar Project] Project Number: [1335-60106]
Date: 02-02-2016
Modeller: [NE]
Company: [Stantec Consulting Ltd. (London)]
License #: 4730904

Existing Conditions
25 mm Water Quality Event
2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm

025:0002

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002010 | Number of SEGMENTS = 3
| OUT< 01:002020 | Slopes (%), CHANNEL=1.700 FLOODPLAIN= .2000
LENGTH = 1000.00 (m)

DATA FOR SECTION ( 2.0)
Distance Elevation Manning
100.00 1.80 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .2000 Main Channel
207.00 2.00 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

0.71 .071 .645E+02 .325E+01 .005 .059 197.27 .004
1.41 .141 .140E+03 .141E+02 .018 .089 131.37 .013
2.12 .212 .225E+03 .340E+02 .036 .111 104.80 .024

025:0003

LAPPAN DRAIN

DESIGN NASHYD | Area (ha) = 42.26 Curve Number (CN)=73.00
| 01:101 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = 1.454

PEAK FLOW (cms) = 1.319 (I)
TIME TO PEAK (hrs) = 7.084
RUNOFF VOLUME (mm) = 36.299
TOTAL RAINFALL (mm) = 80.801
RUNOFF COEFFICIENT = .449

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0004

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:101 | Number of SEGMENTS = 3
| OUT< 02:002000 | Slopes (%), CHANNEL=1.000 FLOODPLAIN= .2000
LENGTH = 700.00 (m)

DATA FOR SECTION ( 1.0)
Distance Elevation Manning
100.00 1.20 .2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

0.71 .071 .645E+02 .325E+01 .005 .059 197.27 .004
1.41 .141 .140E+03 .141E+02 .018 .089 131.37 .013
2.12 .212 .225E+03 .340E+02 .036 .111 104.80 .024

025:0005

DESIGN NASHYD | Area (ha) = 22.52 Curve Number (CN)=82.00
| 01:102 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = .677

PEAK FLOW (cms) = .829 (I)
TIME TO PEAK (hrs) = 7.234
RUNOFF VOLUME (mm) = 46.563
TOTAL RAINFALL (mm) = 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0006

DESIGN NASHYD | Area (ha) = 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm) = 1.500 # of Linear Res. (N) = 3.00

Unit Hyd Qpeak (cms) = 1.473

PEAK FLOW (cms) = 1.744 (I)
TIME TO PEAK (hrs) = 7.051
RUNOFF VOLUME (mm) = 46.563
TOTAL RAINFALL (mm) = 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0007

LAPPAN Drain - Total Flow at Filette Road

ADD HYD ( 2010) | ID: NHYD AREA OPEAK TPEAK R.V. DWF
ID1 01:102 (ha) (cms) (hrs) (mm) (cms)
+ID2 02: 2000 42.26 1.100 7.97 36.30 .000
+ID3 03:103 42.81 1.744 7.05 46.56 .000
SUM 04: 2010 107.59 3.428 7.33 42.53 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0008

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002010 | Number of SEGMENTS = 3
| OUT< 01:002020 | Slopes (%), CHANNEL=1.700 FLOODPLAIN= .2000
LENGTH = 1000.00 (m)

DATA FOR SECTION ( 2.0)
Distance Elevation Manning
100.00 1.80 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .2000 Main Channel
207.00 2.00 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

100.00 1.00 .165E+03 .486E+01 .016 .096 172.86 .010
200.00 200.00 .361E+03 .212E+02 .052 .144 115.66 .029
300.00 300.00 .568E+03 .518E+02 .106 .180 92.51 .054

400.00 400.00 .844E+03 .993E+02 .177 .210 79.29 .084
500.00 .500 .113E+04 .166E+03 .268 .236 70.48 .118

Table with 10 columns: X, Y, Z, S, T, U, V, W, X, Y. Values range from 0.600 to 2.000.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 10 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

025:0009

DESIGN NASHYD | Area (ha)= 19.36 Curve Number (CN)=82.00 | 02:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .510
PEAK FLOW (cms)= .644 (I)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0010

DESIGN NASHYD | Area (ha)= 25.24 Curve Number (CN)=82.00 | 03:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .665
PEAK FLOW (cms)= .840 (I)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0011

ADD HYD ( 2030) | ID: NHYD AREA QPEAK TPEAK R.V. DWF. Includes ID1, ID2, ID3, and SUM 04 data.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0012

ROUTE CHANNEL | Routing time step (min) = 1.00 | IN: 04:002030 | Number of SEGMENTS = 3 | SLOPE (%), CHANNEL= 1200 FLOODPLAIN= .2000

DATA FOR SECTION ( 3.0) table with columns: Distance, Elevation, Manning. Values range from 0.00 to 407.00.

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Values range from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 10 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

025:0013

DESIGN NASHYD | Area (ha)= 15.67 Curve Number (CN)=82.00 | 02:108 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .549
PEAK FLOW (cms)= .647 (I)
TIME TO PEAK (hrs)= 7.034
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0014

Table with 10 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

DESIGN NASHYD | Area (ha)= 6.80 Curve Number (CN)=82.00 | 03:105A DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .271
PEAK FLOW (cms)= .309 (I)
TIME TO PEAK (hrs)= 6.884
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0015

ADD HYD ( 2050) | ID: NHYD AREA QPEAK TPEAK R.V. DWF. Includes ID1, ID2, ID3, and SUM 04 data.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0016

ROUTE CHANNEL | Routing time step (min) = 1.00 | IN: 04:002050 | Number of SEGMENTS = 3 | SLOPE (%), CHANNEL= 1200 FLOODPLAIN= .2000

DATA FOR SECTION ( 4.0) table with columns: Distance, Elevation, Manning. Values range from 0.00 to 407.00.

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Values range from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

025:0017

DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00 | 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .336 (I)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0018

DESIGN NASHYD | Area (ha)= 39.07 Curve Number (CN)=82.00 | 01:106 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

ADD HYD ( 2070) | ID: NHYD AREA QPEAK TPEAK R.V. DWF. Includes ID1, ID2, and SUM 10 data.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0019

DESIGN NASHYD | Area (ha)= 39.07 Curve Number (CN)=82.00 | 01:106 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .916
PEAK FLOW (cms)= 1.188 (I)
TIME TO PEAK (hrs)= 7.651
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(I) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0020

ROUTE CHANNEL | Routing time step (min) = 1.00 | IN: 01:106 | Number of SEGMENTS = 3 | SLOPE (%), CHANNEL= 1500 FLOODPLAIN= .2000

DATA FOR SECTION ( 5.0) table with columns: Distance, Elevation, Manning. Values range from 0.00 to 407.00.

Distance	Elevation	Manning
.00	1.40	.0200
200.00	1.00	.0200 / .1000
201.50	.00	.1000
203.50	.00	.1000
205.00	1.00	.1000 / .2000
405.00	1.40	.2000

TRAVEL TIME TABLE							
DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV. TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.071	.071	.376E+02	.358E+01	.010	.064	65.43	.005
.143	.143	.791E+02	.151E+02	.031	.097	42.85	.014
.214	.214	.124E+03	.355E+02	.061	.123	33.82	.026
.286	.286	.172E+03	.661E+02	.101	.145	28.74	.041
.357	.357	.226E+03	.108E+03	.148	.164	25.41	.059
.429	.429	.283E+03	.162E+03*	.205	.181	23.02	.078
.500	.500	.344E+03	.229E+03*	.270	.197	21.20	.098
.571	.571	.408E+03	.311E+03*	.344	.213	19.75	.121
.643	.643	.476E+03	.408E+03*	.428	.225	18.56	.144
.714	.714	.548E+03	.522E+03*	.521	.237	17.56	.169
.786	.786	.624E+03	.654E+03*	.623	.249	16.71	.196
.857	.857	.704E+03	.803E+03*	.735	.261	15.96	.224
.929	.929	.788E+03	.975E+03*	.858	.272	15.31	.253
1.000	1.000	.875E+03	.117E+04*	.990	.283	14.73	.283
1.080	1.080	.177E+04	.256E+04*	1.270	.179	23.30	.193
1.160	1.160	.427E+04	.661E+04*	1.927	.113	36.97	.131
1.240	1.240	.837E+04	.138E+05*	3.185	.095	43.82	.118
1.320	1.320	.141E+05	.248E+05*	5.229	.093	44.86	.123
1.400	1.400	.214E+05	.399E+05*	8.222	.096	43.33	.135

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph --->								<-pipe / channel->			
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL						
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)						
INFLOW : ID= 1:106	1.188	7.65	46.563	1.129	1.039						
OUTFLOW: ID= 2:002080	39.07	1.129	8.23 46.562	1.039	.220						

025:0021-----

DESIGN NASHYD	Area	(ha)	21.08	Curve Number	(CN)=81.00
01:EXT4 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00	
	U.H. Tp(hrs)		1.830		

Unit Hyd Qpeak (cms)= .440

PEAK FLOW (cms)= .569 (i)  
TIME TO PEAK (hrs)= 7.901  
RUNOFF VOLUME (mm)= 45.280  
TOTAL RAINFALL (mm)= 80.801  
RUNOFF COEFFICIENT = .560

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0022-----

DESIGN NASHYD	Area	(ha)	6.53	Curve Number	(CN)=82.00
03:107 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00	
	U.H. Tp(hrs)		.820		

Unit Hyd Qpeak (cms)= .304

PEAK FLOW (cms)= .332 (i)  
TIME TO PEAK (hrs)= 6.734  
RUNOFF VOLUME (mm)= 46.563  
TOTAL RAINFALL (mm)= 80.801  
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0023-----

\*\*\*\*\*  
# McGill Drain = 2090 Flow at 366m Reservoir  
\*\*\*\*\*

ID	AREA	QPEAK	TPEAK	R.V.	DWF
(ha)	(cms)	(hrs)	(mm)	(m)	(cms)
ID1 01:EXT4	21.08	.569	7.90	45.28	.000
+ID2 02:	2080	39.07	1.129	8.23 46.56	.000
+ID3 03:107	6.53	.332	6.73	46.56	.000
SUM 04:	2090	66.68	1.840	7.87 46.16	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0024-----

ROUTE CHANNEL	Routing time step (min)	1.00
IN> 04:002100	Number of SEGMENTS = 3	
OUT< 01:002100	Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000	
	LENGTH = 280.00 (m)	

<----- DATA FOR SECTION ( 6.0) ----->

Distance	Elevation	Manning
.00	1.40	.0200
200.00	1.00	.2000 / .1000
201.50	.00	.1000
203.50	.00	.1000
205.00	1.00	.1000 / .2000
405.00	1.40	.2000

TRAVEL TIME TABLE							
DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV. TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.071	.071	.421E+02	.179E+01	.014	.090	51.82	.006
.143	.143	.886E+02	.753E+01	.043	.138	33.94	.020
.214	.214	.139E+03	.178E+02	.087	.174	26.78	.037
.286	.286	.194E+03	.330E+02	.142	.205	22.76	.059
.357	.357	.254E+03	.539E+02	.210	.232	20.12	.089
.429	.429	.317E+03	.809E+02	.290	.256	18.23	.110
.500	.500	.385E+03	.115E+03	.382	.278	16.79	.139
.571	.571	.457E+03	.155E+03	.487	.298	15.64	.171
.643	.643	.534E+03	.204E+03	.605	.318	14.70	.204
.714	.714	.614E+03	.261E+03	.736	.336	13.91	.240
.786	.786	.699E+03	.327E+03	.881	.353	13.23	.277
.857	.857	.789E+03	.402E+03*	1.040	.369	12.64	.316
.929	.929	.882E+03	.488E+03*	1.213	.385	12.12	.357
1.000	1.000	.980E+03	.583E+03*	1.401	.400	11.66	.400
1.080	1.080	.199E+04	.128E+04*	1.761	.248	18.81	.268
1.160	1.160	.479E+04	.331E+04*	2.505	.147	31.85	.170
1.240	1.240	.938E+04	.692E+04*	3.856	.115	40.54	.143
1.320	1.320	.158E+05	.124E+05*	5.997	.107	43.81	.141
1.400	1.400	.239E+05	.199E+05*	9.093	.106	43.88	.149

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph --->								<-pipe / channel->			
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL						
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)						
INFLOW : ID= 4:002090	66.68	1.840	7.87 46.157	1.089	.231						
OUTFLOW: ID= 1:002100	66.68	1.787	8.88 46.157	1.083	.242						

025:0025-----

DESIGN NASHYD	Area	(ha)	14.81	Curve Number	(CN)=82.00
02:EXT5 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00	
	U.H. Tp(hrs)		1.520		

Unit Hyd Qpeak (cms)= .372

PEAK FLOW (cms)= .475 (i)  
TIME TO PEAK (hrs)= 7.518  
RUNOFF VOLUME (mm)= 46.563  
TOTAL RAINFALL (mm)= 80.801  
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0026-----

ID	AREA	QPEAK	TPEAK	R.V.	DWF
(ha)	(cms)	(hrs)	(mm)	(m)	(cms)
ID1 01:	2100	66.68	1.787	8.88 46.16	.000
+ID2 02:EXT5	14.81	.475	7.52	46.56	.000
SUM 03:	2110	81.49	2.179	8.33 46.23	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0027-----

\*\*\*\*\*  
# McGill Drain - Total Flow at Lappan Drain Confluence  
\*\*\*\*\*

ID	AREA	QPEAK	TPEAK	R.V.	DWF
(ha)	(cms)	(hrs)	(mm)	(m)	(cms)
ID1 03:	2110	81.49	2.179	8.33 46.23	.000
+ID2 10:	2070	181.26	4.149	9.45 44.17	.000
SUM 01:	2120	262.75	6.173	8.87 44.81	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0028-----

ROUTE CHANNEL	Routing time step (min)	1.00
IN> 01:002120	Number of SEGMENTS = 3	
OUT< 02:002130	Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000	
	LENGTH = 370.00 (m)	

<----- DATA FOR SECTION ( 7.0) ----->

Distance	Elevation	Manning
.00	1.80	.2000
200.00	1.40	.2000 / .0850
202.60	.00	.0850
204.40	.00	.0850
207.00	1.40	.0850 / .2000
407.00	1.80	.2000

TRAVEL TIME TABLE							
DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV. TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.093	.093	.681E+02	.573E+01	.016	.087	70.58	.008
.187	.187	.148E+03	.249E+02	.053	.131	46.93	.025
.280	.280	.240E+03	.608E+02	.107	.165	37.37	.046
.373	.373	.344E+03	.115E+03	.180	.193	31.94	.072
.467	.467	.460E+03	.194E+03	.271	.218	28.33	.102
.560	.560	.588E+03	.297E+03*	.382	.240	25.70	.134
.653	.653	.728E+03	.429E+03*	.513	.260	23.68	.170
.747	.747	.894E+03	.592E+03*	.665	.280	22.05	.209
.840	.840	.104E+04	.790E+03*	.840	.298	20.71	.250
.933	.933	.122E+04	.103E+04*	1.039	.315	19.58	.294
1.027	1.027	.141E+04	.130E+04*	1.262	.332	18.60	.340
1.120	1.120	.161E+04	.162E+04*	1.510	.348	17.74	.389
1.213	1.213	.182E+04	.199E+04*	1.785	.363	16.99	.440
1.307	1.307	.204E+04	.241E+04*				

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph --->								<-pipe / channel->			
AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL						
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)						
INFLOW : ID= 1:002120	262.75	6.173	8.87 44.809	1.675	1.334						
OUTFLOW: ID= 2:002130	262.75	5.763	9.78 44.809	1.656	.139						

025:0029-----

DESIGN NASHYD	Area	(ha)	47.17	Curve Number	(CN)=82.00
03:109 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00	
	U.H. Tp(hrs)		1.100		

Unit Hyd Qpeak (cms)= 1.638

PEAK FLOW (cms)= 1.935 (i)  
TIME TO PEAK (hrs)= 7.051  
RUNOFF VOLUME (mm)= 46.563  
TOTAL RAINFALL (mm)= 80.801  
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0030-----

DESIGN NASHYD	Area	(ha)	24.11	Curve Number	(CN)=80.00
04:EXT6 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00	
	U.H. Tp(hrs)		1.520		

Unit Hyd Qpeak (cms)= .606

PEAK FLOW (cms)= .729 (i)  
TIME TO PEAK (hrs)= 7.534  
RUNOFF VOLUME (mm)= 44.038  
TOTAL RAINFALL (mm)= 80.801  
RUNOFF COEFFICIENT = .545

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0031-----

ID	AREA	QPEAK	TPEAK	R.V.	DWF
(ha)	(cms)	(hrs)	(mm)	(m)	(cms)
ID1 02:	2130	262.75	5.763	9.78 44.81	.000
+ID2 03:109	47.17	1.935	7.05 46.56	.000	
+ID3 04:EXT6	24.11	.729	7.53 44.04	.000	
SUM 01:	2140	334.03	6.789	9.05 45.00	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



025:0032-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 01:002140 | Number of SEGMENTS = 3
OUT< 10:002150 | Slopes (%), CHANNEL= .0850 FLOODPLAIN= .2000
LENGTH = 370.00 (m)

Table with 4 columns: Distance, Elevation, Manning, and Flow Rate. Data points range from 0.00 to 407.00 distance and 1.80 to 2.0000 elevation.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Data points range from 0.93 to 1.800 depth and 0.93 to 1.8000 elevation.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph <-> <-pipe / channel-> table with columns: INFLOW ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL.

025:0033-----
DESIGN NASHYD | Area (ha)= 17.65 Curve Number (CN)=82.00
01:113 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .910

Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= 833 (i)
TIME TO PEAK (hrs)= 6.834
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0034-----
\* Calculate culvert routing and flow split near eastern site boundary
\* Storage volumes calculated based on site survey
\* Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities

ROUTING RESULTS table with columns: INFLOW >01: (113), OUTFLOW <02: (002160), AREA, QPEAK, TPEAK, R.V.

PEAK FLOW REDUCTION [Qout/Qin] (%) = 89.397
TIME SHIFT OF PEAK FLOW (min) = 25.00
MAXIMUM STORAGE USED (ha.m.) = 51.79E-01

025:0035-----
DIVERGE HYD |
IND=02 (002160) |

Outflow / Inflow Relationships table with columns: Flow 03 + Flow 04 = Total, (cms), (cms), (cms)

NHYD table with columns: IDin, AREA, QPEAK, TpeakDate, hh:mm, R.V., NFE, WetHrs

025:0036-----
DESIGN NASHYD | Area (ha)= 4.88 Curve Number (CN)=82.00
01:114 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .910

Unit Hyd Qpeak (cms)= .205
PEAK FLOW (cms)= .230 (i)
TIME TO PEAK (hrs)= 6.834
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0037-----
ADD HYD ( 2190) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01:114 4.88 .230 6.83 46.56 .000
+ID2 03: 2170 15.78 .623 7.25 46.57 .000

SUM 02: 2190 20.66 .836 7.12 46.57 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0038-----
DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
01:115 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.470

Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .612 (i)
TIME TO PEAK (hrs)= 7.468
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0039-----
MCGILL Drain - Total Flow at Eastern WSP

ADD HYD ( 2200) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01:115 18.59 .612 7.47 46.56 .000
+ID2 05: 2190 20.66 .836 7.12 46.57 .000
+ID3 10: 2150 334.03 6.311 10.05 45.00 .000

SUM 05: 2200 373.28 6.806 9.77 45.17 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0040-----
AREA CHECK

ADD HYD ( 2210) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 04: 2180 1.87 .122 7.25 46.57 .000
+ID2 05: 2200 373.28 6.806 9.77 45.17 .000

SUM 01: 2210 375.15 6.813 9.77 45.17 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0041-----
DESIGN NASHYD | Area (ha)= 17.65 Curve Number (CN)=82.00
01:113 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .910

Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= 833 (i)
TIME TO PEAK (hrs)= 6.834
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

\*\* END OF RUN : 49

025:0042-----
START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
METOUT= 2 (output = METRIC)
NRUN = 050
NSTORM= 1
# 1=12acc50.stm

050:0002-----
Project Name: [Windsor Solar Project] Project Number: [1335-60106]
Date : 02-02-2016
Modeller : [NE]
Company : Stantec Consulting Ltd. (London)
Licence # : 4730904

050:0002-----
READ STORM | Filename: 50-yr scs 12 hr windsor
Ptotal= 89.40 mm Comments: 50-yr scs 12 hr windsor

Table with columns: TIME RAIN, TIME RAIN, TIME RAIN, TIME RAIN, TIME RAIN, TIME RAIN

050:0003-----
LAPPAN DRAIN

DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
01:101 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110

Unit Hyd Qpeak (cms)= 1.454
PEAK FLOW (cms)= 1.549 (i)
TIME TO PEAK (hrs)= 7.084
RUNOFF VOLUME (mm)= 42.489
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .475

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0004-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 01:101 | Number of SEGMENTS = 3
OUT< 02:002000 | Slopes (%), CHANNEL= .1000 FLOODPLAIN= .2000
LENGTH = 700.00 (m)

DATA FOR SECTION ( 1.0) table with columns: Distance, Elevation, Manning, Flow Rate

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Routing time step, Number of SEGMENTS, Slopes, CHANNEL, FLOODPLAIN, LENGTH

DATA FOR SECTION table with columns: Distance, Elevation, Manning

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD table with columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Routing time step, Number of SEGMENTS, Slopes, CHANNEL, FLOODPLAIN, LENGTH

DATA FOR SECTION table with columns: Distance, Elevation, Manning

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Routing time step, Number of SEGMENTS, Slopes, CHANNEL, FLOODPLAIN, LENGTH

DATA FOR SECTION table with columns: Distance, Elevation, Manning

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL

DESIGN NASHVD table with columns: DESIGN NASHVD, Area, Curve Number, DT, Ia, U.H. Tp

Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT

```

| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002050 | Number of SEGMENTS = 3
| OUT< 01:002060 | Slopes (%), CHANNEL= 1200 FLOODPLAIN= .2000
|-----|-----|
| ROUTE CHANNEL | Length = 450.00 (m)
|-----|-----|
<----- DATA FOR SECTION ( 4.0) ----->
Distance Elevation Manning
.00 2.20 .2000
200.00 1.80 .2000 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .2000 Main Channel
407.00 2.20 .2000

```

```

<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:106 39.07 1.375 7.65 53.784 1.093 .163
OUTFLOW: ID= 2:002080 39.07 1.273 8.42 53.784 1.080 .178

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .848E+02 .882E+01 .016 .087 86.32 .010
.225 .225 .187E+03 .170E+02 .054 .129 58.01 .029
.337 .337 .306E+03 .957E+02 .110 .161 46.50 .054
.450 .450 .443E+03 .185E+03 .185 .188 39.90 .085
.562 .562 .597E+03 .311E+03* .280 .211 35.49 .119
.675 .675 .769E+03 .481E+03* .397 .233 32.26 .157
.788 .788 .958E+03 .698E+03* .537 .252 29.75 .199
.900 .900 .116E+04 .970E+03* .700 .270 27.73 .243
1.013 1.013 .139E+04 .130E+04* .888 .288 26.06 .291
1.125 1.125 .162E+04 .170E+04* 1.102 .304 24.63 .343
1.238 1.238 .189E+04 .216E+04* 1.344 .320 23.41 .397
1.350 1.350 .216E+04 .271E+04* 1.615 .336 22.33 .453
1.463 1.463 .246E+04 .333E+04* 1.916 .351 21.38 .513
1.575 1.575 .277E+04 .404E+04* 2.247 .365 20.53 .575
1.688 1.688 .310E+04 .484E+04* 2.611 .379 19.77 .640
1.800 1.800 .344E+04 .574E+04* 3.008 .393 19.07 .708
1.933 1.933 .386E+04 .674E+04* 3.431 .407 18.43 .781
2.067 2.067 .438E+04 .794E+04* 3.887 .422 17.82 .858
2.200 2.200 .497E+04 .938E+04* 4.377 .438 17.25 .938

```

```

050:0021-----
| DESIGN NASHYD | Area (ha)= 21.08 Curve Number (CN)=81.00
| 01:EXT4 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= 1.830

```

```

Unit Hyd Qpeak (cms)= .440
PEAK FLOW (cms)= .660 (l)
TIME TO PEAK (hrs)= 7.901
RUNOFF VOLUME (mm)= 52.390
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .586

```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

050:0022-----
| DESIGN NASHYD | Area (ha)= 6.53 Curve Number (CN)=82.00
| 03:107 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .820

```

```

Unit Hyd Qpeak (cms)= .304
PEAK FLOW (cms)= .385 (l)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002050 174.66 4.928 8.60 51.051 1.986 .184
OUTFLOW: ID= 1:002060 174.66 4.576 9.70 51.051 1.964 .200

```

```

050:0023-----
| ADD HYD ( 2090) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|
| ID1:01:EXT4 21.08 .660 7.90 52.39 .000
| ID2:02: 2080 39.07 1.273 8.42 53.78 .000
| ID3:03:107 6.53 .385 6.73 53.78 .000
|-----|-----|
| SUM 04: 2090 66.68 2.080 7.97 53.34 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

050:0024-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= 3000 FLOODPLAIN= .2000
|-----|-----|
| ROUTE CHANNEL | Length = 280.00 (m)
|-----|-----|
<----- DATA FOR SECTION ( 6.0) ----->
Distance Elevation Manning
.00 1.40 .2000
200.00 1.00 .2000 / .1000 Main Channel
201.50 .00 .1000 Main Channel
205.00 1.00 .1000 / .2000 Main Channel
405.00 1.40 .2000

```

```

050:0017-----
| DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00
| 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .820

```

```

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .389 (l)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

050:0018-----
| ADD HYD ( 2070) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|
| ID1:01: 2060 174.66 4.576 9.70 51.05 .000
| ID2:02:EXT8 6.60 .389 6.73 53.78 .000
|-----|-----|
| SUM 10: 2070 181.26 4.641 9.70 51.15 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .421E+02 .179E+01 .014 .090 51.82 .006
.143 .143 .848E+02 .358E+01 .028 .182 33.94 .020
.214 .214 .124E+03 .518E+02 .042 .265 26.78 .037
.286 .286 .174E+03 .730E+02 .060 .345 20.56 .059
.357 .357 .234E+03 .959E+02 .080 .450 16.32 .083
.429 .429 .317E+03 .124E+03 .100 .580 12.75 .110
.500 .500 .418E+03 .161E+03 .120 .740 9.80 .139
.571 .571 .534E+03 .204E+03 .150 .940 7.60 .171
.643 .643 .674E+03 .254E+03 .180 .1200 6.00 .204
.714 .714 .838E+03 .311E+03 .220 .1500 4.60 .240
.786 .786 .103E+04 .377E+03 .270 .1900 3.50 .277
.857 .857 .129E+04 .452E+03 .330 .2400 2.90 .316
.929 .929 .162E+04 .548E+03 .400 .3000 2.30 .357
1.000 1.000 .202E+04 .666E+03 .480 .3600 1.90 .400
1.080 1.080 .249E+04 .809E+03 .580 .4300 1.60 .440
1.160 1.160 .304E+04 .980E+03 .700 .5100 1.30 .470
1.240 1.240 .368E+04 .118E+04 .840 .6000 1.10 .500
1.320 1.320 .442E+04 .142E+04 .1000 .7000 .90 .530
1.400 1.400 .528E+04 .170E+04 .1200 .8200 .70 .560

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

050:0019-----
| DESIGN NASHYD | Area (ha)= 39.07 Curve Number (CN)=82.00
| 01:106 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= 1.630

```

```

Unit Hyd Qpeak (cms)= .916
PEAK FLOW (cms)= 1.375 (l)
TIME TO PEAK (hrs)= 7.651
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002090 66.68 2.080 7.97 53.343 1.114 .191
OUTFLOW: ID= 1:002100 66.68 2.006 8.73 53.343 1.105 .204

```

```

050:0025-----
| DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00
| 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= 1.520

```

```

Unit Hyd Qpeak (cms)= .372
PEAK FLOW (cms)= .550 (l)
TIME TO PEAK (hrs)= 7.518
RUNOFF VOLUME (mm)= 53.785
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

```

(l) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

050:0026-----
| ADD HYD ( 2110) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|
| ID1:01: 2100 66.68 2.006 8.73 53.34 .000
| ID2:02:EXT5 14.81 .550 7.52 53.78 .000
|-----|-----|
| SUM 03: 2110 81.49 2.441 8.50 53.42 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

050:0027-----
| ADD HYD ( 2110) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|
| ID1:01: 2100 66.68 2.006 8.73 53.34 .000
| ID2:02:EXT5 14.81 .550 7.52 53.78 .000
|-----|-----|
| SUM 03: 2110 81.49 2.441 8.50 53.42 .000

```

```

050:0027-----
| ADD HYD ( 2110) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|
| ID1:01: 2100 66.68 2.006 8.73 53.34 .000
| ID2:02:EXT5 14.81 .550 7.52 53.78 .000
|-----|-----|
| SUM 03: 2110 81.49 2.441 8.50 53.42 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



Table with columns: ADD HYD ( 2120) | ID: NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes summary row: SUM 01: 2120 262.75 6.922 9.25 51.86 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL routing table with columns: ROUTE CHANNEL, Routing time step (min) = 1.00, Number of SEGMENTS = 3, SLOPE (%), CHANNEL=1500, FLOODPLAIN=.2000, LENGTH = 370.00 (m)

DATA FOR SECTION ( 7.0) table with columns: Distance, Elevation, Manning, Main Channel. Includes values for 200.00, 202.60, 204.40, 207.00, 407.00

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=80.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2140) | ID: NHYD routing table with columns: ADD HYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes summary row: SUM 01: 2140 334.03 7.490 9.22 52.07 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL routing table with columns: ROUTE CHANNEL, Routing time step (min) = 1.00, Number of SEGMENTS = 3, SLOPE (%), CHANNEL=0800, FLOODPLAIN=.2000, LENGTH = 370.00 (m)

DATA FOR SECTION ( 7.0) table with columns: Distance, Elevation, Manning, Main Channel. Includes values for 200.00, 202.60, 204.40, 207.00, 407.00

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Summary table with columns: AREA, QPEAK, TPEAK, R.V., DWF. Includes values: 1.500, 1.500, .439E+04, .111E+05\*, 2.264, .191, 32.30, .286

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTING RESULTS table with columns: ROUTING RESULTS, AREA, QPEAK, TPEAK, R.V. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTING RESULTS table with columns: ROUTING RESULTS, AREA, QPEAK, TPEAK, R.V. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2190) | ID: NHYD routing table with columns: ADD HYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes summary row: SUM 02: 2190 20.46 .941 6.98 53.79 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHDY routing table with columns: DESIGN NASHDY, Area, Curve Number (CN)=82.00, DT=1.00, # of Linear Res. (N)=3.00. Includes summary row: (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2200) | ID: NHYD routing table with columns: ADD HYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes summary row: SUM 05: 2200 373.08 7.599 9.80 52.25 .000

Windsor Solar Energy Project

Existing Conditions SWMHYMO

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0040-----
#\* AREA CHECK
#\*
| ADD HYD ( 2210 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 04: 2180 2.07 .141 7.33 53.79 .000
+ID2 05: 2200 373.08 7.599 9.80 52.25 .000
SUM 01: 2210 375.15 7.612 9.80 52.26 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0041-----
050:0002-----
050:0002-----
050:0002-----
\*\* END OF RUN : 99

| START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
TEEROUT = .00 hrs on 0
METOUT = 2 (output = METRIC)
NRUN = 100
NSTORM = 1
# 1=12accs100.stm

100:0002-----
#\* Project Name: [Windsor Solar Project] Project Number: [1335-60106]
#\* Date : 02-02-2016
#\* Modeller : [NE]
#\* Company : Stantec Consulting Ltd. (London)
#\* License # : 4730904

| READ STORM | Filename: 100-yr scs 12 hr windsor
| Pictals: 98.00 mm | Comments: 100-yr scs 12 hr windsor
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.960 | 3.50 3.920 | 6.50 17.640 | 9.50 3.920
1.00 1.960 | 4.00 3.920 | 7.00 7.840 | 10.00 1.960
1.50 1.960 | 4.50 5.880 | 7.50 5.880 | 10.50 1.960
2.00 1.960 | 5.00 7.840 | 8.00 5.880 | 11.00 1.960
2.50 3.920 | 5.50 11.760 | 8.50 3.920 | 11.50 1.960
3.00 3.920 | 6.00 88.200 | 9.00 3.920 | 12.00 1.960

100:0003-----
#\* LAPPAN DRAIN
| DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
| 01:101 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms) = 1.454
PEAK FLOW (cms) = 1.788 (i)
TIME TO PEAK (hrs) = 7.058
RUNOFF VOLUME (mm) = 48.897
TOTAL RAINFALL (mm) = 98.000
RUNOFF COEFFICIENT = .499

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0004-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 01:101 | Number of SEGMENTS = 3
| OUT: 02:002000 | Slopes (%), CHANNEL= .1000 FLOODPLAIN= .2000
LENGTH = 700.00 (m)
<----- DATA FOR SECTION ( 1.0 ) ----->
Distance Elevation Manning
100.00 1.40 .2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .645E+02 .325E+01 .005 .059 197.27 .004
.141 .141 .140E+03 .141E+02 .018 .089 131.37 .013
.212 .212 .225E+03 .340E+02 .036 .111 104.80 .024
.282 .282 .321E+03 .647E+02 .060 .130 89.71 .037
.353 .353 .427E+03 .108E+03 .089 .146 79.68 .052
.424 .424 .544E+03 .165E+03 .125 .161 72.40 .068
.494 .494 .671E+03 .237E+03 .168 .175 66.79 .086
.565 .565 .809E+03 .326E+03 .217 .187 62.29 .106
.635 .635 .957E+03 .434E+03 .272 .199 58.56 .127
.706 .706 .112E+04 .563E+03\* .336 .211 55.41 .149
.776 .776 .129E+04 .713E+03\* .407 .221 52.69 .172
.847 .847 .146E+04 .886E+03\* .485 .232 50.32 .196
.918 .918 .166E+04 .108E+04\* .572 .242 48.22 .222
.988 .988 .186E+04 .131E+04\* .667 .252 46.35 .249
1.059 1.059 .207E+04 .156E+04\* .771 .261 44.66 .277
1.129 1.129 .229E+04 .185E+04\* .884 .271 43.13 .306
1.200 1.200 .252E+04 .216E+04\* 1.006 .280 41.73 .335
1.300 1.300 .336E+04 .290E+04\* 1.392 .353 76.12 .199
1.400 1.400 .172E+05 .172E+05\* 2.456 .100 116.67 .140

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:101 42.26 1.788 7.07 48.897 1.337 .128
OUTFLOW : ID= 2:002000 42.26 1.336 8.50 48.897 1.285 .164

100:0005-----
| DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00
| 01:102 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.270
Unit Hyd Qpeak (cms) = .677
PEAK FLOW (cms) = 1.094 (i)
TIME TO PEAK (hrs) = 7.218
RUNOFF VOLUME (mm) = 61.161
TOTAL RAINFALL (mm) = 98.000
RUNOFF COEFFICIENT = .624
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0006-----
| DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00
| 03:103 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms) = 1.473
PEAK FLOW (cms) = 2.302 (i)
TIME TO PEAK (hrs) = 7.051
RUNOFF VOLUME (mm) = 61.161
TOTAL RAINFALL (mm) = 98.000
RUNOFF COEFFICIENT = .624
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0007-----
#\* Lappan Drain - Total Flow at Ellette Road
| ADD HYD ( 2010 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:102 22.52 1.094 7.22 61.16 .000
+ID2 02: 2000 42.26 1.336 8.50 48.90 .000
+ID3 03:103 42.81 2.302 7.05 61.16 .000
SUM 04: 2010 107.59 4.402 7.23 56.34 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0008-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 04:002010 | Number of SEGMENTS = 3
| OUT: 01:002020 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
LENGTH = 1000.00 (m)

<----- DATA FOR SECTION ( 2.0 ) ----->
Distance Elevation Manning
100.00 2.00 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .2000 Main Channel
207.00 2.00 .2000
TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
100 .100 .165E+03 .486E+01 .016 .096 172.86 .010
.200 .200 .361E+03 .212E+02 .052 .144 115.66 .029
.300 .300 .598E+03 .518E+02 .106 .180 92.51 .054
.400 .400 .840E+03 .892E+02 .177 .210 79.29 .084
.500 .500 .113E+04 .166E+03 .268 .230 70.48 .118
.600 .600 .145E+04 .256E+03 .377 .260 64.05 .156
.700 .700 .180E+04 .370E+03 .507 .282 59.09 .197
.800 .800 .218E+04 .512E+03 .659 .303 55.09 .242
.900 .900 .259E+04 .685E+03 .833 .322 51.78 .290
1.000 1.000 .303E+04 .891E+03 1.031 .340 48.97 .340
1.100 1.100 .350E+04 .113E+04 1.253 .358 46.55 .394
1.200 1.200 .400E+04 .141E+04 1.500 .375 44.43 .450
1.300 1.300 .453E+04 .173E+04 1.775 .392 42.56 .509
1.400 1.400 .509E+04 .210E+04 2.077 .408 40.88 .571
1.500 1.500 .569E+04 .251E+04 2.407 .423 39.37 .635
1.600 1.600 .631E+04 .297E+04 2.768 .439 38.01 .702
1.700 1.700 .697E+04 .348E+04 3.158 .453 36.76 .771
1.800 1.800 .765E+04 .405E+04\* 3.580 .468 35.61 .842
2.000 2.000 .291E+05 .171E+05\* 5.701 .196 84.93 .392

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002010 107.59 4.402 7.23 56.344 1.878 .304
OUTFLOW : ID= 1:002020 107.59 3.926 8.18 56.344 1.836 .375

100:0009-----
| DESIGN NASHYD | Area (ha)= 19.36 Curve Number (CN)=82.00
| 02:104 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.450
Unit Hyd Qpeak (cms) = .510
PEAK FLOW (cms) = .850 (i)
TIME TO PEAK (hrs) = 7.434
RUNOFF VOLUME (mm) = 61.161
TOTAL RAINFALL (mm) = 98.000
RUNOFF COEFFICIENT = .624
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0010-----
| DESIGN NASHYD | Area (ha)= 25.24 Curve Number (CN)=82.00
| 03:105 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.450
Unit Hyd Qpeak (cms) = .665
PEAK FLOW (cms) = 1.108 (i)
TIME TO PEAK (hrs) = 7.434
RUNOFF VOLUME (mm) = 61.161
TOTAL RAINFALL (mm) = 98.000
RUNOFF COEFFICIENT = .624
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0011-----
| ADD HYD ( 2030 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01: 2020 107.59 3.926 8.18 56.34 .000

+ID2 02:104	19.36	.850	7.43	61.16	.000	
+ID3 03:105	25.24	1.108	7.43	61.16	.000	
SUM 04:	2030	152.19	5.663	7.98	57.76	.000

1.800	1.800	.344E+04	.574E+04*	3.008	.393	19.07	.708
1.933	1.933	.786E+04	.141E+05*	3.971	.227	33.00	.439
2.067	2.067	.203E+05	.388E+05*	6.403	.142	52.79	.294
2.200	2.200	.407E+05	.829E+05*	11.177	.124	60.70	.272

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

100:0012-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN 04:002030	Number of SEGMENTS = 3
OUT< 01:002040	Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
	LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 3.0) ----->			
Distance	Elevation	Manning	
.00	2.20	.2000	
200.00	1.80	.2000 / .0850	Main Channel
202.75	.00	.0850	Main Channel
204.25	.00	.0850	Main Channel
207.00	1.80	.0850 / .2000	Main Channel
407.00	2.20	.2000	

<----- hydrograph -----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
INFLOW : ID= 4:002050	174.66	5.394	8.82	58.194	2.011	.168
OUTFLOW: ID= 1:002060	174.66	5.013	9.83	58.194	1.991	.181

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (cu.m.)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.112	.112	.940E+02	.882E+01	.016	.087	95.91	.010
.225	.225	.207E+03	.389E+02	.054	.129	64.45	.029
.337	.337	.340E+03	.957E+02	.110	.161	51.67	.054
.450	.450	.492E+03	.185E+03	.185	.188	44.34	.085
.562	.562	.664E+03	.311E+03	.280	.211	39.43	.119
.675	.675	.854E+03	.481E+03*	.397	.233	35.84	.157
.788	.788	.106E+04	.698E+03*	.537	.252	33.06	.199
.900	.900	.129E+04	.970E+03*	.700	.270	30.81	.243
1.013	1.013	.154E+04	.130E+04*	.888	.288	28.95	.291
1.125	1.125	.181E+04	.170E+04*	1.102	.304	27.37	.343
1.238	1.238	.210E+04	.216E+04*	1.344	.320	26.01	.397
1.350	1.350	.240E+04	.271E+04*	1.615	.336	24.81	.453
1.463	1.463	.273E+04	.333E+04*	1.916	.351	23.76	.513
1.575	1.575	.308E+04	.404E+04*	2.247	.365	22.82	.575
1.688	1.688	.344E+04	.484E+04*	2.611	.379	21.97	.640
1.800	1.800	.382E+04	.574E+04*	3.008	.393	21.19	.708
1.933	1.933	.424E+04	.674E+04*	3.437	.407	20.53	.776
2.067	2.067	.470E+04	.786E+04*	3.911	.422	19.94	.846
2.200	2.200	.520E+04	.911E+04*	4.433	.437	19.44	.916

100:0017-----

DESIGN NASHYD	Area (ha) = 6.60	Curve Number (CN)=82.00
02:EXT8 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .820	

Unit Hyd Qpeak (cms) = .307

PEAK FLOW (cms) = .443 (i)

TIME TO PEAK (hrs) = 6.718

RUNOFF VOLUME (mm) = 61.161

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

100:0018-----

DESIGN NASHYD	Area (ha) = 6.60	Curve Number (CN)=82.00
02:EXT8 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .820	

Unit Hyd Qpeak (cms) = .307

PEAK FLOW (cms) = .443 (i)

TIME TO PEAK (hrs) = 6.718

RUNOFF VOLUME (mm) = 61.161

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- hydrograph -----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
INFLOW : ID= 4:002030	152.19	5.663	7.98	57.755	2.026	.160
OUTFLOW: ID= 1:002040	152.19	4.915	9.05	57.755	1.984	.185

100:0019-----

DESIGN NASHYD	Area (ha) = 39.07	Curve Number (CN)=82.00
01:106 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= 1.630	

Unit Hyd Qpeak (cms) = .916

PEAK FLOW (cms) = 1.567 (i)

TIME TO PEAK (hrs) = 7.634

RUNOFF VOLUME (mm) = 61.161

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0013-----

DESIGN NASHYD	Area (ha) = 15.67	Curve Number (CN)=82.00
02:108 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= 1.090	

Unit Hyd Qpeak (cms) = .549

PEAK FLOW (cms) = .854 (i)

TIME TO PEAK (hrs) = 7.018

RUNOFF VOLUME (mm) = 61.161

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0020-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN 01:106	Number of SEGMENTS = 3
OUT< 02:002080	Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000
	LENGTH = 250.00 (m)

<----- DATA FOR SECTION ( 5.0) ----->

Distance	Elevation	Manning	
.00	1.40	.2000	
200.00	1.00	.2000 / .1000	Main Channel
201.50	.00	.1000	Main Channel
203.50	.00	.1000	Main Channel
205.00	1.00	.1000 / .2000	Main Channel
405.00	1.40	.2000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (cu.m.)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.071	.071	.376E+02	.338E+01	.010	.064	65.43	.005
.143	.143	.791E+02	.151E+02	.031	.097	42.85	.014
.214	.214	.124E+03	.355E+02	.061	.123	33.82	.026
.286	.286	.173E+03	.661E+02	.101	.145	28.74	.041
.357	.357	.226E+03	.109E+03	.148	.164	25.41	.059
.429	.429	.283E+03	.162E+03*	.205	.181	23.02	.078
.500	.500	.344E+03	.229E+03*	.270	.197	21.20	.098
.571	.571	.408E+03	.311E+03*	.344	.211	19.75	.121
.643	.643	.476E+03	.409E+03*	.428	.225	18.56	.144
.714	.714	.548E+03	.522E+03*	.521	.237	17.56	.169
.786	.786	.624E+03	.654E+03*	.623	.249	16.71	.196
.857	.857	.704E+03	.805E+03*	.735	.261	15.96	.224
.929	.929	.788E+03	.975E+03*	.858	.272	15.31	.253
1.000	1.000	.875E+03	.117E+04*	.990	.283	14.73	.283
1.080	1.080	.117E+04	.256E+04*	1.270	.179	23.30	.193
1.160	1.160	.427E+04	.661E+04*	1.927	.113	36.37	.131
1.240	1.240	.837E+04	.138E+05*	3.185	.095	43.82	.118
1.320	1.320	.141E+05	.248E+05*	5.229	.093	44.86	.123
1.400	1.400	.214E+05	.399E+05*	8.222	.096	43.33	.135

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

100:0014-----

DESIGN NASHYD	Area (ha) = 6.80	Curve Number (CN)=82.00
03:105A DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .960	

Unit Hyd Qpeak (cms) = .271

PEAK FLOW (cms) = .407 (i)

TIME TO PEAK (hrs) = 6.884

RUNOFF VOLUME (mm) = 61.161

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- hydrograph -----> <-pipe / channel->

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL	
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)	
INFLOW : ID= 1:106	39.07	1.567	7.63	61.161	1.116	.141
OUTFLOW: ID= 2:002080	39.07	1.434	8.47	61.161	1.100	.156

100:0015-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN 04:002050	Number of SEGMENTS = 3
OUT< 01:002060	Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
	LENGTH = 450.00 (m)

<----- DATA FOR SECTION ( 4.0) ----->			
Distance	Elevation	Manning	
.00	2.20	.2000	
200.00	1.80	.2000 / .0850	Main Channel
202.75	.00	.0850	Main Channel
204.25	.00	.0850	Main Channel
207.00	1.80	.0850 / .2000	Main Channel
407.00	2.20	.2000	

100:0021-----

DESIGN NASHYD	Area (ha) = 21.08	Curve Number (CN)=81.00
01:EXT4 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= 1.830	

Unit Hyd Qpeak (cms) = .440

PEAK FLOW (cms) = .753 (i)

TIME TO PEAK (hrs) = 7.884

RUNOFF VOLUME (mm) = 59.663

TOTAL RAINFALL (mm) = 98.000

RUNOFF COEFFICIENT = .609

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (cu.m.)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)	D x v (m2/s)
.225	.225	.187E+03	.389E+02	.054	.129	58.01	.029
.337	.337	.306E+03	.957E+02	.110	.161	46.50	.054
.450	.450	.443E+03	.185E+03	.185	.188	39.90	.085
.562	.562	.597E+03	.311E+03*	.280	.211	35.49	.119
.675	.675	.769E+03	.481E+03*	.397	.233	32.26	.157
.788	.788	.958E+03	.698E+03*	.537	.252	29.75	.199
.900	.900	.116E+04	.970E+03*	.700	.270	27.73	.243
1.013	1.013	.139E+04	.130E+04*	.888	.288	26.06	.291
1.125	1.125	.163E+04	.170E+04*	1.102	.304	24.63	.343
1.238	1.238	.189E+04	.216E+04*	1.344	.320	23.41	.397
1.350	1.350	.216E+04	.271E+04*	1.615	.336	22.33	.453
1.463	1.463	.246E+04	.333E+04*	1.916	.351	21.38	.513
1.575	1.575	.277E+04	.404E+04*	2.247	.365	20.53	.575
1.688	1.688	.310E+04	.484E+04*	2.611	.379	19.77	.640

100:0022-----

DESIGN NASHYD	Area (ha) = 6.53	Curve Number (CN)=82.00
03:107 DT= 1.00	Ia (mm) = 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .820	



Unit Hyd Qpeak (cms)= .304
PEAK FLOW (cms)= .438 (i)
TIME TO PEAK (hrs)= 6.718
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0023-----
\*\*\*\*\*
\*# McGill Drain - Total Flow at Jefferson Boulevard
\*\*\*\*\*
| ADD HYD ( 2090 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:EXT4 | 21.08 | .753 | 7.88 | 59.66 | .000
+ID2 02: | 2080 | 39.07 | 1.434 | 8.47 | 61.16 | .000
+ID3 03:107 | 6.53 | .438 | 6.72 | 61.16 | .000
SUM 04: 2090 66.68 2.343 8.03 60.69 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0024-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN< 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000
LENGTH = 280.00 (m)

<----- DATA FOR SECTION ( 6.0 ) ----->
Distance Elevation Manning
.00 1.40 .2000
200.00 1.00 .2000 / .1000 Main Channel
200.00 1.00 .1000 Main Channel
203.50 .00 .1000 Main Channel
205.00 1.00 .1000 / .2000 Main Channel
405.00 1.40 .2000

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002090 66.68 2.343 8.03 60.687 1.143 .161
OUTFLOW: ID= 1:002100 66.68 2.229 8.97 60.687 1.131 .173

100:0025-----
| DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00
| 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp (hrs)= 1.520
Unit Hyd Qpeak (cms)= .372
PEAK FLOW (cms)= .627 (i)
TIME TO PEAK (hrs)= 7.518
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
100:0026-----
| ADD HYD ( 2110 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01: 2100 | 66.68 | 2.229 | 8.97 | 60.69 | .000
+ID2 02:EXT5 | 14.81 | .627 | 7.52 | 61.16 | .000
SUM 03: 2110 81.49 2.707 8.55 60.77 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0027-----
\*\*\*\*\*
\*# McGill Drain - Total Flow at Lappan Drain Confluence
\*\*\*\*\*
| ADD HYD ( 2120 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 03: 2110 | 81.49 | 2.707 | 8.55 | 60.77 | .000
+ID2 10: 2070 | 181.26 | 5.084 | 9.77 | 58.30 | .000
SUM 01: 2120 262.75 7.589 9.42 59.07 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
100:0028-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN< 01:002120 | Number of SEGMENTS = 3
| OUT< 02:002130 | Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000
LENGTH = 370.00 (m)

<----- DATA FOR SECTION ( 7.0 ) ----->
Distance Elevation Manning
.00 1.80 .2000
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .421E+02 .179E+01 .014 .090 51.82 .006
.143 .143 .842E+02 .358E+01 .043 .138 33.94 .020
.214 .214 .126E+03 .537E+02 .087 .174 26.78 .037
.286 .286 .170E+03 .730E+02 .142 .205 22.76 .059
.357 .357 .214E+03 .923E+02 .210 .232 20.12 .083
.429 .429 .258E+03 .112E+03 .290 .256 18.23 .110
.500 .500 .302E+03 .131E+03 .382 .278 16.79 .139
.571 .571 .346E+03 .150E+03 .487 .298 15.64 .171
.643 .643 .390E+03 .169E+03 .605 .318 14.70 .204
.714 .714 .434E+03 .188E+03 .736 .336 13.91 .240
.786 .786 .478E+03 .207E+03 .881 .353 13.23 .277
.857 .857 .522E+03 .226E+03 .1.040 .369 12.64 .316
.929 .929 .566E+03 .245E+03 .1.213 .385 12.12 .357
1.000 1.000 .610E+03 .264E+03 .1.401 .400 11.66 .400
1.080 1.080 .654E+03 .283E+03 .1.761 .248 18.81 .268
1.160 1.160 .698E+03 .302E+03 .2.505 .147 31.85 .170
1.240 1.240 .742E+03 .321E+03 .3.856 .115 40.54 .143
1.320 1.320 .786E+03 .340E+03 .5.997 .107 43.81 .141
1.400 1.400 .830E+03 .359E+03 .9.093 .106 43.88 .149

.280 .280 .240E+03 .606E+02 .107 .165 37.37 .046
.373 .373 .344E+03 .116E+03 .180 .193 31.94 .072
.467 .467 .460E+03 .194E+03 .271 .218 28.33 .102
.560 .560 .588E+03 .297E+03 .382 .240 25.70 .134
.653 .653 .728E+03 .429E+03 .513 .260 23.68 .170
.747 .747 .880E+03 .592E+03 .665 .280 22.05 .209
.840 .840 .104E+04 .790E+03 .840 .298 20.71 .250
.933 .933 .122E+04 .103E+04 .1.039 .315 19.58 .294
1.027 1.027 .141E+04 .130E+04 .1.262 .332 18.60 .340
1.120 1.120 .161E+04 .162E+04 .1.510 .348 17.74 .389
1.213 1.213 .182E+04 .199E+04 .1.785 .363 16.99 .440
1.307 1.307 .204E+04 .241E+04 .2.087 .378 16.32 .494
1.400 1.400 .228E+04 .287E+04 .2.418 .392 15.71 .549
1.500 1.500 .439E+04 .593E+04 .3.044 .257 24.02 .385
1.600 1.600 .102E+05 .147E+05 .4.365 .158 38.94 .253
1.700 1.700 .197E+05 .302E+05 .6.783 .127 48.42 .217
1.800 1.800 .329E+05 .534E+05 .10.633 .120 51.59 .215

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:002120 262.75 7.589 9.42 59.068 1.721 .126
OUTFLOW: ID= 2:002130 262.75 7.110 10.17 59.068 1.707 .127

100:0029-----
| DESIGN NASHYD | Area (ha)= 47.17 Curve Number (CN)=82.00
| 03:109 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp (hrs)= 1.100
Unit Hyd Qpeak (cms)= 1.638
PEAK FLOW (cms)= 2.553 (i)
TIME TO PEAK (hrs)= 7.034
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0030-----
| DESIGN NASHYD | Area (ha)= 24.11 Curve Number (CN)=80.00
| 04:EXT6 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp (hrs)= 1.520
Unit Hyd Qpeak (cms)= .606
PEAK FLOW (cms)= .968 (i)
TIME TO PEAK (hrs)= 7.518
RUNOFF VOLUME (mm)= 58.201
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .594

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0031-----
| ADD HYD ( 2140 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 02: 2130 | 262.75 | 7.110 | 10.17 | 59.07 | .000
+ID2 03:109 | 47.17 | 2.553 | 7.03 | 61.16 | .000
+ID3 04:EXT6 | 24.11 | .968 | 7.52 | 58.20 | .000
SUM 01: 2140 334.03 8.180 9.67 59.30 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0032-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN< 01:002140 | Number of SEGMENTS = 3
| OUT< 10:002150 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000
LENGTH = 370.00 (m)

<----- DATA FOR SECTION ( 7.0 ) ----->
Distance Elevation Manning
.00 1.80 .2000
200.00 1.40 .2000 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.093 .093 .681E+02 .278E+02 .012 .064 96.65 .006
.187 .187 .148E+03 .467E+02 .038 .096 64.26 .018
.280 .280 .240E+03 .114E+03 .078 .121 51.18 .034
.373 .373 .344E+03 .217E+03 .131 .141 43.73 .053
.467 .467 .460E+03 .363E+03 .198 .159 38.79 .074
.560 .560 .588E+03 .557E+03 .279 .175 35.19 .098
.653 .653 .728E+03 .804E+03 .374 .190 32.42 .124
.747 .747 .880E+03 .111E+04 .486 .204 30.20 .152
.840 .840 .104E+04 .148E+04 .614 .217 28.36 .183
.933 .933 .122E+04 .192E+04 .759 .230 26.81 .215
1.027 1.027 .141E+04 .244E+04 .1.021 .242 25.47 .249
1.120 1.120 .161E+04 .304E+04 .1.304 .254 24.30 .284
1.213 1.213 .182E+04 .373E+04 .1.704 .265 23.27 .322
1.307 1.307 .204E+04 .451E+04 .2.276 .276 22.34 .361
1.400 1.400 .228E+04 .539E+04 .3.044 .287 21.51 .401
1.500 1.500 .439E+04 .111E+05 .3.944 .191 32.30 .286
1.600 1.600 .102E+05 .278E+05 .5.244 .125 49.30 .200
1.700 1.700 .197E+05 .566E+05 .7.120 .107 57.42 .183
1.800 1.800 .329E+05 .1.00E+06 .9.415 .106 58.27 .191

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

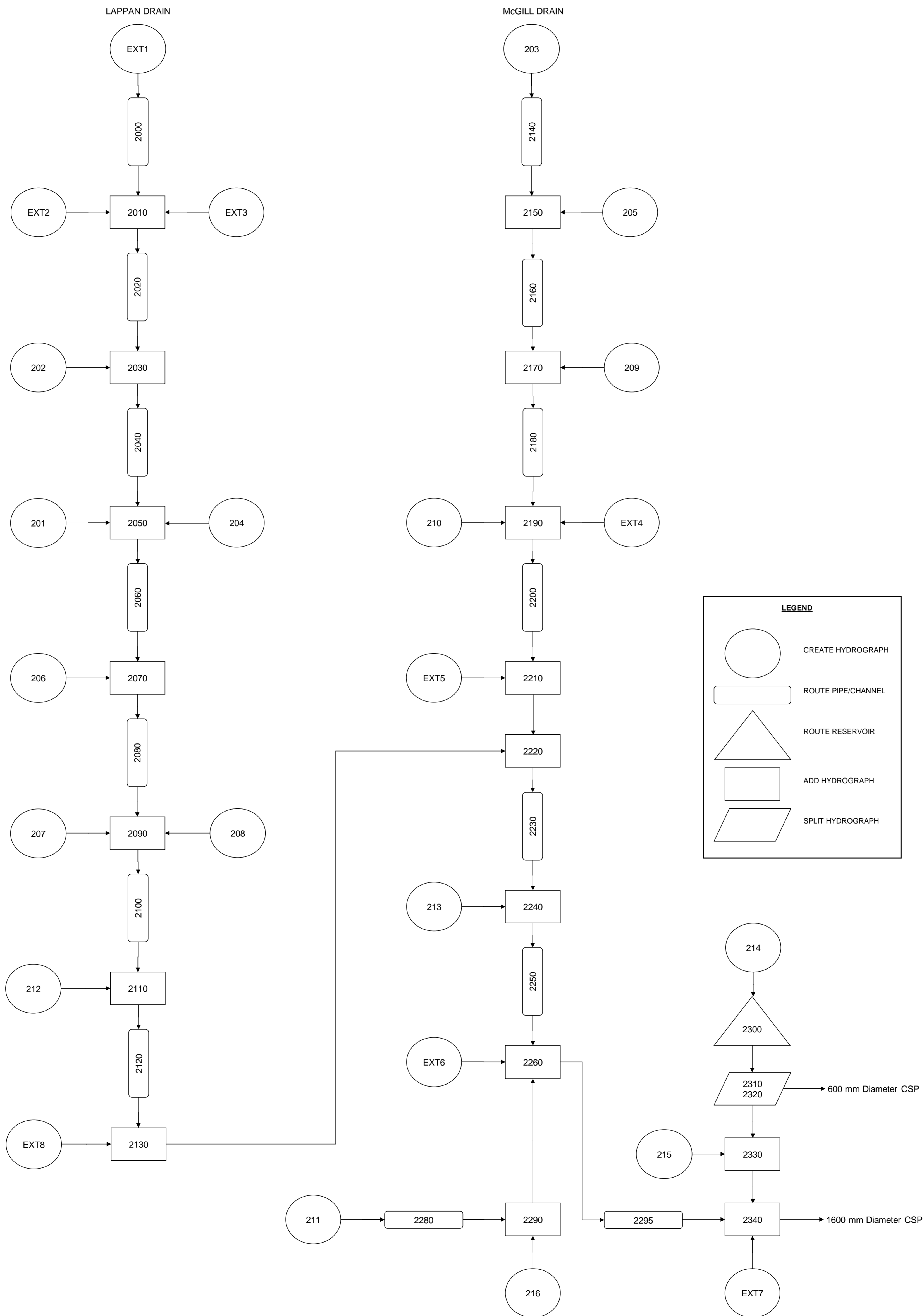
<--- hydrograph ---> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:002140 334.03 8.180 9.67 59.301 1.767 .106
OUTFLOW: ID= 10:002150 334.03 7.784 10.27 59.301 1.756 .107

100:0033-----
| DESIGN NASHYD | Area (ha)= 17.65 Curve Number (CN)=82.00
| 01:113 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp (hrs)= .910
Unit Hyd Qpeak (cms)= .741
PEAK FLOW (cms)= 1.099 (i)
TIME TO PEAK (hrs)= 6.818
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



Subject: Proposed Conditions SWMHYMO Schematic  
 Project: Windsor Solar Project  
 Project No.: 133560106  
 Client: Windsor Solar LP  
 Date: February 1, 2016





```

SSSS W W M M H H Y Y M M O O 999 999
S W W W M M H H Y Y M M O O 9 9 9 9
SSSS W W M M H H H H Y Y M M O O ## 9 9 9 9 Ver 4.05
S W W M M H H Y Y M M O O 9999 9999 Sept 2011
SSSS W W M M H H Y Y M M O O 9 9 9 9 # 4730904

StormWater Management Hydrologic Model 999 999

***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhyo@jfsa.com *****

***** Licensed user: Stantec Consulting Ltd. (Kitchener) *****
***** Kitchener SERIAL#:4730904 *****

***** PROGRAM ARRAY DIMENSIONS *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****

***** DETAILED OUTPUT *****
***** DATE: 2016-02-15 TIME: 14:15:11 RUN COUNTER: 000342 *****
***** Input filename: F:\WSP\60106PR3.dat *****
***** Output filename: F:\WSP\60106PR3.out *****
***** Summary filename: F:\WSP\60106PR3.sum *****
***** User comments: *****
***** 1: *****
***** 2: *****
***** 3: *****

001:0001-----
## Project Name: [Windsor Solar Project] Project Number: [1335-60106]
## Date : 02-10-2016
## Modeller : [NE]
## Company : Stantec Consulting Ltd. (London)
## License # : 4730904
##
## Proposed Conditions
## 25 mm Water Quality Event
## 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
##
** END OF RUN : 1

```

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV.TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m <sup>2</sup> /s)
141	141	140E+03	141E+02	0.08	0.89	131.37	.013
212	212	225E+03	340E+02	0.36	1.11	104.80	.024
282	282	321E+03	647E+02	0.60	1.30	89.71	.037
353	353	427E+03	108E+03	0.89	1.46	79.68	.052
424	424	544E+03	165E+03	1.25	1.61	72.40	.068
494	494	671E+03	237E+03	1.68	1.75	66.79	.086
565	565	809E+03	326E+03	2.17	1.87	62.29	.106
635	635	957E+03	434E+03	2.72	1.99	58.56	.127
706	706	112E+04	563E+03*	3.36	2.11	55.41	.149
776	776	129E+04	713E+03*	4.07	2.21	52.69	.172
847	847	146E+04	886E+03*	4.85	2.32	50.32	.196
918	918	166E+04	110E+04*	5.72	2.42	48.22	.222
988	988	186E+04	131E+04*	6.67	2.52	46.35	.249
1059	1059	207E+04	156E+04*	7.71	2.61	44.66	.277
1129	1129	229E+04	185E+04*	8.84	2.71	43.13	.306
1200	1200	252E+04	218E+04*	10.06	2.80	41.73	.335
1300	1300	366E+04	590E+04*	13.92	1.53	76.12	.199
1400	1400	172E+05	172E+05*	24.56	1.00	116.67	.140

X-VOLUME= Total X-section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

INFLOW : ID=	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
1:EXT1	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
42.26	.514	7.12	14.412	.870	.235	
OUTFLOW: ID= 2:002000	42.26	.396	7.67	14.411	.766	.220

002:0005-----

DESIGN NASHVD	Area	(ha)	Curve Number	(CN)=82.00
01:EXT2 DT= 1.00	Ia	(mm)= 1.500	# of Linear Res. (N)= 3.00	
U.H. Tp(hrs)= 1.270				

Unit Hyd Qpeak (cms)= .677  
PEAK FLOW (cms)= .348 (i)  
TIME TO PEAK (hrs)= 7.283  
RUNOFF VOLUME (mm)= 19.890  
TOTAL RAINFALL (mm)= 46.200  
RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0006-----

DESIGN NASHVD	Area	(ha)	Curve Number	(CN)=82.00
03:EXT3 DT= 1.00	Ia	(mm)= 1.500	# of Linear Res. (N)= 3.00	
U.H. Tp(hrs)= 1.110				

Unit Hyd Qpeak (cms)= 1.473  
PEAK FLOW (cms)= .732 (i)  
TIME TO PEAK (hrs)= 7.100  
RUNOFF VOLUME (mm)= 19.890  
TOTAL RAINFALL (mm)= 46.200  
RUNOFF COEFFICIENT = .431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

| START | Project dir.: F:\WSP\
| METOUT= 2 (output= METRIC)
| NRUN= 002
| NSTORM= 1
| l=128CS2.atm

002:0002-----
## Project Name: [Windsor Solar Project] Project Number: [1335-60106]
## Date : 02-10-2016
## Modeller : [NE]
## Company : Stantec Consulting Ltd. (London)
## License # : 4730904
##
## Proposed Conditions
## 25 mm Water Quality Event
## 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
##
*****

```

002:0007-----

ADD HYD ( 2010 )	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
(ha)	(cms)	(hrs)	(mm)	(cms)		
22.52	.348	7.28	19.89	.900		
42.26	.396	7.67	14.41	.000		
42.81	.732	7.10	19.89	.000		
SUM 04: 2010 107.59 1.436 7.30 17.74 .000						

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0008-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN: 04:002010	Number of SEGMENTS = 3
OUT: 01:002020	Slopes (%), CHANNEL= 1.700 FLOODPLAIN= .2000
LENGTH = 350.00 (m)	

002:0002-----

Distance	Elevation	Manning
.00	2.00	.2000
100.00	1.80	.0850 / .0850 Main Channel
102.75	.00	.0850 Main Channel
200	1.04	.25 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

002:0003-----

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV.TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m <sup>2</sup> /s)
100	100	578E+02	488E+01	0.16	0.96	60.50	.010
200	200	126E+03	212E+02	0.52	1.44	40.48	.029
300	300	206E+03	518E+02	1.06	1.80	32.38	.054
400	400	296E+03	993E+02	1.77	2.10	27.75	.084
500	500	396E+03	166E+03	2.68	2.36	24.67	.118
600	600	508E+03	256E+03*	3.77	2.60	22.42	.156
700	700	630E+03	370E+03*	5.07	2.82	20.68	.197
800	800	762E+03	512E+03*	6.59	3.03	19.28	.242
900	900	906E+03	685E+03*	8.33	3.22	18.12	.290
1000	1000	1066E+04	891E+03*	10.31	3.40	17.14	.340
1100	1100	122E+04	113E+04*	12.53	3.58	16.29	.394
1200	1200	140E+04	141E+04*	15.00	3.75	15.55	.450
1300	1300	159E+04	173E+04*	17.75	3.92	14.89	.509
1400	1400	178E+04	210E+04*	20.77	4.08	14.31	.571
1500	1500	199E+04	251E+04*	24.07	4.23	13.78	.635
1600	1600	221E+04	297E+04*	27.68	4.39	13.30	.702
1700	1700	244E+04	348E+04*	31.58	4.53	12.87	.771
1800	1800	268E+04	405E+04*	35.80	4.68	12.44	.842
2000	2000	102E+05	171E+05*	5.907	2.03	28.69	.407

X-VOLUME= Total X-section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

002:0004-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN: 01:EXT1	Number of SEGMENTS = 3
OUT: 02:002000	Slopes (%), CHANNEL= 1000 FLOODPLAIN= .2000
LENGTH = 700.00 (m)	

002:0009-----

DESIGN NASHVD	Area	(ha)	Curve Number	(CN)=72.00
02:202 DT= 1.00	Ia	(mm)= 1.500	# of Linear Res. (N)= 3.00	

U.H. Tp(hrs)= .970

Unit Hyd Qpeak (cms)	=	.411
PEAK FLOW (cms)	=	.135 (i)
TIME TO PEAK (hrs)	=	6.850
RUNOFF VOLUME (mm)	=	13.926
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0010

ADD HYD ( 2030)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01: 2020	107.59	1.376	7.52	17.74	.000
+ID2 02:202	10.43	.135	6.95	13.93	.000
SUM 03:	2030	118.02	1.492	7.48	17.40 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0011

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 03:002030	Number of SEGMENTS = 3
OUT< 01:002040	Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000
	LENGTH = 450.00 (m)

<----- DATA FOR SECTION ( 3.0) ----->

Distance	Elevation	Manning
.00	2.00	.0850
100.00	1.80	.2000 / .0850 Main Channel
102.75	.00	.0850 Main Channel
104.25	.00	.0850 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.100	.100	.744E+02	.486E+01	.016	.096	77.79	.010
.200	.200	.163E+03	.212E+02	.052	.144	52.05	.029
.300	.300	.264E+03	.518E+02	.106	.180	41.63	.054
.400	.400	.380E+03	.939E+02	.177	.210	35.68	.084
.500	.500	.509E+03	1.66E+03	.268	.236	31.72	.118
.600	.600	.653E+03	2.25E+03	.377	.260	28.82	.156
.700	.700	.809E+03	3.70E+03	.507	.282	26.59	.197
.800	.800	.980E+03	5.12E+03	.659	.303	24.78	.242
.900	.900	1.16E+04	6.85E+03	.833	.322	23.30	.290
1.000	1.000	1.36E+04	8.91E+03	1.031	.340	22.04	.340
1.100	1.100	1.57E+04	1.13E+04	1.253	.358	20.95	.394
1.200	1.200	1.80E+04	1.41E+04	1.500	.375	19.99	.450
1.300	1.300	2.04E+04	1.73E+04	1.775	.392	19.15	.509
1.400	1.400	2.29E+04	2.10E+04	2.077	.408	18.40	.571
1.500	1.500	2.56E+04	2.51E+04	2.407	.423	17.72	.635
1.600	1.600	2.84E+04	2.97E+04	2.768	.439	17.10	.702
1.700	1.700	3.13E+04	3.48E+04	3.158	.453	16.54	.771
1.800	1.800	3.44E+04	4.05E+04	3.580	.468	16.03	.842
2.000	2.000	4.31E+05	1.71E+05	5.907	.203	36.88	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- DATA FOR SECTION ( 5.0) ----->

Distance	Elevation	Manning
.00	2.00	.1400 / .0850 Main Channel
200.00	1.80	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .1400 Main Channel
407.00	2.20	.1400

002:0012

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:201 DT= 1.00	15.29	82.00
U.H. Tp(hrs)=	1.290	# of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .453

PEAK FLOW (cms)	=	.234 (i)
TIME TO PEAK (hrs)	=	7.300
RUNOFF VOLUME (mm)	=	19.890
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.431

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0013

DESIGN NASHYD	Area (ha)	Curve Number (CN)
03:204 DT= 1.00	10.88	72.00
U.H. Tp(hrs)=	.850	# of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .489

PEAK FLOW (cms)	=	.155 (i)
TIME TO PEAK (hrs)	=	6.817
RUNOFF VOLUME (mm)	=	13.926
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0014

ADD HYD ( 2050)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01: 2040	118.02	1.406	7.78	17.40	.000
+ID2 02:201	15.29	.234	7.30	19.89	.000
+ID3 03:204	10.88	.155	6.82	13.93	.000
SUM 04:	2050	144.19	1.729	7.67	17.40 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0015

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 04:002050	Number of SEGMENTS = 3
OUT< 01:002060	Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000
	LENGTH = 200.00 (m)

<----- DATA FOR SECTION ( 4.0) ----->

Distance	Elevation	Manning
.00	2.00	.1400
100.00	1.80	.1400 / .0850 Main Channel
102.75	.00	.0850 Main Channel
104.25	.00	.0850 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.100	.100	.331E+02	.486E+01	.016	.096	34.57	.010

.200	.200	.722E+02	.212E+02	.052	.144	23.13	.029
.300	.300	1.18E+03	.518E+02	.106	.180	18.50	.054
.400	.400	1.69E+03	.939E+02	.177	.210	15.86	.084
.500	.500	2.26E+03	1.66E+03	.268	.236	14.10	.118
.600	.600	2.90E+03	2.25E+03	.377	.260	12.81	.156
.700	.700	3.60E+03	3.70E+03	.507	.282	11.82	.197
.800	.800	4.38E+03	5.12E+03	.659	.303	11.02	.242
.900	.900	5.18E+03	6.85E+03	.833	.322	10.36	.290
1.000	1.000	6.06E+03	8.91E+03	1.031	.340	9.79	.340
1.100	1.100	7.00E+03	1.13E+04	1.253	.358	9.31	.394
1.200	1.200	8.00E+03	1.41E+04	1.500	.375	8.89	.450
1.300	1.300	9.06E+03	1.73E+04	1.775	.392	8.51	.509
1.400	1.400	1.02E+04	2.10E+04	2.077	.408	8.18	.571
1.500	1.500	1.14E+04	2.51E+04	2.407	.423	7.87	.635
1.600	1.600	1.28E+04	2.97E+04	2.768	.439	7.60	.702
1.700	1.700	1.39E+04	3.48E+04	3.158	.453	7.35	.771
1.800	1.800	1.53E+04	4.05E+04	3.580	.468	7.12	.842
2.000	2.000	.581E+04	.171E+05	6.114	2.10	15.84	.421

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (mm)	MAX VEL (m/s)
INFLOW : ID= 4:002050	144.19	1.729	7.67	17.403	1.283
OUTFLOW : ID= 1:002060	144.19	1.706	7.78	17.403	1.270

002:0016

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:206 DT= 1.00	4.78	72.00
U.H. Tp(hrs)=	.890	# of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .205

PEAK FLOW (cms)	=	.066 (i)
TIME TO PEAK (hrs)	=	6.850
RUNOFF VOLUME (mm)	=	13.926
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0017

ADD HYD ( 2070)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01: 2060	144.19	1.706	7.78	17.40	.000
+ID2 02:206	4.78	.066	6.85	13.93	.000
SUM 03:	2070	148.97	1.750	7.77	17.29 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0018

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 03:002070	Number of SEGMENTS = 3
OUT< 01:002080	Slopes (%), CHANNEL= 1200 FLOODPLAIN= .2000
	LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 5.0) ----->

Distance	Elevation	Manning
.00	2.20	.1400
200.00	1.80	.1400 / .0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .1400 Main Channel
407.00	2.20	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.112	.112	.940E+02	.892E+01	.016	.087	95.91	.010
.225	.225	2.07E+03	3.89E+02	.054	.129	64.45	.029
.337	.337	3.40E+03	9.57E+02	.110	.161	51.67	.054
.450	.450	4.92E+03	1.85E+03	.185	.188	44.34	.085
.562	.562	6.64E+03	3.11E+03	.280	.211	39.43	.119
.675	.675	8.54E+03	4.81E+03	.397	.233	35.84	.157
.788	.788	1.06E+04	6.98E+03	.537	.252	33.06	.199
.900	.900	1.29E+04	9.70E+03	.700	.270	30.81	.243
1.013	1.013	1.54E+04	1.30E+04	.898	.288	28.95	.291
1.125	1.125	1.81E+04	1.70E+04	1.102	.304	27.37	.343
1.238	1.238	2.10E+04	2.16E+04	1.344	.320	26.01	.397
1.350	1.350	2.40E+04	2.71E+04	1.615	.336	24.81	.453
1.463	1.463	2.73E+04	3.33E+04	1.916	.351	23.76	.513
1.575	1.575	3.08E+04	4.04E+04	2.247	.365	22.82	.575
1.688	1.688	3.44E+04	4.84E+04	2.611	.379	21.97	.640
1.800	1.800	3.82E+04	5.74E+04	3.008	.393	21.19	.708
1.933	1.933	4.24E+04	6.74E+04	3.433	.406	20.52	.777
2.067	2.067	4.70E+04	7.93E+04	3.900	.418	19.93	.848
2.200	2.200	5.20E+04	9.31E+04	4.420	.429	19.42	.921

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (mm)	MAX VEL (m/s)
INFLOW : ID= 3:002070	148.97	1.750	7.77	17.291	1.401
OUTFLOW : ID= 1:002080	148.97	1.617	8.10	17.291	1.344

002:0019

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:207 DT= 1.00	14.96	72.00
U.H. Tp(hrs)=	1.330	# of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .430

PEAK FLOW (cms)	=	.153 (i)
TIME TO PEAK (hrs)	=	7.383
RUNOFF VOLUME (mm)	=	13.926
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0020

DESIGN NASHYD	Area (ha)	Curve Number (CN)
03:208 DT= 1.00	7.92	72.00
U.H. Tp(hrs)=	1.110	# of Linear Res. (N)= 3.00

Unit Hyd Qpeak (cms)= .273

PEAK FLOW (cms)	=	.093 (i)
TIME TO PEAK (hrs)	=	7.117
RUNOFF VOLUME (mm)	=	13.926
TOTAL RAINFALL (mm)	=	46.200
RUNOFF COEFFICIENT	=	.301

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0021-----
#*****
# Lappan Drain - Total Flow at Jefferson Boulevard
#*****
| ADD HYD ( 2090 ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
|-----|-----|-----|-----|-----|-----|
| IN> 01: 2080   | 148.97 | 1.617 | 8.10 | 17.29 | .000
| +ID2 02:207   | 14.96  | .153  | 7.38 | 13.93 | .000
| +ID3 03:208   | 7.92   | .093  | 7.12 | 13.93 | .000
|-----|-----|-----|-----|-----|
| SUM 04: 2090 | 171.85 | 1.820 | 8.08 | 16.84 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0022-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= 1200 FLOODPLAIN=.2000
|-----|-----|
| LENGTH = 130.00 (m)

```

<----- DATA FOR SECTION ( 6.0 ) ----->

Distance	Elevation	Manning
.00	2.20	1.400
200.00	1.80	.1400 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.112	1.12	.245E+02	.882E+01	.016	.087	24.94	.010
.225	.225	.539E+02	.389E+02	.054	.129	16.76	.029
.337	.337	.884E+02	.957E+02	.110	.161	13.43	.054
.450	.450	.128E+03	.185E+03	.185	.188	11.53	.085
.562	.562	.173E+03	.311E+03	.280	.211	10.25	.119
.675	.675	.222E+03	.481E+03	.397	.233	9.32	.157
.788	.788	.277E+03	.698E+03	.537	.252	8.59	.199
.900	.900	.336E+03	.970E+03	.700	.270	8.01	.243
1.013	1.013	.401E+03	.130E+04	.888	.288	7.53	.291
1.125	1.125	.471E+03	.170E+04	1.102	.304	7.12	.343
1.238	1.238	.545E+03	.216E+04	1.344	.320	6.76	.397
1.350	1.350	.625E+03	.271E+04	1.615	.336	6.45	.453
1.463	1.463	.710E+03	.333E+04	1.916	.351	6.18	.513
1.575	1.575	.800E+03	.404E+04	2.247	.365	5.93	.575
1.688	1.688	.892E+03	.484E+04	2.611	.379	5.71	.640
1.800	1.800	.994E+03	.574E+04	3.008	.393	5.51	.708
1.933	1.933	.227E+04	.141E+05	4.041	.231	9.37	.447
2.067	2.067	.586E+04	.388E+05	6.848	.152	14.26	.314
2.200	2.200	.118E+05	.829E+05	12.488	.138	15.69	.304

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
| AREA   QPEAK   TPEAK   R.V.   MAX DEPTH   MAX VEL
| (ha)   (cms)   (hrs)   (mm)   (m)         (m/s)
INFLOW : ID= 4:002090 171.85 1.820 8.08 16.843 1.427 .346
OUTFLOW : ID= 1:002100 171.85 1.807 8.10 16.843 1.421 .345

```

```

002:0023-----
| DESIGN NASHYD | Area (ha)= 4.95 Curve Number (CN)=73.00
| 02:212 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .480

```

```

Unit Hyd Qpeak (cms)= .394
PEAK FLOW (cms)= .107 (i)
TIME TO PEAK (hrs)= 6.367
RUNOFF VOLUME (mm)= 14.411
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .312

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0024-----
| ADD HYD ( 2110 ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
|-----|-----|-----|-----|-----|
| IN> 01:2100   | 171.85 | 1.807 | 8.10 | 16.84 | .000
| +ID2 02:212   | 4.95   | .107 | 6.37 | 14.41 | .000
|-----|-----|-----|-----|-----|
| SUM 03: 2110 | 176.80 | 1.829 | 8.10 | 16.78 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0025-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002110 | Number of SEGMENTS = 3
| OUT< 01:002120 | Slopes (%), CHANNEL= 1200 FLOODPLAIN=.2000
|-----|-----|
| LENGTH = 330.00 (m)

```

<----- DATA FOR SECTION ( 7.0 ) ----->

Distance	Elevation	Manning
.00	2.20	1.400
200.00	1.80	.1400 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.112	1.12	.621E+02	.882E+01	.016	.087	63.30	.010
.225	.225	.137E+03	.389E+02	.054	.129	42.54	.029
.337	.337	.224E+03	.957E+02	.110	.161	34.10	.054
.450	.450	.325E+03	.185E+03	.185	.188	29.26	.085
.562	.562	.438E+03	.311E+03	.280	.211	26.02	.119
.675	.675	.564E+03	.481E+03	.397	.233	23.65	.157
.788	.788	.702E+03	.698E+03	.537	.252	21.82	.199
.900	.900	.854E+03	.970E+03	.700	.270	20.34	.243
1.013	1.013	.102E+04	.130E+04	.888	.288	19.11	.291
1.125	1.125	.119E+04	.170E+04	1.102	.304	18.06	.343
1.238	1.238	.138E+04	.216E+04	1.344	.320	17.16	.397
1.350	1.350	.159E+04	.271E+04	1.615	.336	16.38	.453
1.463	1.463	.180E+04	.333E+04	1.916	.351	15.68	.513
1.575	1.575	.203E+04	.404E+04	2.247	.365	15.06	.575
1.688	1.688	.227E+04	.484E+04	2.611	.379	14.50	.640
1.800	1.800	.252E+04	.574E+04	3.008	.393	13.99	.708
1.933	1.933	.577E+04	.141E+05	4.041	.231	23.78	.447
2.067	2.067	.149E+05	.388E+05	6.848	.152	36.20	.314
2.200	2.200	.298E+05	.829E+05	12.488	.138	39.84	.304

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
| AREA   QPEAK   TPEAK   R.V.   MAX DEPTH   MAX VEL
| (ha)   (cms)   (hrs)   (mm)   (m)         (m/s)
INFLOW : ID= 1:203 12.75 .165 6.95 13.926 .297 .226
OUTFLOW : ID= 2:002140 12.75 .137 7.43 13.926 .265 .211

```

```

INFLOW : ID= 3:002110 176.80 1.829 8.10 16.775 1.430 .346
OUTFLOW : ID= 1:002120 176.80 1.754 8.33 16.775 1.402 .343

```

```

002:0026-----
| DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00
| 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .820

```

```

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .141 (i)
TIME TO PEAK (hrs)= 6.750
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0027-----
#*****
# Lappan Drain - Total Flow at McGill Drain
#*****
| ADD HYD ( 2130 ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
|-----|-----|-----|-----|-----|
| IN> 01: 2120   | 176.80 | 1.754 | 8.10 | 16.78 | .000
| +ID2 02:EXT8   | 6.60   | .141 | 6.75 | 19.89 | .000
|-----|-----|-----|-----|-----|
| SUM 10: 2130 | 183.40 | 1.812 | 8.18 | 16.89 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0028-----
#*****
# McGill Drain
#*****
| DESIGN NASHYD | Area (ha)= 12.75 Curve Number (CN)=72.00
| 01:203 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .970

```

```

Unit Hyd Qpeak (cms)= .502
PEAK FLOW (cms)= .165 (i)
TIME TO PEAK (hrs)= 6.950
RUNOFF VOLUME (mm)= 13.926
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .301

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0029-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:203 | Number of SEGMENTS = 3
| OUT< 02:002140 | Slopes (%), CHANNEL= 3500 FLOODPLAIN=.2000
|-----|-----|
| LENGTH = 500.00 (m)

```

<----- DATA FOR SECTION ( 8.0 ) ----->

Distance	Elevation	Manning
.00	1.40	1.400
200.00	1.00	.1400 / .1000 Main Channel
201.50	.00	.1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / .2000 Main Channel
405.00	1.40	.2000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.071	.071	.753E+02	.154E+01	.015	.097	85.67	.007
.143	.143	.158E+03	.646E+01	.047	.149	56.11	.021
.214	.214	.249E+03	.152E+02	.094	.188	44.28	.040
.286	.286	.347E+03	.283E+02	.154	.221	37.63	.063
.357	.357	.453E+03	.462E+02	.227	.250	33.27	.089
.429	.429	.566E+03	.693E+02	.313	.276	30.14	.118
.500	.500	.687E+03	.982E+02	.413	.300	27.75	.150
.571	.571	.816E+03	.133E+03	.526	.322	25.85	.184
.643	.643	.953E+03	.175E+03	.654	.343	24.30	.220
.714	.714	.110E+04	.224E+03	.795	.362	22.99	.259
.786	.786	.125E+04	.290E+03	.952	.381	21.87	.299
.857	.857	.141E+04	.345E+03	1.123	.399	20.90	.342
.929	.929	.158E+04	.418E+03	1.310	.416	20.04	.386
1.000	1.000	.175E+04	.500E+03	1.513	.432	19.28	.432
1.080	1.080	.358E+04	.110E+04	1.913	.269	30.92	.291
1.160	1.160	.855E+04	.283E+04	2.777	.162	51.31	.188
1.240	1.240	.167E+05	.593E+04	4.375	.131	63.81	.162
1.320	1.320	.281E+05	.106E+05	6.931	.123	67.70	.162
1.400	1.400	.427E+05	.171E+05	10.642	.124	66.95	.174

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

```

<----- hydrograph -----> <-pipe / channel->
| AREA   QPEAK   TPEAK   R.V.   MAX DEPTH   MAX VEL
| (ha)   (cms)   (hrs)   (mm)   (m)         (m/s)
INFLOW : ID= 1:203 12.75 .165 6.95 13.926 .297 .226
OUTFLOW : ID= 2:002140 12.75 .137 7.43 13.926 .265 .211

```

```

002:0030-----
| DESIGN NASHYD | Area (ha)= 12.89 Curve Number (CN)=72.00
| 01:205 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|
| U.H. Tp(hrs)= .860

```

```

Unit Hyd Qpeak (cms)= .572
PEAK FLOW (cms)= .182 (i)
TIME TO PEAK (hrs)= 6.817
RUNOFF VOLUME (mm)= 13.926
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .301

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

002:0031-----
| ADD HYD ( 2150 ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
|-----|-----|-----|-----|-----|
| IN> 01:205   | 12.89 | 1.829 | 8.10 | 16.84 | .000
| +ID2 02: 2140 | 12.75 | .137 | 7.43 | 13.93 | .000
|-----|-----|-----|-----|-----|
| SUM 03: 2150 | 25.64 | .300 | 7.10 | 13.93 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

002:0032-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002150 | Number of SEGMENTS = 3
| OUT< 01:002160 | Slopes (%), CHANNEL= 0500 FLOODPLAIN=.2000
|-----|-----|
| LENGTH = 360.00 (m)

```



Table with columns: Distance, Elevation, Manning, 9.0. Rows show channel data from 200.00 to 405.00.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Rows show travel time data for various depths.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTE CHANNEL table with columns: Routing time step, Number of SEGMENTS, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DATA FOR SECTION ( 10.0 ) table with columns: Distance, Elevation, Manning. Rows show channel data from 200.00 to 405.00.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Rows show travel time data for various depths.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTE CHANNEL table with columns: Routing time step, Number of SEGMENTS, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTE CHANNEL table with columns: Routing time step, Number of SEGMENTS, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DATA FOR SECTION ( 11.0 ) table with columns: Distance, Elevation, Manning. Rows show channel data from 200.00 to 405.00.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Rows show travel time data for various depths.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTE CHANNEL table with columns: Routing time step, Number of SEGMENTS, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, U.H. Tp. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTE CHANNEL table with columns: Routing time step, Number of SEGMENTS, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.



Windsor Solar Energy Project

Proposed Conditions SWMHYMO

INFLOW : ID= 3:002260 (ha) (cms) (hrs) (mm) (m) (m/s)
OUTFLOW: ID=10:002295 333.75 3.146 8.37 16.822 1.563 .150
333.75 2.854 9.27 16.822 1.541 .163

ID1 03: 2320 .78 .036 6.52 16.00 .000
+ID2 05: 2340 374.37 3.104 9.08 16.90 .000
SUM 01: 2350 375.15 3.104 9.08 16.89 .000

002:0054-----
DESIGN NASHYD | Area (ha)= 17.47 Curve Number (CN)=76.00
| 03:214 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .600
Unit Hyd Qpeak (cms)= 1.112
PEAK FLOW (cms)= .366 (i)
TIME TO PEAK (hrs)= 6.517
RUNOFF VOLUME (mm)= 15.996
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .346
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
002:0062-----
\*\* END OF RUN : 4

002:0055-----
\*# Calculate culvert routing and flow split near eastern site boundary
\*# - Storage volumes calculated based on site survey
\*# - Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03: (214 ) |
| OUT<01: (002300) |
OUTFLOW STORAGE TABLE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | 1.130 .4600E+00
.150 .0000E+00 | 5.470 .8100E+00
.450 .0000E+00 | 83.090 .3400E+01
.820 .6500E-01 | .000 .0000E+00
ROUTING RESULTS
AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >03: (214 ) 17.47 .366 6.517 15.996
OUTFLOW<01: (002300) 17.47 .366 6.517 15.996
PEAK FLOW REDUCTION (Qout/Qin) (%) = 100.000
TIME SHIFT OF PEAK FLOW (min) = 00
MAXIMUM STORAGE USED (ha.m.) = .3322E-08

START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 005
NSTORM= 1
# 1=12scs5.stm
005:0002-----
Project Name: [Windsor Solar Project] Project Number: [1335-60106]
Date : 02-10-2016
Modeller : [ME]
Company : Stantec Consulting Ltd. (London)
License # : 4730904
Proposed Conditions
25 mm Water Quality Event
2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm

002:0056-----
| DIVERT HYD |
| INID=01 (002300) |

005:0002-----
| READ STORM | Filename: 5-yr scs 12 hr windsor
| Ptotal= 60.10 mm | Comments: 5-yr scs 12 hr windsor
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.202 | 3.50 2.404 | 6.50 10.818 | 9.50 2.404
1.00 1.202 | 4.00 2.404 | 7.00 4.808 | 10.00 1.202
1.50 1.202 | 4.50 3.606 | 7.50 3.606 | 10.50 1.202
2.00 1.202 | 5.00 4.808 | 8.00 3.606 | 11.00 1.202
2.50 2.404 | 5.50 7.212 | 8.50 2.404 | 11.50 1.202
3.00 2.404 | 6.00 54.090 | 9.00 2.404 | 12.00 1.202

Outflow / Inflow Relationships
Flow 02 + Flow 03 = Total
(cms) (cms) (cms)
.000 .000 .000
.150 .000 .150
.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090
NHYD AREA QPEAK TpeakDate\_hh:mm R.V. NFE WetHrs
(ha) (cms) (mm) (hrs)
IDin = 01:002300 17.47 .366 No\_date 6:31 15.996 1 13.
IDout= 02:002310 16.69 .320 No\_date 6:31 15.996 1 13.
IDout= 03:002320 .78 .036 No\_date 6:31 15.996 1 2.

005:0003-----
\*# LAPPAN DRAIN
DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
| 01:EXT1 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms)= 1.454
PEAK FLOW (cms)= .810 (i)
TIME TO PEAK (hrs)= 7.101
RUNOFF VOLUME (mm)= 22.511
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .375
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0057-----
DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=72.00
| 01:215 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .860
Unit Hyd Qpeak (cms)= .237
PEAK FLOW (cms)= .075 (i)
TIME TO PEAK (hrs)= 6.817
RUNOFF VOLUME (mm)= 13.926
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .301
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0004-----
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 01:EXT1 | Number of SEGMENTS = 3
| OUT< 02:002000 | Slopes (%), CHANNEL= .1000 FLOODPLAIN= .2000
LENGTH = 700.00 (m)
<----- DATA FOR SECTION ( 1.0) ----->
Distance Elevation Manning
.00 1.40 .2000
100.00 1.20 .2000 / .0850 Main Channel
.00 .0850 Main Channel
103.00 0.00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 .2000

002:0058-----
ADD HYD ( 2330) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms) (cms)
ID1 01:215 5.34 .075 6.82 13.93 .000
+ID2 02: 2310 16.69 .330 6.52 16.00 .000
SUM 04: 2330 22.03 .399 6.57 15.49 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV. TIME D x V
(m) (m) (cu.m.) (cu.m.) (m3/s) (m/s) (min) (m2/s)
.071 .071 .645E+02 .325E+01 .005 .059 197.27 .004
.141 .141 .140E+03 .141E+02 .018 .089 131.37 .013
.212 .212 .225E+03 .340E+02 .036 .111 104.80 .024
.282 .282 .321E+03 .647E+02 .060 .130 89.71 .037
.353 .353 .427E+03 .108E+03 .089 .146 79.68 .052
.424 .424 .546E+03 .165E+03 .125 .161 72.40 .068
.494 .494 .671E+03 .237E+03 .168 .175 66.79 .086
.565 .565 .809E+03 .326E+03 .217 .187 62.29 .106
.635 .635 .957E+03 .434E+03 .272 .199 58.56 .127
.706 .706 .112E+04 .563E+03 .336 .211 55.41 .149
.776 .776 .129E+04 .713E+03 .407 .221 52.69 .172
.847 .847 .146E+04 .886E+03 .485 .232 50.32 .196
.918 .918 .166E+04 .108E+04 .572 .242 48.22 .222
.988 .988 .186E+04 .131E+04 .667 .252 46.35 .249
1.059 1.059 .207E+04 .156E+04 .771 .261 44.66 .277
1.129 1.129 .229E+04 .185E+04 .884 .271 43.13 .306
1.200 1.200 .252E+04 .218E+04 1.006 .280 41.73 .335
1.300 1.300 .282E+04 .259E+04 1.192 .292 39.92 .371
1.400 1.400 .317E+04 .306E+04 1.456 .306 38.22 .400

002:0059-----
DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
| 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.470
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .257 (i)
TIME TO PEAK (hrs)= 7.517
RUNOFF VOLUME (mm)= 19.890
TOTAL RAINFALL (mm)= 46.200
RUNOFF COEFFICIENT = .431
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

002:0060-----
McGill Drain - Total Flow at Eastern WSP
ADD HYD ( 2340) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms) (cms)
ID1 01:EXT7 18.59 .257 7.52 19.89 .000
+ID2 04: 2330 22.03 .399 6.57 15.49 .000
+ID3 10: 2295 333.75 2.854 9.27 16.82 .000
SUM 05: 2340 374.37 3.104 9.08 16.90 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

hydrograph <--> <-channel-->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:EXT1 42.26 .810 7.10 22.511 1.083 .264
OUTFLOW: ID= 2:002000 42.26 .643 7.63 22.511 .971 .249

002:0061-----
ADD HYD ( 2350) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms) (cms)
ID1 01:EXT7 18.59 .257 7.52 19.89 .000
+ID2 04: 2330 22.03 .399 6.57 15.49 .000
+ID3 10: 2295 333.75 2.854 9.27 16.82 .000
SUM 05: 2340 374.37 3.104 9.08 16.90 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0005-----
DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00
| 01:EXT2 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.270
Unit Hyd Qpeak (cms)= .677
PEAK FLOW (cms)= .530 (i)
TIME TO PEAK (hrs)= 7.251
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.



```

005:0006-----
| DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00
| 03:EXT3 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|
| U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms)= 1.473
PEAK FLOW (cms)= 1.115 (i)
TIME TO PEAK (hrs)= 7.068
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
  
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0007-----
# Lappan Drain - Total Flow at Pilette Road
| ADD HYD ( 2010) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|
| ID1 01:EXT2 | 22.52 .530 7.25 30.03 .000
| +ID2 02:200 | 42.26 .643 7.63 22.51 .000
| +ID3 03:EXT3 | 42.81 1.115 7.07 30.03 .000
|-----|-----|-----|-----|
| SUM 04: 2010 107.59 2.235 7.27 27.08 .000
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

005:0008-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002010 | Number of SEGMENTS = 3
| OUT< 01:002020 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
|-----|-----|-----|
| LENGTH = 350.00 (m)
  
```

<----- DATA FOR SECTION ( 2.0) ----->

Distance	Elevation	Manning
.00	2.00	.2000
100.00	1.80	.2000 / .0850 Main Channel
102.75	.00	.0850 Main Channel
104.25	.00	.0850 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.100	1.00	.578E+02	.486E+01	.016	.096	60.50	.010
.200	1.00	.126E+03	.212E+02	.052	.144	40.48	.029
.300	1.00	.206E+03	.518E+02	.106	.180	32.38	.054
.400	1.00	.296E+03	.993E+02	.177	.210	27.75	.084
.500	1.00	.396E+03	.166E+03	.268	.236	24.67	.118
.600	1.00	.508E+03	.256E+03	.377	.260	22.42	.156
.700	1.00	.630E+03	.370E+03	.507	.282	20.68	.197
.800	1.00	.762E+03	.512E+03	.659	.303	19.28	.242
.900	1.00	.906E+03	.685E+03	.833	.322	18.12	.290
1.000	1.00	1.06E+04	.891E+03	1.031	.340	17.14	.340
1.100	1.00	1.22E+04	.113E+04	1.253	.358	16.29	.394
1.200	1.200	.140E+04	.141E+04	1.500	.375	15.55	.450
1.300	1.300	.159E+04	.173E+04	1.775	.392	14.89	.509
1.400	1.400	.178E+04	.210E+04	2.077	.408	14.31	.571
1.500	1.500	.199E+04	.251E+04	2.407	.423	13.78	.635
1.600	1.600	.221E+04	.297E+04	2.768	.439	13.30	.702
1.700	1.700	.244E+04	.348E+04	3.158	.453	12.87	.771
1.800	1.800	.268E+04	.405E+04	3.580	.468	12.46	.842
2.000	2.000	.102E+05	.171E+05	5.907	.203	28.69	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002010 107.59 2.235 7.27 27.076 1.448 .415
OUTFLOW : ID= 1:002020 107.59 2.150 7.47 27.076 1.420 .411
  
```

```

005:0009-----
| DESIGN NASHYD | Area (ha)= 10.43 Curve Number (CN)=72.00
| 02:202 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|
| U.H. Tp(hrs)= .970
Unit Hyd Qpeak (cms)= .411
PEAK FLOW (cms)= .214 (i)
TIME TO PEAK (hrs)= 6.934
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363
  
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0010-----
| ADD HYD ( 2030) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|
| ID1 01: 2020 107.59 2.150 7.47 27.08 .000
| +ID2 02:202 | 10.43 .214 6.93 21.82 .000
|-----|-----|-----|
| SUM 03: 2030 118.02 2.336 7.43 26.61 .000
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

005:0011-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002030 | Number of SEGMENTS = 3
| OUT< 01:002040 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
|-----|-----|
| LENGTH = 450.00 (m)
  
```

<----- DATA FOR SECTION ( 3.0) ----->

Distance	Elevation	Manning
.00	2.00	.2000
100.00	1.80	.2000 / .0850 Main Channel
102.75	.00	.0850 Main Channel
104.25	.00	.0850 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.100	1.00	.744E+02	.48E+01	.016	.096	77.79	.010
.200	1.00	.163E+03	.212E+02	.052	.144	52.05	.029
.300	1.00	.264E+03	.518E+02	.106	.180	41.63	.054
.400	1.00	.380E+03	.993E+02	.177	.210	35.68	.084
.500	1.00	.509E+03	.166E+03	.268	.236	31.72	.118
.600	1.00	.653E+03	.256E+03	.377	.260	28.82	.156
.700	1.00	.809E+03	.370E+03	.507	.282	26.59	.197
.800	1.00	.980E+03	.512E+03	.659	.303	24.79	.242
.900	1.00	1.16E+04	.685E+03	.833	.322	23.30	.290
1.000	1.000	.136E+04	.891E+03	1.031	.340	22.04	.340

1.100	1.100	.157E+04	.113E+04	1.253	.358	20.95	.394
1.200	1.200	.180E+04	.141E+04	1.500	.375	19.99	.450
1.300	1.300	.204E+04	.173E+04	1.775	.392	19.15	.509
1.400	1.400	.229E+04	.210E+04	2.077	.408	18.40	.571
1.500	1.500	.256E+04	.251E+04	2.407	.423	17.72	.635
1.600	1.600	.284E+04	.297E+04	2.768	.439	17.10	.702
1.700	1.700	.313E+04	.348E+04	3.158	.453	16.54	.771
1.800	1.800	.344E+04	.405E+04	3.580	.468	16.03	.842
2.000	2.000	.131E+05	.171E+05	5.907	.203	36.88	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 3:002030 118.02 2.336 7.43 26.611 1.478 .420
OUTFLOW : ID= 1:002040 118.02 2.216 7.65 26.611 1.443 .414
  
```

```

005:0012-----
| DESIGN NASHYD | Area (ha)= 15.29 Curve Number (CN)=82.00
| 02:201 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|
| U.H. Tp(hrs)= 1.290
Unit Hyd Qpeak (cms)= .453
  
```

```

PEAK FLOW (cms)= .356 (i)
TIME TO PEAK (hrs)= 7.284
RUNOFF VOLUME (mm)= 30.029
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
  
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0013-----
| DESIGN NASHYD | Area (ha)= 10.88 Curve Number (CN)=72.00
| 03:204 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|
| U.H. Tp(hrs)= .850
Unit Hyd Qpeak (cms)= .489
  
```

```

PEAK FLOW (cms)= .245 (i)
TIME TO PEAK (hrs)= 6.801
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363
  
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0014-----
| ADD HYD ( 2050) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|
| ID1 01: 2040 118.02 2.216 7.65 26.61 .000
| +ID2 02:201 | 15.29 .356 7.28 30.03 .000
| +ID3 03:204 | 10.88 .245 6.80 21.82 .000
|-----|-----|-----|
| SUM 04: 2050 144.19 2.726 7.58 26.61 .000
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

005:0015-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002050 | Number of SEGMENTS = 3
| OUT< 01:002060 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
|-----|-----|
| LENGTH = 200.00 (m)
  
```

<----- DATA FOR SECTION ( 4.0) ----->

Distance	Elevation	Manning
.00	2.00	.1400
100.00	1.80	.1400 / .0850 Main Channel
102.75	.00	.0850 Main Channel
104.25	.00	.0850 Main Channel
107.00	1.80	.0850 / .1400 Main Channel
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x v (m2/s)
.100	1.00	.331E+02	.48E+01	.016	.096	34.57	.010
.200	1.00	.722E+02	.212E+02	.052	.144	23.13	.029
.300	1.00	1.18E+03	.518E+02	.106	.180	18.50	.054
.400	1.00	1.69E+03	.993E+02	.177	.210	15.86	.084
.500	1.00	.226E+03	.166E+03	.268	.236	14.10	.118
.600	1.00	.290E+03	.256E+03	.377	.260	12.81	.156
.700	1.00	.360E+03	.370E+03	.507	.282	11.82	.197
.800	1.00	.436E+03	.512E+03	.659	.303	11.02	.242
.900	1.00	.518E+03	.685E+03	.833	.322	10.36	.290
1.000	1.000	.606E+03	.891E+03	1.031	.340	9.79	.340
1.100	1.100	.700E+03	.113E+04	1.253	.358	9.31	.394
1.200	1.200	.800E+03	.141E+04	1.500	.375	8.89	.450
1.300	1.300	.906E+03	.173E+04	1.775	.392	8.51	.509
1.400	1.400	1.02E+04	.210E+04	2.077	.408	8.18	.571
1.500	1.500	1.14E+04	.251E+04	2.407	.423	7.87	.635
1.600	1.600	1.26E+04	.297E+04	2.768	.439	7.60	.702
1.700	1.700	1.39E+04	.348E+04	3.158	.453	7.35	.771
1.800	1.800	1.53E+04	.405E+04	3.580	.468	7.12	.842
2.000	2.000	.581E+04	.171E+05	6.114	.210	15.84	.421

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002050 144.19 2.726 7.58 26.612 1.589 .437
OUTFLOW : ID= 1:002060 144.19 2.693 7.62 26.612 1.580 .435
  
```

```

005:0016-----
| DESIGN NASHYD | Area (ha)= 4.78 Curve Number (CN)=72.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|
| U.H. Tp(hrs)= .890
Unit Hyd Qpeak (cms)= .205
  
```

```

PEAK FLOW (cms)= .104 (i)
TIME TO PEAK (hrs)= 6.851
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363
  
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

005:0017-----
| ADD HYD ( 2070) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|
| ID1 01: 2060 144.19 2.693 7.62 26.61 .000
| +ID2 02:206 | 4.78 .104 6.85 21.82 .000
|-----|-----|-----|
| SUM 02: 2070 148.97 2.797 7.62 26.61 .000
  
```

SUM 03: 2070 148.97 2.769 7.62 26.46 .000

2.067 2.067 .586E+04 .388E+05\* 6.848 .152 14.26 .314
2.200 2.200 .118E+05 .829E+05\* 12.488 .138 15.69 .304

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

005:0018-----

ROUTE CHANNEL Routing time step (min) = 1.00
INP 03:002070 Number of SEGMENTS = 3
OUTK 01:002080 Slopes (%), CHANNEL= 1200 FLOODPLAIN= .2000
LENGTH = 500.00 (m)

<---- hydrograph ----> <-pipe / channel->
AREA OPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002090 171.85 2.906 7.92 25.841 1.771 .390
OUTFLOW: ID= 1:002100 171.85 2.784 7.70 25.841 2.047 .160

----- DATA FOR SECTION ( 5.0) -----
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .1400 Main Channel
407.00 2.20 .1400

005:0023-----
DESIGN NASHYD Area (ha)= 4.95 Curve Number (CN)=73.00
ID: 02:212 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .480

----- TRAVEL TIME TABLE -----
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .940E+02 .882E+01 .016 .087 95.91 .010
.225 .225 .181E+04 .170E+04 1.102 .304 27.37 .343
.337 .337 .340E+03 .957E+02 .110 .161 51.67 .054
.450 .450 .492E+03 .185E+03 .185 .188 44.34 .085
.562 .562 .664E+03 .311E+03 .280 .211 39.43 .119
.675 .675 .858E+03 .481E+03 .297 .233 35.84 .157
.788 .788 .106E+04 .698E+03\* .537 .252 33.06 .199
.900 .900 .129E+04 .970E+03\* .700 .270 30.81 .243
1.013 1.013 .154E+04 .130E+04\* .888 .288 28.95 .291
1.125 1.125 .181E+04 .170E+04\* 1.102 .304 27.37 .343
1.238 1.238 .210E+04 .216E+04\* 1.344 .320 26.01 .397
1.350 1.350 .240E+04 .271E+04\* 1.615 .336 24.81 .453
1.463 1.463 .273E+04 .333E+04\* 1.916 .351 23.76 .513
1.575 1.575 .308E+04 .404E+04\* 2.247 .365 22.82 .575
1.688 1.688 .344E+04 .484E+04\* 2.611 .379 21.97 .640
1.800 1.800 .382E+04 .574E+04\* 3.008 .393 21.19 .708
1.933 1.933 .427E+04 .674E+04\* 3.431 .408 20.52 .778
2.067 2.067 .478E+05 .829E+05\* 4.111 .425 19.42 .855
2.200 2.200 .532E+05 .829E+05\* 4.829 .452 18.52 .936

Unit Hyd Qpeak (cms)= .394
PEAK FLOW (cms)= .170 (l)
TIME TO PEAK (hrs)= 6.351
RUNOFF VOLUME (mm)= 22.511
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .375
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

005:0024-----
ADD HYD ( 2110) ID: NHYD AREA OPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (m) (m/s)
ID1 01: 2100 171.85 2.784 7.70 25.84 .000
+ID2 02:212 4.95 .170 6.35 22.51 .000
SUM 03: 2110 176.80 2.827 7.67 25.75 .000

----- DATA FOR SECTION ( 7.0) -----
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .2000 Main Channel
407.00 2.20 .2000

005:0025-----
ROUTE CHANNEL Routing time step (min) = 1.00
INP 03:002110 Number of SEGMENTS = 3
OUTK 01:002120 Slopes (%), CHANNEL= 1200 FLOODPLAIN= .2000
LENGTH = 330.00 (m)

005:0019-----
DESIGN NASHYD Area (ha)= 14.96 Curve Number (CN)=72.00
ID: 02:207 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.330

----- TRAVEL TIME TABLE -----
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.225 .225 .137E+03 .389E+02 .054 .087 63.30 .010
.337 .337 .224E+03 .957E+02 .110 .161 51.67 .054
.450 .450 .323E+03 .185E+03 .185 .188 29.26 .085
.562 .562 .430E+03 .311E+03 .280 .211 39.43 .119
.675 .675 .564E+03 .481E+03\* .297 .233 35.84 .157
.788 .788 .702E+03 .698E+03\* .537 .252 33.06 .199
.900 .900 .854E+03 .970E+03\* .700 .270 20.34 .243
1.013 1.013 .102E+04 .130E+04\* .888 .288 19.11 .291
1.125 1.125 .119E+04 .170E+04\* 1.102 .304 18.06 .343
1.238 1.238 .138E+04 .216E+04\* 1.344 .320 17.16 .397
1.350 1.350 .159E+04 .271E+04\* 1.615 .336 16.38 .453
1.463 1.463 .180E+04 .333E+04\* 1.916 .351 15.68 .513
1.575 1.575 .203E+04 .404E+04\* 2.247 .365 15.06 .575
1.688 1.688 .227E+04 .484E+04\* 2.611 .379 14.50 .640
1.800 1.800 .252E+04 .574E+04\* 3.008 .393 13.99 .708
1.933 1.933 .278E+04 .674E+04\* 3.431 .408 13.50 .778
2.067 2.067 .308E+05 .829E+05\* 4.041 .425 12.98 .847
2.200 2.200 .342E+05 .829E+05\* 4.829 .452 12.48 0.914

Unit Hyd Qpeak (cms)= .430
PEAK FLOW (cms)= .242 (l)
TIME TO PEAK (hrs)= 7.368
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0026-----
DESIGN NASHYD Area (ha)= 7.92 Curve Number (CN)=72.00
ID: 03:208 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110

005:0020-----
DESIGN NASHYD Area (ha)= 7.92 Curve Number (CN)=72.00
ID: 03:208 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110

Unit Hyd Qpeak (cms)= .273
PEAK FLOW (cms)= .147 (l)
TIME TO PEAK (hrs)= 7.101
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0021-----
DESIGN NASHYD Area (ha)= 14.96 Curve Number (CN)=72.00
ID: 02:207 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.330

005:0026-----
DESIGN NASHYD Area (ha)= 6.60 Curve Number (CN)=82.00
ID: 02:EXT8 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

005:0022-----
DESIGN NASHYD Area (ha)= 7.92 Curve Number (CN)=72.00
ID: 03:208 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .215 (l)
TIME TO PEAK (hrs)= 6.751
RUNOFF VOLUME (mm)= 30.028
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

005:0022-----
ROUTE CHANNEL Routing time step (min) = 1.00
INP 04:002090 Number of SEGMENTS = 3
OUTK 01:002100 Slopes (%), CHANNEL= 1200 FLOODPLAIN= .2000
LENGTH = 130.00 (m)

<---- hydrograph ----> <-pipe / channel->
AREA OPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 3:002110 176.80 2.827 7.67 25.747 1.749 .387
OUTFLOW: ID= 1:002120 176.80 2.609 8.63 25.747 1.688 .379

----- DATA FOR SECTION ( 6.0) -----
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .2000 Main Channel
407.00 2.20 .2000

005:0026-----
DESIGN NASHYD Area (ha)= 6.60 Curve Number (CN)=82.00
ID: 02:EXT8 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

----- TRAVEL TIME TABLE -----
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .245E+02 .882E+01 .016 .087 24.94 .010
.225 .225 .439E+02 .389E+02\* .054 .087 16.76 .029
.337 .337 .637E+02 .957E+02\* .110 .161 13.43 .054
.450 .450 .835E+02 .185E+03\* .185 .188 11.53 .085
.562 .562 .103E+03 .311E+03\* .280 .211 10.25 .119
.675 .675 .123E+03 .481E+03\* .397 .233 9.32 .157
.788 .788 .143E+03 .698E+03\* .537 .252 8.59 .199
.900 .900 .163E+03 .970E+03\* .700 .270 8.01 .243
1.013 1.013 .183E+03 .130E+04\* .888 .288 7.53 .291
1.125 1.125 .203E+03 .170E+04\* 1.102 .304 7.12 .343
1.238 1.238 .223E+03 .216E+04\* 1.344 .320 6.76 .397
1.350 1.350 .243E+03 .271E+04\* 1.615 .336 6.45 .453
1.463 1.463 .263E+03 .333E+04\* 1.916 .351 6.18 .513
1.575 1.575 .283E+03 .404E+04\* 2.247 .365 5.93 .575
1.688 1.688 .303E+03 .484E+04\* 2.611 .379 5.71 .640
1.800 1.800 .323E+03 .574E+04\* 3.008 .393 5.51 .708
1.933 1.933 .343E+03 .674E+04\* 3.431 .408 5.37 .778

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .215 (l)
TIME TO PEAK (hrs)= 6.751
RUNOFF VOLUME (mm)= 30.028
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0027-----
Lappan Drain - Total Flow at McGill Drain

005:0028-----
DESIGN NASHYD Area (ha)= 12.75 Curve Number (CN)=72.00
ID: 01:203 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .970

Unit Hyd Qpeak (cms)= .502
PEAK FLOW (cms)= .261 (l)
TIME TO PEAK (hrs)= 6.934
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0029-----
ROUTE CHANNEL Routing time step (min) = 1.00
IN> 01:203 Number of SEGMENTS = 3
OUT< 02:002140 Slopes (%), CHANNEL= .3500 FLOODPLAIN= .2000
LENGTH = 500.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show channel profile data from 200.00 to 405.00.

TRAVEL TIME TABLE

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show travel time data for various depths.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

Hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows show peak flow data for inflow and outflow.

005:0030-----
DESIGN NASHYD Area (ha)= 12.89 Curve Number (CN)=72.00
01:205 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .860

Unit Hyd Qpeak (cms)= .572
PEAK FLOW (cms)= .288 (1)
TIME TO PEAK (hrs)= 6.818
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0031-----
ADD HYD ( 2150) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01:205 2150 25.64 486 7.07 21.82 .000
SUM 03: 2150 25.64 486 7.07 21.82 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0032-----
ROUTE CHANNEL Routing time step (min) = 1.00
IN> 03:002150 Number of SEGMENTS = 3
OUT< 01:002160 Slopes (%), CHANNEL= .0500 FLOODPLAIN= .2000
LENGTH = 360.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show channel profile data for section 03:002150.

TRAVEL TIME TABLE

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show travel time data for various depths.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows show peak flow data for inflow and outflow.

005:0033-----
DESIGN NASHYD Area (ha)= 15.50 Curve Number (CN)=72.00
02:209 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .970

Unit Hyd Qpeak (cms)= .610
PEAK FLOW (cms)= .317 (1)

TIME TO PEAK (hrs)= 6.934
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0034-----
ADD HYD ( 2170) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2160 25.64 .392 7.33 21.82 .000
+ID2 02:209 15.50 .317 6.93 21.82 .000
SUM 03: 2170 41.14 .690 7.22 21.82 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0035-----
ROUTE CHANNEL Routing time step (min) = 1.00
IN> 03:002170 Number of SEGMENTS = 3
OUT< 01:002180 Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000
LENGTH = 250.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show channel profile data for section 03:002170.

TRAVEL TIME TABLE

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show travel time data for various depths.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows show peak flow data for inflow and outflow.

005:0036-----
DESIGN NASHYD Area (ha)= 7.27 Curve Number (CN)=82.00
02:210 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

Unit Hyd Qpeak (cms)= .339
PEAK FLOW (cms)= .237 (1)
TIME TO PEAK (hrs)= 6.751
RUNOFF VOLUME (mm)= 30.028
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0037-----
DESIGN NASHYD Area (ha)= 21.08 Curve Number (CN)=80.00
03:EXT4 DT= 1.00 Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.830

Unit Hyd Qpeak (cms)= .440
PEAK FLOW (cms)= .350 (1)
TIME TO PEAK (hrs)= 7.951
RUNOFF VOLUME (mm)= 28.124
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .468

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0038-----
# McGill Drain - Total Flow at Jefferson Boulevard

ADD HYD ( 2190) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2180 41.14 .650 7.38 21.82 .000
+ID2 02:210 7.27 .237 6.75 30.03 .000
+ID3 03:EXT4 21.08 .350 7.95 28.12 .000
SUM 04: 2190 69.49 1.158 7.35 24.59 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0039-----
ROUTE CHANNEL Routing time step (min) = 1.00
IN> 04:002190 Number of SEGMENTS = 3
OUT< 01:002200 Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000
LENGTH = 280.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show channel profile data for section 04:002190.

TRAVEL TIME TABLE

Table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show travel time data for various depths.

Table with 7 columns: ID, Area, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows include design points 286 through 1400.

Summary table for ID: NHYD, Area, QPEAK, TPEAK, R.V., DWF. Includes sub-sections for ID1 and ID2.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

DATA FOR SECTION ( 13.0 ) table with columns: Distance, Elevation, Manning. Rows show channel characteristics at various elevations.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for INFLOW and OUTFLOW.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x v. Rows show travel time for various depths.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

Summary table for ID: NHYD, Area, QPEAK, TPEAK, R.V., DWF.

hydrograph table with columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for INFLOW and OUTFLOW.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTING table with columns: ROUTE CHANNEL, IN, OUTF, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DATA FOR SECTION ( 12.0 ) table with columns: Distance, Elevation, Manning. Rows show channel characteristics.

ROUTING table with columns: ROUTE CHANNEL, IN, OUTF, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

ROUTING table with columns: ROUTE CHANNEL, IN, OUTF, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DATA FOR SECTION ( 15.0 ) table with columns: Distance, Elevation, Manning. Rows show channel characteristics.

ROUTING table with columns: ROUTE CHANNEL, IN, OUTF, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x v.

ROUTING table with columns: ROUTE CHANNEL, IN, OUTF, SLOPES, CHANNEL, FLOODPLAIN, LENGTH.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area, Curve Number, # of Linear Res. Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.



```

005:0050-----
| DESIGN NASHYD | Area (ha)= 10.57 Curve Number (CN)=72.00
| 03:216 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|-----|-----|
| U.H. Tp(hrs)= 1.210

Unit Hyd Qpeak (cms)= .334

PEAK FLOW (cms)= .184 (i)
TIME TO PEAK (hrs)= 7.218
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0051-----
| ADD HYD ( 2290) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|-----|
| ID1 03:216 | 10.57 .184 7.22 21.82 .000
|+ID2 04: | 2280 14.49 .367 7.32 30.03 .000
|-----|-----|-----|-----|-----|-----|
| SUM 05: | 2290 25.06 .550 7.28 26.57 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

```

005:0052-----
| ADD HYD ( 2260) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|-----|
| ID1 01: | 2250 284.58 3.824 8.97 25.55 .000
|+ID2 02:EXT6 | 24.11 .461 7.57 28.12 .000
|+ID3 05: | 2290 25.06 .550 7.28 26.57 .000
|-----|-----|-----|-----|-----|-----|
| SUM 03: | 2260 333.75 4.483 8.52 25.82 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

```

005:0053-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 01:002260 | Number of SEGMENTS = 3
| OUT< 10:002295 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000
|-----|-----|-----|-----|-----|-----|
| LENGTH = 370.00 (m)

<----- DATA FOR SECTION ( 14.0) ----->
Distance Elevation Manning
.00 1.80 1.400
200.00 1.40 1.400 / .0850 Main Channel
202.60 1.00 0.850 Main Channel
204.40 1.00 0.850 Main Channel
207.00 1.40 0.850 / .2000 Main Channel
407.00 1.80 2.000

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.093 .093 .481E+02 .107E+02 .012 .064 96.65 .006
.187 .187 .148E+03 .467E+02 .038 .096 64.26 .018
.280 .280 .240E+03 .114E+03 .078 .121 51.18 .034
.373 .373 .344E+03 .217E+03* .131 .141 43.73 .053
.467 .467 .462E+03 .363E+03* .198 .159 38.79 .074
.560 .560 .588E+03 .557E+03* .279 .175 35.19 .098
.653 .653 .728E+03 .804E+03* .374 .190 32.42 .124
.747 .747 .880E+03 .111E+04* .486 .204 30.20 .152
.840 .840 .104E+04 .149E+04* .614 .217 28.36 .183
.933 .933 .122E+04 .192E+04* .759 .230 26.81 .215
1.027 1.027 .141E+04 .244E+04* .921 .242 25.47 .249
1.120 1.120 .161E+04 .304E+04* 1.103 .254 24.30 .284
1.213 1.213 .182E+04 .373E+04* 1.304 .265 23.27 .322
1.307 1.307 .204E+04 .451E+04* 1.524 .276 22.34 .361
1.400 1.400 .228E+04 .539E+04* 1.766 .287 21.51 .401
1.500 1.500 .439E+04 .111E+05* 2.297 .194 31.84 .290
1.600 1.600 .102E+05 .278E+05* 3.654 .133 46.51 .212
1.700 1.700 .197E+05 .566E+05* 6.329 .119 51.90 .202
1.800 1.800 .329E+05 .100E+06* 10.726 .121 51.14 .217

```

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 3:002260 333.75 4.483 8.52 25.816 1.631 .128
OUTFLOW : ID=10:002295 333.75 4.087 9.58 25.816 1.616 .130

```

```

005:0054-----
| DESIGN NASHYD | Area (ha)= 17.47 Curve Number (CN)=76.00
| 03:214 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|-----|-----|
| U.H. Tp(hrs)= .600

Unit Hyd Qpeak (cms)= 1.112

PEAK FLOW (cms)= .572 (i)
TIME TO PEAK (hrs)= 6.501
RUNOFF VOLUME (mm)= 24.738
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .412

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0055-----
*****
## Calculate culvert routing and flow split near eastern site boundary
## - Storage volumes calculated based on site survey
## - Discharges calculated based on the 600 mm diameter CSP and 1500 mm
## diameter CSP capacities
*****
Requested routing time step = 1.0 min.
| ROUTE RESERVOIR |
| IN:03:(214 ) |
| OUT<01:(002300) |
|-----|-----|-----|-----|-----|-----|
| OUTFLOW STORAGE | OUTFLOW STORAGE |
| (cms) (ha.m.) | (cms) (ha.m.) |
| .000 .000E+00 | 1.130 .4600E+00 |
| .150 .0000E+00 | 5.470 .8100E+00 |
| .450 .0000E+00 | 83.090 .3400E+01 |
| .820 .6500E-01 | .000 .0000E+00 |

ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >03: (214 ) 17.47 .572 6.501 24.738
OUTFLOW<01: (002300) 17.47 .519 6.784 24.754

PEAK FLOW REDUCTION [Qout/Qin] (%) = 90.773
TIME SHIFT OF PEAK FLOW (min)= 17.00
MAXIMUM STORAGE USED (ha.m.)=.1212E-01

```

```

005:0056-----
| DIVERT HYD |

```

```

| INID=01 (002300)|
Outflow / Inflow Relationships
Flow 02 + Flow 03 = Total
(cms) (cms) (cms)
.000 .000 .000
.150 .000 .150
.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090

```

```

NHYD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
(ha) (cms) (hrs) (mm) (hrs)
IDin = 01:002300 17.47 .519 No_date 6:47 24.754 184 11.
IDout= 02:002310 16.14 .452 No_date 6:47 24.754 184 11.
IDout= 03:002260 1.33 .067 No_date 6:47 24.754 87 3.

```

```

005:0057-----
| DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=72.00
| 01:215 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|-----|-----|
| U.H. Tp(hrs)= .860

Unit Hyd Qpeak (cms)= .237

PEAK FLOW (cms)= .119 (i)
TIME TO PEAK (hrs)= 6.818
RUNOFF VOLUME (mm)= 21.820
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .363

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0058-----
| ADD HYD ( 2330) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|-----|
| ID1 01:215 | 5.34 .119 6.82 21.82 .000
|+ID2 02: | 2310 16.14 .452 6.78 24.75 .000
|-----|-----|-----|-----|-----|-----|
| SUM 04: | 2330 21.48 .571 6.78 24.02 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

```

005:0059-----
| DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
| 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|-----|-----|
| U.H. Tp(hrs)= 1.470

Unit Hyd Qpeak (cms)= .483

PEAK FLOW (cms)= .391 (i)
TIME TO PEAK (hrs)= 7.484
RUNOFF VOLUME (mm)= 30.929
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .500

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0060-----
*****
## McGill Drain - Total Flow at Eastern WSP
*****
| ADD HYD ( 2340) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|-----|
| ID1 01:EXT7 | 18.59 .391 7.48 30.03 .000
|+ID2 04: | 2330 21.48 .571 6.78 24.02 .000
|+ID3 10: | 2295 333.75 4.087 9.58 25.82 .000
|-----|-----|-----|-----|-----|-----|
| SUM 05: | 2340 373.82 4.487 9.37 25.92 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

```

005:0061-----
*****
## AREA CHECK
*****
| ADD HYD ( 2350) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----|-----|-----|-----|-----|-----|
| ID1 03: | 2320 1.33 .067 6.78 24.75 .000
|+ID2 05: | 2340 373.82 4.487 9.37 25.92 .000
|-----|-----|-----|-----|-----|-----|
| SUM 01: | 2350 375.15 4.489 9.37 25.92 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

```

005:0062-----
| DESIGN NASHYD | Area (ha)= 17.47 Curve Number (CN)=76.00
| 03:214 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
|-----|-----|-----|-----|-----|-----|
| U.H. Tp(hrs)= .600

Unit Hyd Qpeak (cms)= 1.112

PEAK FLOW (cms)= .572 (i)
TIME TO PEAK (hrs)= 6.501
RUNOFF VOLUME (mm)= 24.738
TOTAL RAINFALL (mm)= 60.100
RUNOFF COEFFICIENT = .412

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

005:0062-----
** END OF RUN : 9

```

```

| START | Project dir.: F:\WSP\
|-----|-----|-----|-----|-----|-----|
| Rainfall dir.: F:\WSP\
TEERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
l=12scs10.stm

010:0002-----
## Project Name: [Windsor Solar Project] Project Number: [1335-60106]
## Date : 02-10-2016
## Modeller : [NE]
## Company : Stantec Consulting Ltd. (London)
## License # : 4730904
*****
## Proposed Conditions
## 25 mm Water Quality Event
## 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
*****

```

```

010:0002-----
| READ STORM | Filename: 10-yr scs 12 hr windsor
| Ptotal= 69.20 mm | Comments: 10-yr scs 12 hr windsor

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.384 | 3.50 2.768 | 6.50 12.456 | 9.50 2.768
1.00 1.384 | 4.00 2.768 | 7.00 5.536 | 10.00 1.384
1.50 1.384 | 4.50 4.152 | 7.50 4.152 | 10.50 1.384
2.00 1.384 | 5.00 5.536 | 8.00 4.152 | 11.00 1.384

```

2.50	2.768	5.50	8.304	8.50	2.768	11.50	1.384
3.00	2.768	6.00	62.280	9.00	2.768	12.00	1.384

010:0003-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00  
 | 01:EXT1 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= 1.110  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= 1.454  
 PEAK FLOW (cms)= 1.025 (i)  
 TIME TO PEAK (hrs)= 7.101  
 RUNOFF VOLUME (mm)= 28.354  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .410

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0004-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN> 01:EXT1 | Number of SEGMENTS = 3  
 | OUT< 02:002000 | Slopes (%), CHANNEL= 1000 FLOODPLAIN= .2000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | LENGTH = 700.00 (m)  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 <----- DATA FOR SECTION ( 1.0) ----->  
 Distance Elevation Manning  
 .00 1.40 .2000  
 100.00 1.20 .0850 Main Channel  
 101.80 .00 .0850 Main Channel  
 103.00 .00 .0850 Main Channel  
 104.80 1.20 .0850 / .2000 Main Channel  
 204.80 1.40 .2000

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .071 .141 .048E+02 .323E+01 .005 .059 197.27 .004  
 .141 .141 .140E+03 .141E+02 .018 .089 131.37 .013  
 .212 .212 .225E+03 .340E+02 .036 .111 104.80 .024  
 .282 .282 .321E+03 .647E+02 .060 .130 89.71 .037  
 .353 .353 .427E+03 1.08E+03 .089 .146 79.68 .052  
 .424 .424 .544E+03 1.65E+03 .125 .161 72.40 .068  
 .494 .494 .671E+03 2.37E+03 .168 .175 66.79 .086  
 .565 .565 .809E+03 3.24E+03 .217 .187 62.29 .106  
 .635 .635 .957E+03 4.34E+03 .272 .199 58.56 .127  
 .706 .706 .112E+04 .563E+03 .336 .211 55.41 .149  
 .776 .776 .129E+04 .713E+03 .407 .221 52.69 .172  
 .847 .847 .146E+04 .886E+03 .485 .232 50.32 .196  
 .918 .918 .166E+04 1.08E+04 .572 .242 48.22 .222  
 .988 .988 .186E+04 1.31E+04 .667 .252 46.35 .249  
 1.059 1.059 .207E+04 1.56E+04 .771 .261 44.66 .277  
 1.129 1.129 .229E+04 1.85E+04 .884 .271 43.13 .306  
 1.200 1.200 .252E+04 2.18E+04 1.006 .280 41.73 .335  
 1.300 1.300 .336E+04 2.59E+04 1.392 .353 37.12 .445  
 1.400 1.400 .472E+05 3.17E+05 2.456 .500 21.67 .610

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 1:EXT1 42.26 1.025 7.10 28.354 1.205 .269  
 OUTFLOW: ID= 2:002000 42.26 .829 7.53 28.354 1.095 .266

010:0005-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00  
 | 01:EXT2 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= 1.270  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= .677  
 PEAK FLOW (cms)= .650 (i)  
 TIME TO PEAK (hrs)= 7.251  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0006-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00  
 | 03:EXT3 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= 1.110  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= 1.473  
 PEAK FLOW (cms)= 1.385 (i)  
 TIME TO PEAK (hrs)= 7.068  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0007-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN - Total Flow at Pilette Road  
 #\*\*\*\*\*  
 | ADD HYD ( 2010) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | ID1 01:EXT2 22.52 .650 7.25 37.12 .000  
 | +ID2 02: 2000 42.26 .829 7.53 28.35 .000  
 | +ID3 03:EXT3 42.81 1.385 7.07 37.12 .000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | SUM 04: 2010 107.59 2.808 7.28 33.68 .000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0008-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN> 04:002010 | Number of SEGMENTS = 3  
 | OUT< 01:002020 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= 2000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | LENGTH = 350.00 (m)  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 <----- DATA FOR SECTION ( 2.0) ----->  
 Distance Elevation Manning  
 .00 2.00 .2000  
 100.00 1.80 .2000 / .0850 Main Channel  
 102.75 .00 .0850 Main Channel  
 104.25 .00 .0850 Main Channel  
 107.00 1.80 .0850 / .1400 Main Channel  
 207.00 2.00 .1400

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .071 .141 .048E+02 .323E+01 .005 .059 197.27 .004  
 .141 .141 .140E+03 .141E+02 .018 .089 131.37 .013  
 .212 .212 .225E+03 .340E+02 .036 .111 104.80 .024  
 .282 .282 .321E+03 .647E+02 .060 .130 89.71 .037  
 .353 .353 .427E+03 1.08E+03 .089 .146 79.68 .052  
 .424 .424 .544E+03 1.65E+03 .125 .161 72.40 .068  
 .494 .494 .671E+03 2.37E+03 .168 .175 66.79 .086  
 .565 .565 .809E+03 3.24E+03 .217 .187 62.29 .106  
 .635 .635 .957E+03 4.34E+03 .272 .199 58.56 .127  
 .706 .706 .112E+04 .563E+03 .336 .211 55.41 .149  
 .776 .776 .129E+04 .713E+03 .407 .221 52.69 .172  
 .847 .847 .146E+04 .886E+03 .485 .232 50.32 .196  
 .918 .918 .166E+04 1.08E+04 .572 .242 48.22 .222  
 .988 .988 .186E+04 1.31E+04 .667 .252 46.35 .249  
 1.059 1.059 .207E+04 1.56E+04 .771 .261 44.66 .277  
 1.129 1.129 .229E+04 1.85E+04 .884 .271 43.13 .306  
 1.200 1.200 .252E+04 2.18E+04 1.006 .280 41.73 .335  
 1.300 1.300 .336E+04 2.59E+04 1.392 .353 37.12 .445  
 1.400 1.400 .472E+05 3.17E+05 2.456 .500 21.67 .610

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
100	.100	.578E+02	.486E+01	.016	.096	60.50	.010
200	.200	1.056E+03	2.12E+02	.052	.144	40.48	.029
300	.300	2.06E+03	5.18E+02	.106	.180	32.38	.054
400	.400	2.96E+03	9.93E+02	.177	.210	27.75	.084
500	.500	3.96E+03	1.66E+03	.268	.236	24.67	.118
600	.600	5.00E+03	2.56E+03	.377	.260	22.42	.156
700	.700	6.30E+03	3.70E+03	.507	.282	20.68	.197
800	.800	7.62E+03	5.12E+03	.659	.303	19.28	.242
900	.900	9.06E+03	6.85E+03	.833	.322	18.12	.290
1.000	1.000	1.05E+04	8.91E+03	1.031	.340	17.14	.340
1.100	1.100	1.22E+04	1.13E+04	1.253	.358	16.29	.394
1.200	1.200	1.40E+04	1.41E+04	1.500	.375	15.55	.450
1.300	1.300	1.59E+04	1.73E+04	1.775	.392	14.89	.509
1.400	1.400	1.78E+04	2.10E+04	2.077	.408	14.31	.571
1.500	1.500	1.99E+04	2.51E+04	2.407	.423	13.78	.635
1.600	1.600	2.21E+04	2.97E+04	2.768	.439	13.30	.702
1.700	1.700	2.44E+04	3.48E+04	3.158	.453	12.87	.771
1.800	1.800	2.68E+04	4.05E+04	3.580	.468	12.46	.842
2.000	2.000	3.17E+05	1.71E+05	5.907	.203	28.69	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 4:002010 107.59 2.808 7.28 33.680 1.610 .440  
 OUTFLOW: ID= 1:002020 107.59 2.710 7.45 33.680 1.578 .435

010:0009-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 10.43 Curve Number (CN)=72.00  
 | 02:202 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= .970  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= .411  
 PEAK FLOW (cms)= .271 (i)  
 TIME TO PEAK (hrs)= 6.934  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0010-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | ADD HYD ( 2030) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | ID1 01: 2020 107.59 2.710 7.45 33.680 .000  
 | +ID2 02:202 107.59 2.710 7.45 33.680 .000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | SUM 03: 2030 118.02 2.949 7.42 33.14 .000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0011-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN> 03:002030 | Number of SEGMENTS = 3  
 | OUT< 01:002040 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= 2000  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | LENGTH = 450.00 (m)  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 <----- DATA FOR SECTION ( 3.0) ----->  
 Distance Elevation Manning  
 .00 2.00 .2000  
 100.00 1.80 .2000 / .0850 Main Channel  
 102.75 .00 .0850 Main Channel  
 104.25 .00 .0850 Main Channel  
 107.00 1.80 .0850 / 1400 Main Channel  
 207.00 2.00 .1400

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .100 .100 .744E+02 4.86E+01 .016 .096 77.79 .010  
 .200 .200 1.63E+03 2.12E+02 .052 .144 52.05 .029  
 .300 .300 2.64E+03 5.18E+02 .106 .180 41.63 .054  
 .400 .400 3.80E+03 9.93E+02 .177 .210 35.68 .084  
 .500 .500 5.09E+03 1.66E+03 .268 .236 31.72 .118  
 .600 .600 6.53E+03 2.56E+03 .377 .260 28.82 .156  
 .700 .700 8.09E+03 3.70E+03 .507 .282 26.59 .197  
 .800 .800 9.80E+03 5.12E+03 .659 .303 24.79 .242  
 .900 .900 1.16E+04 6.85E+03 .833 .322 23.30 .290  
 1.000 1.000 1.36E+04 8.91E+03 1.031 .340 22.04 .340  
 1.100 1.100 1.57E+04 1.13E+04 1.253 .358 20.95 .394  
 1.200 1.200 1.80E+04 1.41E+04 1.500 .375 19.99 .450  
 1.300 1.300 2.04E+04 1.73E+04 1.775 .392 19.15 .509  
 1.400 1.400 2.29E+04 2.10E+04 2.077 .408 18.40 .571  
 1.500 1.500 2.56E+04 2.51E+04 2.407 .423 17.72 .635  
 1.600 1.600 2.84E+04 2.97E+04 2.768 .439 17.10 .702  
 1.700 1.700 3.13E+04 3.48E+04 3.158 .453 16.54 .771  
 1.800 1.800 3.44E+04 4.05E+04 3.580 .468 16.03 .842  
 2.000 2.000 4.13E+05 1.71E+05 5.907 .203 36.88 .407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\* Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 3:002030 118.02 2.949 7.42 33.136 1.646 .445  
 OUTFLOW: ID= 1:002040 118.02 2.798 7.58 33.136 1.608 .440

010:0012-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 15.29 Curve Number (CN)=82.00  
 | 02:203 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= 1.290  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= .453  
 PEAK FLOW (cms)= .442 (i)  
 TIME TO PEAK (hrs)= 7.268  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0013-----  
 #\*\*\*\*\*  
 # LAPPAN DRAIN  
 #\*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 10.88 Curve Number (CN)=72.00  
 | 03:204 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 | U.H. Tp(hrs)= .850  
 |-----|-----|-----|-----|-----|-----|-----|-----|  
 Unit Hyd Qpeak (cms)= .489  
 PEAK FLOW (cms)= .311 (i)  
 TIME TO PEAK (hrs)= 6.801  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0014-----
| ADD HYD ( 2050 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (cms)
| ID1 01: 2040 | 118.02 | 2.798 | 7.58 | 33.14 | .000
| +ID2 02:201 | 15.29 | .442 | 7.27 | 37.12 | .000
| +ID3 03:204 | 10.88 | .311 | 6.80 | 27.53 | .000
| SUM 04: 2050 | 144.19 | 3.448 | 7.55 | 33.14 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0015-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002050 | Number of SEGMENTS = 3
| OUT< 01:002060 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
| LENGTH = 200.00 (m)

```

```

<----- DATA FOR SECTION ( 4.0 ) ----->
Distance Elevation Manning
200.00 1.80 .1400 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .331E+02 .486E+01 .016 .096 34.57 .010
.200 .200 .722E+02 .212E+02 .052 .144 23.13 .029
.300 .300 .118E+03 .518E+02 .106 .180 18.50 .054
.400 .400 .169E+03 .993E+02* .177 .210 15.86 .084
.500 .500 .226E+03 .166E+03* .268 .236 14.10 .118
.600 .600 .290E+03 .256E+03* .377 .260 12.81 .156
.700 .700 .360E+03 .370E+03* .507 .282 11.82 .197
.800 .800 .436E+03 .512E+03* .659 .303 11.02 .242
.900 .900 .518E+03 .685E+03* .833 .322 10.36 .290
1.000 1.000 .606E+03 .891E+03* 1.031 .340 9.79 .340
1.100 1.100 .700E+03 .113E+04* 1.253 .358 9.31 .394
1.200 1.200 .800E+03 .141E+04* 1.500 .375 8.89 .450
1.300 1.300 .906E+03 .173E+04* 1.775 .392 8.51 .509
1.400 1.400 .102E+04 .210E+04* 2.077 .408 8.18 .571
1.500 1.500 .114E+04 .251E+04* 2.407 .423 7.87 .635
1.600 1.600 .126E+04 .297E+04* 2.768 .439 7.60 .702
1.700 1.700 .139E+04 .348E+04* 3.158 .453 7.35 .771
1.800 1.800 .153E+04 .405E+04* 3.580 .468 7.12 .842
2.000 2.000 .181E+04 .571E+05* 6.114 .210 15.84 .421

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002050 144.19 3.448 7.55 33.136 1.769 .463
OUTFLOW : ID= 1:002060 144.19 3.395 7.60 33.136 1.756 .461

```

```

010:0016-----
| DESIGN NASHYD | Area (ha)= 4.78 Curve Number (CN)=72.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .890

```

Unit Hyd Qpeak (cms)= .205

PEAK FLOW (cms)= .132 (1)

TIME TO PEAK (hrs)= 6.834

RUNOFF VOLUME (mm)= 27.531

TOTAL RAINFALL (mm)= 69.200

RUNOFF COEFFICIENT = .398

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0017-----
| ADD HYD ( 2070 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (cms)
| ID1 01: 2060 | 144.19 | 3.395 | 7.60 | 33.14 | .000
| +ID2 02:206 | 4.78 | .132 | 6.83 | 27.53 | .000
| SUM 03: 2070 | 148.97 | 3.492 | 7.58 | 32.96 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0018-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002070 | Number of SEGMENTS = 3
| OUT< 01:002080 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
| LENGTH = 500.00 (m)

```

```

<----- DATA FOR SECTION ( 5.0 ) ----->
Distance Elevation Manning
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .1400 Main Channel
407.00 2.20 .1400

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .940E+02 .892E+01 .016 .087 95.91 .010
.225 .225 .207E+03 .389E+02 .054 .129 64.45 .029
.337 .337 .340E+03 .957E+02 .110 .161 51.67 .054
.450 .450 .492E+03 .185E+03 .185 .188 44.34 .085
.562 .562 .646E+03 .313E+03 .280 .211 39.43 .119
.675 .675 .854E+03 .481E+03* .397 .233 35.84 .157
.788 .788 .106E+04 .698E+03* .537 .252 33.06 .199
.900 .900 .129E+04 .970E+03* .700 .270 30.81 .243
1.013 1.013 .154E+04 .130E+04* .888 .288 28.95 .291
1.125 1.125 .181E+04 .170E+04* 1.102 .304 27.37 .343
1.238 1.238 .210E+04 .216E+04* 1.344 .320 26.01 .397
1.350 1.350 .240E+04 .271E+04* 1.615 .336 24.81 .453
1.463 1.463 .273E+04 .333E+04* 1.916 .351 23.76 .513
1.575 1.575 .308E+04 .404E+04* 2.247 .365 22.82 .575
1.688 1.688 .344E+04 .484E+04* 2.611 .379 21.97 .640
1.800 1.800 .382E+04 .574E+04* 3.008 .393 21.19 .708
1.933 1.933 .427E+04 .674E+04* 3.433 .407 20.42 .779
2.067 2.067 .475E+04 .788E+04* 3.893 .421 19.67 .854
2.200 2.200 .525E+04 .918E+04* 4.383 .435 18.93 .933

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

<----- hydrograph -----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002050 144.19 3.448 7.55 33.136 1.769 .463
OUTFLOW : ID= 1:002060 144.19 3.395 7.60 33.136 1.756 .461

```

INFLOW : ID= 3:002070 148.97 3.492 7.58 32.956 1.859 .304  
OUTFLOW : ID= 1:002080 148.97 3.242 8.38 32.956 1.827 .346

```

010:0019-----
| DESIGN NASHYD | Area (ha)= 14.96 Curve Number (CN)=72.00
| 02:207 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.330

```

Unit Hyd Qpeak (cms)= .430

PEAK FLOW (cms)= .307 (1)

TIME TO PEAK (hrs)= 7.351

RUNOFF VOLUME (mm)= 27.531

TOTAL RAINFALL (mm)= 69.200

RUNOFF COEFFICIENT = .398

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0020-----
| DESIGN NASHYD | Area (ha)= 7.92 Curve Number (CN)=72.00
| 03:208 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110

```

Unit Hyd Qpeak (cms)= .273

PEAK FLOW (cms)= .186 (1)

TIME TO PEAK (hrs)= 7.101

RUNOFF VOLUME (mm)= 27.531

TOTAL RAINFALL (mm)= 69.200

RUNOFF COEFFICIENT = .398

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0021-----
#####
## Laegan Drain - Total Flow at Jefferson Boulevard
#####
| ADD HYD ( 2090 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (cms)
| ID1 01: 2080 | 148.97 | 3.242 | 8.38 | 32.96 | .000
| +ID2 02:207 | 14.96 | .307 | 7.35 | 27.53 | .000
| +ID3 03:208 | 7.92 | .186 | 7.10 | 27.53 | .000
| SUM 04: 2090 | 171.85 | 3.617 | 8.15 | 32.23 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0022-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
| LENGTH = 130.00 (m)

```

```

<----- DATA FOR SECTION ( 6.0 ) ----->
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .2000 Main Channel
407.00 2.20 .2000

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .245E+02 .892E+01 .016 .087 24.94 .010
.225 .225 .473E+02 .389E+02 .054 .129 16.76 .029
.337 .337 .884E+02 .957E+02* .110 .161 13.43 .054
.450 .450 .128E+03 .185E+03* .185 .188 11.53 .085
.562 .562 .173E+03 .313E+03* .280 .211 10.25 .119
.675 .675 .222E+03 .481E+03* .397 .233 9.32 .157
.788 .788 .277E+03 .698E+03* .537 .252 8.59 .199
.900 .900 .336E+03 .970E+03* .700 .270 8.01 .243
1.013 1.013 .401E+03 .130E+04* .888 .288 7.53 .291
1.125 1.125 .473E+03 .170E+04* 1.102 .304 7.12 .343
1.238 1.238 .545E+03 .216E+04* 1.344 .320 6.76 .397
1.350 1.350 .625E+03 .271E+04* 1.615 .336 6.45 .453
1.463 1.463 .710E+03 .333E+04* 1.916 .351 6.18 .513
1.575 1.575 .800E+03 .404E+04* 2.247 .365 5.93 .575
1.688 1.688 .895E+03 .484E+04* 2.611 .379 5.71 .640
1.800 1.800 .994E+03 .574E+04* 3.008 .393 5.51 .708
1.933 1.933 .1.027E+04 .674E+04* 3.433 .407 5.37 .779
2.067 2.067 .1.067E+04 .788E+04* 3.893 .421 5.24 .854
2.200 2.200 .1.118E+04 .918E+04* 4.383 .435 5.12 .933

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

010:0023-----
| DESIGN NASHYD | Area (ha)= 4.95 Curve Number (CN)=73.00
| 02:212 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .480

```

Unit Hyd Qpeak (cms)= .394

PEAK FLOW (cms)= .215 (1)

TIME TO PEAK (hrs)= 6.351

RUNOFF VOLUME (mm)= 28.354

TOTAL RAINFALL (mm)= 69.200

RUNOFF COEFFICIENT = .410

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0024-----
| ADD HYD ( 2110 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (cms)
| ID1 01: 2100 | 171.85 | 3.381 | 7.95 | 32.23 | .000
| +ID2 02:212 | 4.95 | .215 | 6.35 | 28.35 | .000
| SUM 03: 2110 | 176.80 | 3.425 | 7.95 | 32.13 | .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0025-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002110 | Number of SEGMENTS = 3
| OUT< 01:002120 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
| LENGTH = 330.00 (m)

```

```

<----- DATA FOR SECTION ( 7.0 ) ----->

```

Distance	Elevation	Manning
.00	2.20	.1400
200.00	1.80	.1400 / .0850 Main Channel
202.75	.00	.0850 Main Channel
204.25	.00	.0850 Main Channel
207.00	1.80	.0850 / .2000 Main Channel
407.00	2.20	.2000

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.112	.112	.621E+02	.882E+01	.016	.087	63.30	.010
.225	.225	.137E+03	.389E+02	.054	.129	42.54	.029
.337	.337	.224E+03	.957E+02	.110	.161	34.10	.054
.450	.450	.322E+03	1.85E+03*	.185	.188	29.26	.095
.562	.562	.438E+03	.311E+03*	.280	.211	26.02	.119
.675	.675	.564E+03	.481E+03*	.397	.233	23.65	.157
.788	.788	.702E+03	.698E+03*	.537	.252	21.82	.199
1.900	1.900	.854E+04	.870E+04*	3.700	.270	20.34	.243
1.013	1.013	.102E+04	.130E+04*	.888	.288	19.11	.291
1.125	1.125	.119E+04	.170E+04*	1.102	.304	18.06	.343
1.238	1.238	.138E+04	.216E+04*	1.344	.320	17.16	.397
1.350	1.350	.159E+04	.271E+04*	1.615	.336	16.38	.453
1.463	1.463	.180E+04	.333E+04*	1.916	.351	15.68	.513
1.575	1.575	.203E+04	.404E+04*	2.247	.365	15.06	.575
1.688	1.688	.227E+04	.484E+04*	2.611	.379	14.50	.640
1.800	1.800	.254E+04	.574E+04*	2.993	.393	13.99	.708
1.933	1.933	.277E+04	.671E+04*	3.401	.411	13.50	.781
2.067	2.067	.299E+04	.784E+04*	3.848	.432	13.04	.858
2.200	2.200	.320E+04	.902E+04*	4.334	.458	12.62	.940

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 3:002110	176.80	3.425	7.95	32.125	1.854
OUTFLOW : ID= 1:002120	176.80	3.158	8.10	32.125	1.819

DESIGN NASHYD	Area	(ha)	Curve Number	(CN)=82.00
02:EXT8 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp (hrs)		.820	

Unit Hyd Qpeak (cms)= .307  
 PEAK FLOW (cms)= .267 (i)  
 TIME TO PEAK (hrs)= 6.734  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD	Area	(ha)	Curve Number	(CN)=82.00
02:EXT8 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp (hrs)		.820	

Unit Hyd Qpeak (cms)= .307

PEAK FLOW (cms)= .267 (i)  
 TIME TO PEAK (hrs)= 6.734  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD	Area	(ha)	Curve Number	(CN)=72.00
01:203 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp (hrs)		.970	

Unit Hyd Qpeak (cms)= .502

PEAK FLOW (cms)= .331 (i)  
 TIME TO PEAK (hrs)= 6.934  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN> 01:203	Number of SEGMENTS = 3	
OUT< 02:002140	Slopes (%), CHANNEL= .3500 FLOODPLAIN= .2000	LENGTH = 500.00 (m)

Distance	Elevation	Manning
.00	1.40	.1400
200.00	1.00	.1400 / .1000 Main Channel
201.50	.00	.1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / .2000 Main Channel
405.00	1.40	.2000

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.071	.071	.753E+02	.154E+01	.015	.097	85.67	.007
.143	.143	.158E+03	.646E+01	.047	.149	56.11	.021
.214	.214	.249E+03	1.52E+02	.094	.188	44.28	.040
.286	.286	.347E+03	.283E+02	.154	.221	37.63	.063
.357	.357	.453E+03	.462E+02	.227	.250	33.27	.089
.429	.429	.566E+03	.693E+02	.313	.276	30.14	.118
.500	.500	.697E+03	.982E+02	.413	.269	27.75	.151
.571	.571	.816E+03	1.33E+03	.526	.232	25.85	.184
.643	.643	.953E+03	1.75E+03	.654	.243	24.30	.220
.714	.714	1.10E+04	2.24E+03	.795	.262	22.99	.259
.786	.786	1.25E+04	2.80E+03	.952	.281	21.87	.299
.857	.857	1.41E+04	3.45E+03	1.123	.299	20.90	.342
.929	.929	1.58E+04	4.18E+03	1.310	.316	20.04	.386
1.000	1.000	1.75E+04	5.00E+03	1.513	.332	19.28	.432
1.080	1.080	1.93E+04	5.91E+03	1.733	.349	18.62	.480
1.160	1.160	2.12E+04	6.93E+03	2.000	.367	18.04	.530
1.240	1.240	2.32E+04	8.06E+03	2.313	.386	17.52	.582
1.320	1.320	2.54E+04	9.31E+03	2.683	.411	17.04	.638
1.400	1.400	2.77E+04	1.068E+04	3.113	.436	16.60	.698

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 1:203	12.75	331	6.93	27.531	.441
OUTFLOW : ID= 2:002140	12.75	.289	7.33	27.531	.407

DESIGN NASHYD	Area	(ha)	Curve Number	(CN)=72.00
01:205 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp (hrs)		.860	

Unit Hyd Qpeak (cms)= .572  
 PEAK FLOW (cms)= .365 (i)  
 TIME TO PEAK (hrs)= 6.801  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (	ID:	NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
01:01:205			12.89	.365	6.80	27.53	.000
+ID2 02:	2140		12.75	.289	7.33	27.53	.000
SUM 03:	2150		25.64	.623	7.05	27.53	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN> 03:002150	Number of SEGMENTS = 3	
OUT< 01:002160	Slopes (%), CHANNEL= .0500 FLOODPLAIN= .2000	LENGTH = 360.00 (m)

Distance	Elevation	Manning
.00	1.40	.1400
200.00	1.00	.1400 / .1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / .2000 Main Channel
405.00	1.40	.2000

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.071	.071	.542E+02	1.08E+02	.006	.037	163.19	.003
.143	.143	1.14E+03	452E+02	.018	.056	106.89	.008
.214	.214	1.79E+03	1.07E+03*	.035	.071	84.35	.015
.286	.286	2.50E+03	1.98E+03*	.058	.084	71.69	.024
.357	.357	3.26E+03	3.23E+03*	.086	.095	63.38	.034
.429	.429	4.08E+03	4.85E+03*	.118	.105	57.41	.045
.500	.500	4.95E+03	6.87E+03*	.156	.113	52.87	.057
.571	.571	5.88E+03	9.33E+03*	.199	.122	49.25	.070
.643	.643	6.86E+03	1.23E+04*	.247	.130	46.29	.083
.714	.714	7.90E+03	1.57E+04*	.301	.137	43.80	.098
.786	.786	8.99E+03	1.96E+04*	.360	.144	41.67	.113
.857	.857	1.01E+04	2.41E+04*	.424	.151	39.81	.129
.929	.929	1.13E+04	2.93E+04*	.495	.157	38.18	.146
1.000	1.000	1.26E+04	3.50E+04*	.572	.163	36.73	.163
1.080	1.080	1.40E+04	4.12E+04*	.658	.168	35.36	.181
1.160	1.160	1.55E+04	4.80E+04*	.753	.173	34.07	.199
1.240	1.240	1.71E+04	5.54E+04*	.858	.178	32.84	.218
1.320	1.320	1.88E+04	6.35E+04*	.973	.183	31.66	.238
1.400	1.400	2.06E+04	7.23E+04*	1.098	.188	30.52	.258

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 3:002150	25.64	.623	7.05	27.531	1.019
OUTFLOW : ID= 1:002160	25.64	.514	7.45	27.531	.948

DESIGN NASHYD	Area	(ha)	Curve Number	(CN)=72.00
02:209 DT= 1.00	Ia	(mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp (hrs)		.970	

Unit Hyd Qpeak (cms)= .610  
 PEAK FLOW (cms)= .402 (i)  
 TIME TO PEAK (hrs)= 6.934  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (	ID:	NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
01:01:209			15.50	.402	6.93	27.53	.000
+ID2 02:209	2160		15.50	.402	6.93	27.53	.000
SUM 03:	2170		31.00	.804	7.30	27.53	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL	Routing time step (min)	= 1.00
IN> 03:002170	Number of SEGMENTS = 3	
OUT< 01:002180	Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000	LENGTH = 250.00 (m)

Distance	Elevation	Manning
.00	1.40	.1400
200.00	1.00	.2000 / .1000 Main Channel
201.50	.00	.1000 Main Channel
203.50	.00	.1000 Main Channel
205.00	1.00	.1000 / .2000 Main Channel
405.00	1.40	.2000

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.071	.071	.376E+02	3.58E+01	.010	.064	65.43	.005
.143	.143	.791E+02	1.51E+02	.021	.097	42.85	.014
.214	.214	1.24E+03	3.55E+02	.041	.123	33.82	.026
.286	.286	1.73E+03	6.61E+02	.071	.145	28.74	.041
.357	.357	2.26E+03	1.08E+03	.108	.164	25.41	.059
.429	.429	2.83E+03	1.62E+03*	.156	.181	23	



Table with 7 columns: 1.000, 1.000, .875E+03, .117E+04, .990, .283, 14.73, .283. Includes values for 1.080, 1.160, 1.240, 1.320, 1.400.

SUM 03: 2210 84.30 1.818 7.72 31.89 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

Table with 7 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes routing data for 2220.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 02:210.

Table with 7 columns: ROUTE CHANNEL, IN, OUTFLOW, Routing time step, Number of SEGMENTS, Slopes, CHANNEL, FLOODPLAIN, LENGTH.

Table with 7 columns: DISTANCE, ELEVATION, MANNING. DATA FOR SECTION ( 12.0 )

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 03:EXTA.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV TIME, D x V. TRAVEL TIME TABLE

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 03:EXTA.

Table with 7 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes routing data for 2190.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 04:002190.

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 01:213.

Table with 7 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes routing data for 2240.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV TIME, D x V. TRAVEL TIME TABLE

Table with 7 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Includes routing data for 2240.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Includes INFLOW and OUTFLOW data.

Table with 7 columns: ROUTE CHANNEL, IN, OUTFLOW, Routing time step, Number of SEGMENTS, Slopes, CHANNEL, FLOODPLAIN, LENGTH.

Table with 7 columns: DISTANCE, ELEVATION, MANNING. DATA FOR SECTION ( 13.0 )

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 02:EXTS.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV TIME, D x V. TRAVEL TIME TABLE

Table with 7 columns: DESIGN NASHYD, Area, Curve Number, U.H. Tp. Includes routing data for 02:EXTS.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 3:002240	284.58	4.766	8.20	31.900	1.607	1.64
OUTFLOW: ID= 1:002250	284.58	4.578	9.38	31.900	1.601	1.66

Distance	Elevation	Manning
200.00	1.40	.1400 / .0850
202.60	.00	.0850
204.40	.00	.0850
207.00	1.40	.0850 / .2000
407.00	1.80	.2000

010:0047-----  
 | DESIGN NASHYD | Area (ha)= 24.11 | Curve Number (CN)=80.00  
 | 02:EXT6 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00  
 | U.H. Tp(hrs)= 1.520  
 Unit Hyd Qpeak (cms)= .606  
 PEAK FLOW (cms)= .576 (i)  
 TIME TO PEAK (hrs)= 7.551  
 RUNOFF VOLUME (mm)= 34.934  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .505  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV.TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.093	.093	.681E+02	1.07E+02	.012	.064	96.65	.006
.187	.187	1.48E+03	4.67E+02	.038	.096	64.26	.018
.280	.280	2.40E+03	1.14E+03	.078	.121	51.18	.034
.373	.373	3.44E+03	2.17E+03*	.131	.141	43.73	.053
.467	.467	4.60E+03	3.63E+03*	.198	.159	38.79	.074
.560	.560	5.88E+03	5.57E+03*	.279	.175	35.19	.098
.653	.653	7.28E+03	8.04E+03*	.374	.190	32.42	.124
.747	.747	8.80E+03	1.11E+04*	.486	.204	30.20	.152
.840	.840	1.04E+04	1.48E+04*	.614	.217	28.36	.183
.933	.933	1.22E+04	1.92E+04*	.759	.230	26.81	.215
1.027	1.027	1.41E+04	2.44E+04*	.921	.242	25.47	.249
1.120	1.120	1.61E+04	3.04E+04*	1.103	.254	24.30	.284
1.213	1.213	1.82E+04	3.73E+04*	1.304	.265	23.27	.322
1.307	1.307	2.04E+04	4.51E+04*	1.524	.276	22.34	.361
1.400	1.400	2.28E+04	5.39E+04*	1.766	.287	21.51	.401
1.500	1.500	2.53E+04	6.37E+04*	2.297	.194	31.84	.290
1.600	1.600	1.02E+05	2.76E+05*	3.654	.133	46.51	.212
1.700	1.700	1.97E+05	5.66E+05*	6.329	.119	51.90	.202
1.800	1.800	3.29E+05	1.00E+06*	10.726	.121	51.14	.217

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

010:0048-----  
 | DESIGN NASHYD | Area (ha)= 14.49 | Curve Number (CN)=82.00  
 | 03:211 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00  
 | U.H. Tp(hrs)= 1.070  
 Unit Hyd Qpeak (cms)= .517  
 PEAK FLOW (cms)= .482 (i)  
 TIME TO PEAK (hrs)= 7.018  
 RUNOFF VOLUME (mm)= 37.125  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .536  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV.TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.030	.030	.163E+02	.245E+00	.003	.102	81.78	.003
.060	.060	.353E+02	1.06E+01	.011	.155	53.91	.009
.090	.090	.570E+02	2.56E+01	.022	.195	42.68	.018
.120	.120	.813E+02	4.88E+01	.037	.229	36.32	.028
.150	.150	1.08E+03	8.12E+01	.056	.260	32.11	.039
.180	.180	1.38E+03	1.24E+02	.079	.287	29.06	.052
.210	.210	1.70E+03	1.79E+02	.106	.312	26.72	.065
.240	.240	2.05E+03	2.46E+02	.138	.335	24.85	.080
.270	.270	2.43E+03	3.27E+02	.173	.358	23.31	.097
.300	.300	2.83E+03	4.24E+02	.214	.379	22.01	.114
.330	.330	3.26E+03	5.37E+02	.260	.399	20.89	.132
.360	.360	3.71E+03	6.68E+02	.311	.418	19.92	.151
.390	.390	4.19E+03	8.18E+02	.367	.437	19.06	.171
.420	.420	4.70E+03	9.88E+02	.428	.455	18.30	.191
.450	.450	5.24E+03	1.18E+03	.496	.473	17.61	.213
.480	.480	5.80E+03	1.39E+03	.569	.491	16.99	.235
.510	.510	6.39E+03	1.63E+03	.648	.507	16.42	.259
.540	.540	7.02E+03	1.89E+03	.734	.524	15.90	.283
.570	.570	7.64E+03	2.18E+03	.826	.540	15.43	.308

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

010:0049-----  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN: 03:211 | Number of SEGMENTS = 3  
 | OUT: 04:002280 | Slopes (%), CHANNEL= .2000 FLOODPLAIN= .2000  
 LENGTH = 500.00 (m)  
 <----- DATA FOR SECTION ( 15.0) ----->  
 Distance Elevation Manning  
 .00 .62 .1400  
 10.00 .60 .1400 / .0400 Main Channel  
 11.80 .00 .0400 Main Channel  
 12.80 .00 .0400 Main Channel  
 14.60 .62 .0400 / .2000 Main Channel  
 24.60 .60 .2000

010:0054-----  
 | DESIGN NASHYD | Area (ha)= 17.47 | Curve Number (CN)=76.00  
 | 03:214 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00  
 | U.H. Tp(hrs)= .600  
 Unit Hyd Qpeak (cms)= 1.112  
 PEAK FLOW (cms)= .720 (i)  
 TIME TO PEAK (hrs)= 6.501  
 RUNOFF VOLUME (mm)= 30.987  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .448  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE

DEPTH	ELEV	X-VOLUME	S-VOLUME	FLOW RATE	VELOCITY	TRAV.TIME	D x V
(m)	(m)	(cu.m.)	(cu.m.)	(cms)	(m/s)	(min)	(m2/s)
.030	.030	.163E+02	.245E+00	.003	.102	81.78	.003
.060	.060	.353E+02	1.06E+01	.011	.155	53.91	.009
.090	.090	.570E+02	2.56E+01	.022	.195	42.68	.018
.120	.120	.813E+02	4.88E+01	.037	.229	36.32	.028
.150	.150	1.08E+03	8.12E+01	.056	.260	32.11	.039
.180	.180	1.38E+03	1.24E+02	.079	.287	29.06	.052
.210	.210	1.70E+03	1.79E+02	.106	.312	26.72	.065
.240	.240	2.05E+03	2.46E+02	.138	.335	24.85	.080
.270	.270	2.43E+03	3.27E+02	.173	.358	23.31	.097
.300	.300	2.83E+03	4.24E+02	.214	.379	22.01	.114
.330	.330	3.26E+03	5.37E+02	.260	.399	20.89	.132
.360	.360	3.71E+03	6.68E+02	.311	.418	19.92	.151
.390	.390	4.19E+03	8.18E+02	.367	.437	19.06	.171
.420	.420	4.70E+03	9.88E+02	.428	.455	18.30	.191
.450	.450	5.24E+03	1.18E+03	.496	.473	17.61	.213
.480	.480	5.80E+03	1.39E+03	.569	.491	16.99	.235
.510	.510	6.39E+03	1.63E+03	.648	.507	16.42	.259
.540	.540	7.02E+03	1.89E+03	.734	.524	15.90	.283
.570	.570	7.64E+03	2.18E+03	.826	.540	15.43	.308

010:0055-----  
 ## Calculate culvert routing and flow split near eastern site boundary  
 ## Storage volumes calculated based on site survey  
 ## Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities  
 ROUTE RESERVOIR | Requested routing time step = 1.0 min.  
 | IN:03:(214) |  
 | OUT:01:(002300) |  
 ===== OUTFLOW STORAGE TABLE =====  
 OUTFLOW STORAGE  
 (cms) (ha.m.) | (cms) (ha.m.)  
 .000 .000E+00 | 1.130 .4600E+00  
 .150 .0000E+00 | 5.470 .8100E+00  
 .450 .0000E+00 | 83.090 .3400E+01  
 .820 .6500E-01 | 0.000 .0000E+00  
 ROUTING RESULTS AREA QPEAK TPEAK R.V.  
 (ha) (cms) (hrs) (mm)  
 INFLOW >03: (214) | 17.47 .720 6.501 30.987  
 OUTFLOW<01: (002300) | 17.47 .625 6.834 30.993  
 PEAK FLOW REDUCTION [Qout/Qin] (%) = 86.843  
 TIME SHIFT OF PEAK FLOW (min) = 20.00  
 MAXIMUM STORAGE USED (ha.m.) = .3079E-01

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 <----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID= 3:211 14.49 4.82 7.02 37.125 .444 .469  
 OUTFLOW: ID= 4:002280 14.49 4.57 7.28 37.125 .431 .462

010:0050-----  
 | DESIGN NASHYD | Area (ha)= 10.57 | Curve Number (CN)=72.00  
 | 03:216 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00  
 | U.H. Tp(hrs)= 1.210  
 Unit Hyd Qpeak (cms)= .334  
 PEAK FLOW (cms)= .233 (i)  
 TIME TO PEAK (hrs)= 7.218  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0056-----  
 | DIVERT HYD |  
 | INID=01 (002300) |  
 Outflow / Inflow Relationships  
 Flow 02 + Flow 03 = Total  
 (cms) (cms) (cms)  
 .000 .000 .000  
 .150 .000 .150  
 .400 .050 .450  
 .680 .140 .820  
 .830 .200 1.130  
 1.040 4.430 5.470  
 1.460 81.630 83.090  
 NHYD AREA QPEAK TpeakDate\_hh:mm R.V. NFE WetHrs  
 (ha) (cms) (hrs) (mm) (hrs)  
 IDin = 01:002300 17.47 .625 No\_date 6:50 30.993 79 13.  
 IDout= 02:002310 15.96 .533 No\_date 6:50 30.993 79 13.  
 IDout= 03:002320 1.51 .093 No\_date 6:50 30.993 26 3.

010:0051-----  
 | ADD HYD ( 2290) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (cms)  
 ID1 03:216 10.57 .233 7.22 27.53 .000  
 +ID2 04: 2280 14.49 4.57 7.28 37.12 .000  
 SUM 05: 2290 25.06 .690 7.27 33.08 .000  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0057-----  
 | DESIGN NASHYD | Area (ha)= 5.34 | Curve Number (CN)=72.00  
 | 01:215 DT= 1.00 | Ia (mm)= 1.500 | # of Linear Res. (N)= 3.00  
 | U.H. Tp(hrs)= .860  
 Unit Hyd Qpeak (cms)= .237  
 PEAK FLOW (cms)= .151 (i)  
 TIME TO PEAK (hrs)= 6.801  
 RUNOFF VOLUME (mm)= 27.531  
 TOTAL RAINFALL (mm)= 69.200  
 RUNOFF COEFFICIENT = .398  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0052-----  
 | ADD HYD ( 2260) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (cms)  
 ID1 01: 2250 284.58 4.578 9.38 31.90 .000  
 +ID2 02:EXT6 24.11 .576 7.55 34.93 .000  
 +ID3 05: 2290 25.06 .690 7.27 33.08 .000  
 SUM 03: 2260 333.75 5.456 8.33 32.21 .000  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

010:0058-----  
 | ADD HYD ( 2330) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (cms)  
 ID1 01:215 5.34 .151 6.80 27.53 .000  
 +ID2 02: 2310 15.96 .533 6.83 30.99 .000  
 SUM 04: 2330 21.30 .684 6.83 30.13 .000

010:0053-----  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN: 03:002260 | Number of SEGMENTS = 3  
 | OUT: 10:002295 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000  
 LENGTH = 370.00 (m)  
 <----- DATA FOR SECTION ( 14.0) ----->

010:0059-----  
 | DESIGN NASHYD | Area (ha)= 18.59 | Curve Number (CN)=82.00

```

| 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.470
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .486 (i)
TIME TO PEAK (hrs)= 7.484
RUNOFF VOLUME (mm)= 37.125
TOTAL RAINFALL (mm)= 69.200
RUNOFF COEFFICIENT = .536

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

010:0060-----
*****
# McGill Drain - Total Flow at Eastern WSP
*****
| ADD HYD ( 2340) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| (ha) (cms) (hrs) (mm) (cms)
ID1 01:EXT7 18.59 .486 7.48 37.12 .000
+ID2 04: 2330 21.30 .684 6.83 30.13 .000
+ID3 10: 2295 333.75 4.947 9.65 32.21 .000
SUM 05: 2340 373.64 5.364 9.47 32.33 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0061-----
*****
# AREA CHECK
*****
| ADD HYD ( 2350) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| (ha) (cms) (hrs) (mm) (cms)
ID1 03: 2320 1.51 .093 6.83 30.99 .000
+ID2 05: 2340 373.64 5.364 9.47 32.33 .000
SUM 01: 2350 375.15 5.364 9.47 32.33 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

010:0062-----
*****
# END OF RUN : 24

```

```

| START | Project dir.: F:\WSP\
| Rainfall dir.: F:\WSP\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NWIN = 025
NSTORM= 1
# #1=2secs25.stm

```

```

025:0002-----
*****
# Project Name: [Windsor Solar Project] Project Number: [1335-60106]
# Date : 02-10-2016
# Modeler : [DRE]
# Company : Stantec Consulting Ltd. (London)
# License # : 4730904
*****
# Proposed Conditions
# 25 mm Water Quality Event
# 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
*****

```

```

025:0002-----
| READ STORM | Filename: 25-yr scs 12 hr windsor
| Ptotal= 80.80 mm | Comments: 25-yr scs 12 hr windsor
-----
| TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
| hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.616 | 3.50 3.232 | 6.50 14.544 | 9.50 3.232
1.00 1.616 | 4.00 3.232 | 7.00 6.464 | 10.00 1.616
1.50 1.616 | 4.50 4.848 | 7.50 4.848 | 10.50 1.616
2.00 1.616 | 5.00 6.464 | 8.00 4.848 | 11.00 1.616
2.50 3.232 | 5.50 9.696 | 8.50 3.232 | 11.50 1.616
3.00 3.232 | 6.00 7.272 | 9.00 3.232 | 12.00 1.616

```

```

025:0003-----
*****
# LAPPAN DRAIN
*****
| DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
| 01:EXT1 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms)= 1.454
PEAK FLOW (cms)= 1.319 (i)
TIME TO PEAK (hrs)= 7.084
RUNOFF VOLUME (mm)= 36.299
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .449

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

025:0004-----
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 01:EXT1 | Number of SEGMENTS = 3
| OUT: 02:002000 | Slopes (%), CHANNEL= 1000 FLOODPLAIN= .2000
| LENGTH = 700.00 (m)
-----
<----- DATA FOR SECTION ( 1.0) ----->
Distance Elevation Manning
.00 1.40 2000
100.00 1.20 2000 / .0850 Main Channel
101.80 .00 .0850 Main Channel
103.00 .00 .0850 Main Channel
104.80 1.20 .0850 / .2000 Main Channel
204.80 1.40 2000

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.071 .071 .648E+02 .323E+01 .005 .059 197.27 .004
.141 .141 .140E+03 .141E+02 .018 .089 131.37 .013
.212 .212 .225E+03 .340E+02 .036 .111 104.80 .024
.282 .282 .321E+03 .647E+02 .060 .130 89.71 .037
.353 .353 .427E+03 .108E+03 .089 .146 79.68 .052
.424 .424 .544E+03 .165E+03 .125 .161 72.40 .068
.494 .494 .671E+03 .237E+03 .168 .175 66.79 .086

```

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.
-----
<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 1:EXT1 42.26 1.319 7.08 36.299 1.281 .168
OUTFLOW: ID= 2:002000 42.26 1.100 7.97 36.298 1.223 .235

```

```

025:0005-----
| DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00
| 01:EXT2 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.270
Unit Hyd Qpeak (cms)= .677
PEAK FLOW (cms)= .829 (i)
TIME TO PEAK (hrs)= 7.234
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

025:0006-----
| DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00
| 03:EXT3 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms)= 1.473
PEAK FLOW (cms)= 1.744 (i)
TIME TO PEAK (hrs)= 7.051
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

025:0007-----
*****
# Lappan Drain - Total Flow at Fallette Road
*****
| ADD HYD ( 2010) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| (ha) (cms) (hrs) (mm) (cms)
ID1 01:EXT2 22.52 .829 7.23 46.56 .000
+ID2 02:002000 42.26 1.100 7.97 36.30 .000
+ID3 03:EXT3 42.81 1.744 7.05 46.56 .000
SUM 04: 2010 107.59 3.428 7.33 42.53 .000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

025:0008-----
| IN: 04:002010 | Routing time step (min) = 1.00
| OUT: 01:002010 | Number of SEGMENTS = 3
| SLOPES (%), CHANNEL= 1.700 FLOODPLAIN= .2000
| LENGTH = 350.00 (m)

```

```

<----- DATA FOR SECTION ( 2.0) ----->
Distance Elevation Manning
.00 2.00 2000
100.00 1.80 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .578E+02 .486E+01 .016 .096 60.50 .010
.200 .200 .126E+03 .212E+02 .052 .144 40.48 .029
.300 .300 .208E+03 .518E+02 .106 .180 32.38 .054
.400 .400 .296E+03 .993E+02 .177 .210 27.75 .084
.500 .500 .396E+03 .166E+03 .268 .236 24.67 .118
.600 .600 .508E+03 .256E+03 .377 .260 22.42 .156
.700 .700 .639E+03 .376E+03 .507 .282 20.68 .197
.800 .800 .762E+03 .512E+03 .659 .303 19.28 .242
.900 .900 .906E+03 .685E+03 .833 .322 18.12 .290
1.000 1.000 .106E+04 .891E+03 1.031 .340 17.14 .340
1.100 1.100 .122E+04 .113E+04 1.253 .358 16.29 .394
1.200 1.200 .140E+04 .141E+04 1.500 .375 15.55 .450
1.300 1.300 .159E+04 .173E+04 1.775 .392 14.89 .509
1.400 1.400 .178E+04 .210E+04 2.077 .408 14.31 .571
1.500 1.500 .198E+04 .251E+04 2.407 .423 13.78 .635
1.600 1.600 .221E+04 .297E+04 2.768 .439 13.30 .702
1.700 1.700 .244E+04 .348E+04 3.158 .453 12.87 .771
1.800 1.800 .268E+04 .405E+04 3.580 .468 12.46 .842
2.000 2.000 .102E+05 .171E+05 5.907 .203 28.69 .407

```

```

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

```

```

025:0009-----
<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(cms) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002010 107.59 3.428 7.33 42.531 1.764 .463
OUTFLOW: ID= 1:002020 107.59 3.339 7.43 42.531 1.744 .460

```

```

025:0009-----
| DESIGN NASHYD | Area (ha)= 10.43 Curve Number (CN)=72.00
| 02:202 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
| U.H. Tp(hrs)= .970
Unit Hyd Qpeak (cms)= .411
PEAK FLOW (cms)= .349 (i)
TIME TO PEAK (hrs)= 6.918
RUNOFF VOLUME (mm)= 35.314
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .437

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0010-----

ADD HYD (	2030)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:	2020		107.59	3.339	7.43	42.53	.000
+ID2 02:202			10.43	.349	6.92	35.31	.000
SUM 03:	2030		118.02	3.644	7.43	41.89	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0011-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 03:002030	Number of SEGMENTS = 3
OUT< 01:002040	Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
	LENGTH = 450.00 (m)

<----- DATA FOR SECTION ( 3.0) ----->

Distance	Elevation	Manning
.00	2.00	.1400
100.00	1.80	.1400 / .0850
102.75	.00	.0850
104.25	.00	.0850
107.00	1.80	.0850 / .1400
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.100	1.00	.744E+02	.486E+01	.016	.096	77.79	.010
.200	2.00	.163E+03	.212E+02	.052	.144	52.05	.029
.300	3.00	.264E+03	.518E+02	.106	.180	41.63	.054
.400	4.00	.380E+03	.939E+02	.177	.210	35.68	.084
.500	5.00	.509E+03	.166E+03	.268	.236	31.72	.118
.600	6.00	.653E+03	.256E+03	.377	.260	28.82	.156
.700	7.00	.809E+03	.370E+03	.507	.282	26.59	.197
.800	8.00	.980E+03	.512E+03	.659	.303	24.79	.242
.900	9.00	1.16E+04	.685E+03	.833	.322	23.30	.290
1.000	1.000	.136E+04	.891E+03	1.031	.340	22.04	.340
1.100	1.100	.157E+04	.113E+04	1.253	.358	20.95	.394
1.200	1.200	.180E+04	.141E+04	1.500	.375	19.99	.450
1.300	1.300	.204E+04	.173E+04	1.775	.392	19.15	.509
1.400	1.400	.229E+04	.210E+04	2.077	.408	18.40	.571
1.500	1.500	.256E+04	.251E+04	2.407	.423	17.72	.635
1.600	1.600	.284E+04	.297E+04	2.768	.439	17.10	.702
1.700	1.700	.313E+04	.348E+04	3.158	.453	16.54	.771
1.800	1.800	.344E+04	.405E+04	3.580	.468	16.03	.842
2.000	2.000	.131E+05	.171E+05	5.907	.203	36.88	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
118.02	3.644	7.43	41.893	1.805	452
118.02	3.527	7.70	41.893	1.779	465

025:0012-----

DESIGN NASHYD	Area (ha)	15.29	Curve Number (CN)=82.00
02:201 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.290	

Unit Hyd Qpeak (cms)= .453  
 PEAK FLOW (cms)= .556 (i)  
 TIME TO PEAK (hrs)= 7.268  
 RUNOFF VOLUME (mm)= 46.563  
 TOTAL RAINFALL (mm)= 80.801  
 RUNOFF COEFFICIENT = .576  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0013-----

DESIGN NASHYD	Area (ha)	10.88	Curve Number (CN)=72.00
03:204 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	.850	

Unit Hyd Qpeak (cms)= .489  
 PEAK FLOW (cms)= .401 (i)  
 TIME TO PEAK (hrs)= 6.784  
 RUNOFF VOLUME (mm)= 35.314  
 TOTAL RAINFALL (mm)= 80.801  
 RUNOFF COEFFICIENT = .437  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0014-----

ADD HYD (	2050)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:	2040		118.02	3.527	7.70	41.89	.000
+ID2 02:201			15.29	.556	7.27	46.56	.000
+ID3 03:204			10.88	.401	6.78	35.31	.000
SUM 04:	2050		144.19	4.312	7.67	41.89	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0015-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 04:002050	Number of SEGMENTS = 3
OUT< 01:002060	Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
	LENGTH = 200.00 (m)

<----- DATA FOR SECTION ( 4.0) ----->

Distance	Elevation	Manning
.00	2.00	.1400
100.00	1.80	.1400 / .0850
102.75	.00	.0850
104.25	.00	.0850
107.00	1.80	.0850 / .1400
207.00	2.00	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.100	1.00	.331E+02	.486E+01	.016	.096	34.57	.010
.200	2.00	.722E+02	.212E+02	.052	.144	23.13	.029
.300	3.00	.118E+03	.518E+02	.106	.180	18.50	.054
.400	4.00	.169E+03	.939E+02	.177	.210	15.86	.084
.500	5.00	.226E+03	.166E+03	.268	.236	14.10	.118
.600	6.00	.290E+03	.256E+03	.377	.260	12.81	.156
.700	7.00	.360E+03	.370E+03	.507	.282	11.82	.197
.800	8.00	.436E+03	.512E+03	.659	.303	11.02	.242
.900	9.00	.518E+03	.685E+03	.833	.322	10.36	.290
1.000	1.000	.606E+03	.891E+03	1.031	.340	9.79	.340
1.100	1.100	.700E+03	.113E+04	1.253	.358	9.31	.394
1.200	1.200	.800E+03	.141E+04	1.500	.375	8.89	.450
1.300	1.300	.906E+03	.173E+04	1.775	.392	8.51	.509
1.400	1.400	.102E+04	.210E+04	2.077	.408	8.18	.571

1.500	1.500	.114E+04	.251E+04	2.407	.423	7.87	.635
1.600	1.600	.126E+04	.297E+04	2.768	.439	7.50	.702
1.700	1.700	.139E+04	.348E+04	3.158	.453	7.35	.771
1.800	1.800	.153E+04	.405E+04	3.580	.468	7.12	.842
2.000	2.000	.581E+04	.171E+05	6.114	2.10	15.84	.421

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
144.19	4.312	7.67	41.892	1.858	.346
144.19	4.204	7.85	41.892	1.850	.358

025:0016-----

DESIGN NASHYD	Area (ha)	4.78	Curve Number (CN)=72.00
02:206 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	.890	

Unit Hyd Qpeak (cms)= .205  
 PEAK FLOW (cms)= .170 (i)  
 TIME TO PEAK (hrs)= 6.834  
 RUNOFF VOLUME (mm)= 35.314  
 TOTAL RAINFALL (mm)= 80.801  
 RUNOFF COEFFICIENT = .437  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0017-----

ADD HYD (	2070)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:	2060		144.19	4.204	7.85	41.89	.000
+ID2 02:206			4.78	.170	6.83	35.31	.000
SUM 03:	2070		148.97	4.309	7.85	41.68	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0018-----

ROUTE CHANNEL	Routing time step (min) = 1.00
IN> 03:002070	Number of SEGMENTS = 3
OUT< 01:002080	Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
	LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 5.0) ----->

Distance	Elevation	Manning
.00	2.20	.1400
200.00	1.80	.1400 / .0850
202.75	.00	.0850
207.00	.00	.0850
207.00	1.80	.0850 / .1400
407.00	2.20	.1400

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.112	.112	.940E+02	.882E+01	.016	.087	95.91	.010
.225	.225	.197E+03	.389E+02	.054	.129	64.45	.029
.337	.337	.340E+03	.957E+02	.110	.161	51.67	.054
.450	.450	.492E+03	.185E+03	.185	.188	44.34	.085
.562	.562	.664E+03	.311E+03	.280	.211	39.43	.119
.675	.675	.854E+03	.461E+03	.397	.233	35.84	.157
.788	.788	.106E+04	.698E+03	.537	.252	33.06	.199
.900	.900	.129E+04	.970E+03	.700	.270	30.81	.243
1.013	1.013	.154E+04	.130E+04	.888	.288	28.95	.291
1.125	1.125	.181E+04	.170E+04	1.102	.304	27.37	.343
1.238	1.238	.210E+04	.216E+04	1.344	.320	26.01	.397
1.350	1.350	.240E+04	.271E+04	1.615	.336	24.81	.453
1.463	1.463	.273E+04	.333E+04	1.916	.351	23.76	.513
1.575	1.575	.308E+04	.404E+04	2.247	.365	22.82	.575
1.688	1.688	.344E+04	.484E+04	2.611	.379	21.97	.640
1.800	1.800	.382E+04	.574E+04	3.008	.393	21.19	.708
1.933	1.933	.424E+04	.674E+04	3.433	.407	20.50	.779
2.067	2.067	.472E+04	.794E+04	3.900	.421	19.86	.854
2.200	2.200	.526E+04	.939E+04	4.423	.435	19.33	.935

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
148.97	4.309	7.85	41.681	1.942	.229
148.97	3.895	8.72	41.681	1.907	.256

025:0019-----

DESIGN NASHYD	Area (ha)	14.96	Curve Number (CN)=72.00
02:207 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.330	

Unit Hyd Qpeak (cms)= .430  
 PEAK FLOW (cms)= .396 (i)  
 TIME TO PEAK (hrs)= 7.334  
 RUNOFF VOLUME (mm)= 35.314  
 TOTAL RAINFALL (mm)= 80.801  
 RUNOFF COEFFICIENT = .437  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0020-----

DESIGN NASHYD	Area (ha)	7.92	Curve Number (CN)=72.00
03:208 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.110	

Unit Hyd Qpeak (cms)= .273  
 PEAK FLOW (cms)= .240 (i)  
 TIME TO PEAK (hrs)= 7.084  
 RUNOFF VOLUME (mm)= 35.314  
 TOTAL RAINFALL (mm)= 80.801  
 RUNOFF COEFFICIENT = .437  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0021-----

DESIGN NASHYD	Area (ha)	14.96	Curve Number (CN)=72.00
03:208 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)	1.110	

\*\*\*\*\*  
 # Lappan Drain - Total Flow at Jefferson Boulevard  
 \*\*\*\*\*

025:0022-----

ADD HYD (	2090)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:	2080		148.97	3.895	8.72	41.68	.000
+ID2 02:207			14.96	.396	7.33	35.31	.000
+ID3 03:208			7.92	.240	7.08	35.31	.000



SUM 04: 2090 171.85 4.301 8.60 40.83 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0022-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 04:002090 | Number of SEGMENTS = 3
OUT< 01:002100 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 130.00 (m)

Table with columns: DEPTH (m), ELEV (m), X-VOLUME (cu.m.), S-VOLUME (cu.m.), FLOW RATE (cms), VELOCITY (m/s), TRAV. TIME (min), D x V (m2/s). Rows show data for various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph table with columns: AREA (ha), QPEAK (cms), TPEAK (hrs), R.V. (mm), MAX DEPTH (m), MAX VEL (m/s). Includes inflow and outflow data.

025:0023-----
DESIGN NASHYD | Area (ha)= 4.95 Curve Number (CN)=73.00
02:212 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .480

Unit Hyd Qpeak (cms)= .394
PEAK FLOW (cms)= .277 (i)
TIME TO PEAK (hrs)= 6.351
RUNOFF VOLUME (mm)= 36.299
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .449

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0024-----
ADD HYD ( 2100 | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
+ID1 01: 2100 171.85 4.235 8.75 40.83 .000
+ID2 02:212 4.95 .277 6.35 36.30 .000
SUM 03: 2110 176.80 4.271 8.75 40.71 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0025-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 03:002110 | Number of SEGMENTS = 3
OUT< 01:002120 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 330.00 (m)

Table with columns: DEPTH (m), ELEV (m), X-VOLUME (cu.m.), S-VOLUME (cu.m.), FLOW RATE (cms), VELOCITY (m/s), TRAV. TIME (min), D x V (m2/s). Rows show data for various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph table with columns: AREA (ha), QPEAK (cms), TPEAK (hrs), R.V. (mm), MAX DEPTH (m), MAX VEL (m/s). Includes inflow and outflow data.

025:0026-----
DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00
02:EXTS DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

Unit Hyd Qpeak (cms)= .307

PEAK FLOW (cms)= .336 (i)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0027-----
Lappan Drain - Total Flow at McGill Drain
ADD HYD ( 2130 | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01: 2120 176.80 4.032 9.40 40.71 .000
+ID2 02:EXTS 6.60 .336 6.73 46.56 .000
SUM 10: 2130 183.40 4.096 9.40 40.92 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0028-----
DESIGN NASHYD | Area (ha)= 12.75 Curve Number (CN)=72.00
01:203 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .970

Unit Hyd Qpeak (cms)= .502
PEAK FLOW (cms)= .427 (i)
TIME TO PEAK (hrs)= 6.918
RUNOFF VOLUME (mm)= 35.314
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .437

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0029-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 01:203 | Number of SEGMENTS = 3
OUT< 02:002140 | Slopes (%), CHANNEL= .3500 FLOODPLAIN= .2000
LENGTH = 500.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show data for various elevations from 0.00 to 405.00.

Table with columns: DEPTH (m), ELEV (m), X-VOLUME (cu.m.), S-VOLUME (cu.m.), FLOW RATE (cms), VELOCITY (m/s), TRAV. TIME (min), D x V (m2/s). Rows show data for various depths from 0.071 to 1.400.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

hydrograph table with columns: AREA (ha), QPEAK (cms), TPEAK (hrs), R.V. (mm), MAX DEPTH (m), MAX VEL (m/s). Includes inflow and outflow data.

025:0030-----
DESIGN NASHYD | Area (ha)= 12.89 Curve Number (CN)=72.00
01:205 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .860

Unit Hyd Qpeak (cms)= .572
PEAK FLOW (cms)= .471 (i)
TIME TO PEAK (hrs)= 6.801
RUNOFF VOLUME (mm)= 35.314
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .437

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0031-----
ADD HYD ( 2150 | ID: NHYD AREA QPEAK TPEAK R.V. DWF
(ha) (cms) (hrs) (mm) (cms)
ID1 01:205 2140 12.75 .378 7.30 35.31 .000
+ID2 02: 2140 12.75 .378 7.30 35.31 .000
SUM 03: 2150 25.64 .812 7.03 35.31 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0032-----
ROUTE CHANNEL | Routing time step (min) = 1.00
IN> 03:002150 | Number of SEGMENTS = 3
OUT< 01:002160 | Slopes (%), CHANNEL= .0500 FLOODPLAIN= .2000
LENGTH = 360.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show data for various elevations from 0.00 to 405.00.

Table with columns: DEPTH (m), ELEV (m), X-VOLUME (cu.m.), S-VOLUME (cu.m.), FLOW RATE (cms), VELOCITY (m/s), TRAV. TIME (min), D x V (m2/s). Rows show data for various depths from 0.112 to 2.200.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows include various stationing points like .071, .143, .214, etc.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: INFLOW ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 3:002150 and ID: 1:002160.

DESIGN NASHYD table with columns: Area (ha), Ia (mm), U.H. Tp (hrs), Curve Number (CN), # of Linear Res. (N). Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 2:209 and ID: 2:209.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Number of SEGMENTS, SLOPE (%), CHANNEL, FLOODPLAIN, LENGTH. Includes DATA FOR SECTION (10.0).

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows for various depths from 0.71 to 1.400.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 3:002170 and ID: 1:002180.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 3:002170 and ID: 1:002180.

DESIGN NASHYD table with columns: Area (ha), Ia (mm), U.H. Tp (hrs), Curve Number (CN), # of Linear Res. (N). Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD table with columns: Area (ha), Ia (mm), U.H. Tp (hrs), Curve Number (CN), # of Linear Res. (N). Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 03:EXT4 and ID: 03:EXT4.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 2190 and ID: 2190.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Number of SEGMENTS, SLOPE (%), CHANNEL, FLOODPLAIN, LENGTH. Includes DATA FOR SECTION (11.0).

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows for various depths from 0.71 to 1.400.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 4:002190 and ID: 1:002200.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Number of SEGMENTS, SLOPE (%), CHANNEL, FLOODPLAIN, LENGTH. Includes DATA FOR SECTION (10.0).

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows for various depths from 0.71 to 1.400.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

DESIGN NASHYD table with columns: Area (ha), Ia (mm), U.H. Tp (hrs), Curve Number (CN), # of Linear Res. (N). Includes Unit Hyd Qpeak, PEAK FLOW, TIME TO PEAK, RUNOFF VOLUME, TOTAL RAINFALL, RUNOFF COEFFICIENT.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 2210 and ID: 2210.

ROUTE CHANNEL table with columns: ROUTE CHANNEL, Number of SEGMENTS, SLOPE (%), CHANNEL, FLOODPLAIN, LENGTH. Includes DATA FOR SECTION (12.0).

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows for various depths from 0.71 to 1.400.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

Table with 7 columns: ID, AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Rows for ID: 2220 and ID: 2220.

Table with 8 columns: 1.027, 1.120, 1.213, 1.307, 1.400, 1.500, 1.600, 1.700, 1.800. Values include elevations and flow rates.

Table with 4 columns: Distance, Elevation, Manning, Flow Rate. Values range from 0.0 to 24.60.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

TRAVEL TIME TABLE

Table with 8 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Values include flow rates and depths.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV TIME, D x V. Values range from 0.30 to 570.

Table with 4 columns: DESIGN NASHYD, Area, Curve Number, DT. Values include 1.0213, 16.88, 72.00, 1.00.

Unit Hyd Qpeak (cms)= .837. PEAK FLOW (cms)= .668 (i). TIME TO PEAK (hrs)= 6.701.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

Table with 8 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Values include flow rates and depths.

Table with 8 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Values include 2240, 16.88, 6.70, 35.31.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 4 columns: DESIGN NASHYD, Area, Curve Number, DT. Values include 03:216, 10.57, 72.00, 1.00.

Unit Hyd Qpeak (cms)= .334. PEAK FLOW (cms)= .300 (i). TIME TO PEAK (hrs)= 7.201.

Table with 4 columns: ROUTE CHANNEL, Routing time step, Number of SEGMENTS, SLOPES (%). Values include 1.00, 3, 2000.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Table with 4 columns: Distance, Elevation, Manning, Flow Rate. Values range from 0.0 to 407.00.

Table with 8 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Values include 2290, 10.57, 35.31, 0.00.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Values range from 0.093 to 1.800.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 8 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Values include 2260, 284.58, 5.798, 40.44.

Unit Hyd Qpeak (cms)= .879. PEAK FLOW (cms)= .729 (i). TIME TO PEAK (hrs)= 6.701.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Table with 4 columns: ROUTE CHANNEL, Routing time step, Number of SEGMENTS, SLOPES (%). Values include 1.00, 3, 2000.

Table with 4 columns: Distance, Elevation, Manning, Flow Rate. Values range from 0.0 to 407.00.

Table with 4 columns: ADD HYD, ID, NHYD, AREA, QPEAK, TPEAK, R.V., DWF. Values include 2290, 10.57, 35.31, 0.00.

Table with 4 columns: DESIGN NASHYD, Area, Curve Number, DT. Values include 02:EXT6, 24.11, 80.00, 1.00.

Unit Hyd Qpeak (cms)= .606. PEAK FLOW (cms)= .729 (i). TIME TO PEAK (hrs)= 7.534.

Table with 10 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV.TIME, D x V. Values range from 0.093 to 1.800.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

Table with 4 columns: DESIGN NASHYD, Area, Curve Number, DT. Values include 03:211, 14.49, 82.00, 1.00.

Unit Hyd Qpeak (cms)= .517. PEAK FLOW (cms)= .607 (i). TIME TO PEAK (hrs)= 7.018.

Table with 8 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Values include flow rates and depths.

Table with 4 columns: DESIGN NASHYD, Area, Curve Number, DT. Values include 03:214, 17.47, 76.00, 1.00.

Unit Hyd Qpeak (cms)= 1.112. PEAK FLOW (cms)= 1.112.

PEAK FLOW (cms)= .921 (1)
TIME TO PEAK (hrs)= 6.501
RUNOFF VOLUME (mm)= 39.424
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .488

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0055-----
\*\*\*\*\*
# Calculate culvert routing and flow split near eastern site boundary
# - Storage volumes calculated based on site survey
# - Discharges calculated based on the 600 mm diameter CSP and 1500 mm
# diameter CSP capacities
\*\*\*\*\*

ROUTING RESULTS table with columns: ROUTE RESERVOIR, INFLOW, OUTFLOW, STORAGE, AREA, QPEAK, TPEAK, R.V.

PEAK FLOW REDUCTION (Qout/Qin) (%) = 84.322
TIME SHIFT OF PEAK FLOW (min) = 22.00
MAXIMUM STORAGE USED (ha.m.) = 5739E-01

025:0056-----
# DIVERT HYD
# INDI=01 (002300) |

Outflow / Inflow Relationships table with columns: Flow 02, Flow 03, Total (cms)

NHYD table with columns: NHYD, AREA, QPEAK, TpeakDate, R.V., NFE, WetHrs

025:0057-----
# DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=72.00
# 01:215 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
# U.H. Tp(hrs)= .860

Unit Hyd Qpeak (cms)= .237
PEAK FLOW (cms)= .195 (1)
TIME TO PEAK (hrs)= 6.801
RUNOFF VOLUME (mm)= 35.214
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .437

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0058-----
# ADD HYD ( 2330) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
# ID1 01:215 5.34 1.95 6.80 35.31 .000
# +ID2 02: 2310 15.68 .647 6.87 39.43 .000
# SUM 04: 2330 21.02 .842 6.85 38.38 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0059-----
# DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
# 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
# U.H. Tp(hrs)= 1.470

Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .612 (1)
TIME TO PEAK (hrs)= 7.468
RUNOFF VOLUME (mm)= 46.563
TOTAL RAINFALL (mm)= 80.801
RUNOFF COEFFICIENT = .576

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0060-----
# McGill Drain - Total Flow at Eastern WSP
# ADD HYD ( 2340) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
# ID1 01:EXT7 18.59 .612 7.47 46.56 .000
# +ID2 04: 2330 21.02 .842 6.85 38.38 .000
# +ID3 10: 2295 333.75 6.142 9.87 40.81 .000
# SUM 05: 2340 373.36 6.600 9.68 40.96 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0061-----
# AREA CHECK
# ADD HYD ( 2350) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
# ID1 03: 2320 1.79 .129 6.87 39.43 .000
# +ID2 05: 2340 373.36 6.600 9.68 40.96 .000
# SUM 01: 2350 375.15 6.600 9.68 40.95 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0062-----
025:0002-----
025:0002-----

025:0002-----
\*\* END OF RUN : 49

START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
TEERO = .00 hrs on 0
METOUT = 2 (output = METRIC)
NRUN = 050
NSTORM = 1
# 1=12scs50.stm

050:0002-----
# Project Name: [Windsor Solar Project] Project Number: [1335-60106]
# DATE : 02-10-2016
# Modeller : [NE]
# Company : Stantec Consulting Ltd. (London)
# License # : 4730904
# Proposed Conditions
# 25 mm Water Quality Event
# 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm

050:0002-----
# READ STORM | Filename: 50-yr scs 12 hr windsor
# Ptotal= 89.40 mm | Comments: 50-yr scs 12 hr windsor

Table with columns: TIME, RAIN, TIME, RAIN, TIME, RAIN (hrs, mm/hr)

050:0003-----
# LAPPAN DRAIN
# DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00
# 01:EXT1 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
# U.H. Tp(hrs)= 1.110

Unit Hyd Qpeak (cms)= 1.454
PEAK FLOW (cms)= 1.549 (1)
TIME TO PEAK (hrs)= 7.084
RUNOFF VOLUME (mm)= 42.489
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .475

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0004-----
# ROUTE CHANNEL | Routing time step (min) = 1.00
# IN> 01:EXT1 | Number of SEGMENTS = 3
# OUT< 02:002000 | Slopes (%), CHANNEL=.1000 FLOODPLAIN= .2000
# LENGTH = 700.00 (m)

Table with columns: Distance, Elevation, Manning

TRAVEL TIME TABLE table with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V

X-VOLUME= Total X-section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

050:0005-----
# hydrograph ---> <-pipe / channel->
# INFLOW : ID= 1:EXT1 42.26 1.549 7.08 42.489 1.315 .142
# OUTFLOW: ID= 2:002000 42.26 1.225 8.25 42.489 1.256 .191

050:0005-----
# DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00
# 01:EXT2 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
# U.H. Tp(hrs)= 1.270

Unit Hyd Qpeak (cms)= .677
PEAK FLOW (cms)= .960 (1)
TIME TO PEAK (hrs)= 7.234
RUNOFF VOLUME (mm)= 53.785
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0006-----
# DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00
# 03:EXT3 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
# U.H. Tp(hrs)= 1.110



Unit Hyd Qpeak (cms)= 1.473
PEAK FLOW (cms)= 2.020 (i)
TIME TO PEAK (hrs)= 7.051
RUNOFF VOLUME (mm)= 53.785
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

1.800 1.800 .344E+04 .405E+04\* 3.580 .468 16.03 .842
2.000 2.000 .131E+05 .171E+05\* 5.907 .203 36.88 .407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0007
# Lappan Drain - Total Flow at Pilette Road
| ADD HYD ( 2010 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (m) | (m/s)
---|---|---|---|---|---|---
01:EXT2 2000 42.26 1.225 8.25 42.49 .000
+ID2 02: 42.81 2.020 7.05 53.78 .000
+ID3 03:EXT3
SUM 04: 2010 107.59 3.916 7.30 49.35 .000

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLW : ID= 3:002030 118.02 4.104 7.65 48.644 1.845 .362
OUTFLOW: ID= 1:002040 118.02 3.957 8.22 48.644 1.830 .392

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0012
| DESIGN NASHYD | Area (ha)= 15.29 Curve Number (CN)=82.00
| 02:201 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.290

Unit Hyd Qpeak (cms)= .453
PEAK FLOW (cms)= .644 (i)
TIME TO PEAK (hrs)= 7.251
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0008
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002010 | Number of SEGMENTS = 3
| OUT< 01:002020 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000
LENGTH = 350.00 (m)

050:0013
| DESIGN NASHYD | Area (ha)= 10.88 Curve Number (CN)=72.00
| 03:204 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .850

Unit Hyd Qpeak (cms)= .489
PEAK FLOW (cms)= .472 (i)
TIME TO PEAK (hrs)= 6.784
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- DATA FOR SECTION ( 2.0 ) ----->
Distance Elevation Manning
.00 2.00 .2000
100.00 1.80 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

050:0014
| ADD HYD ( 2050 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (m) | (m/s)
---|---|---|---|---|---|---
ID1 01: 2040 118.02 3.957 8.22 48.64 .000
+ID2 02:201 15.29 .644 7.25 53.78 .000
+ID3 03:204 10.88 .472 6.78 41.39 .000
SUM 04: 2050 144.19 4.704 7.98 48.64 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .578E+02 .486E+01 .016 .096 60.50 .010
.200 .200 .136E+03 .212E+02 .052 .144 40.48 .029
.300 .300 .206E+03 .518E+02 .106 .180 32.38 .054
.400 .400 .296E+03 .993E+02 .177 .210 27.75 .084
.500 .500 .396E+03 .166E+03 .268 .236 24.67 .118
.600 .600 .508E+03 .256E+03 .377 .260 22.42 .156
.700 .700 .630E+03 .370E+03 .507 .282 20.68 .197
.800 .800 .762E+03 .512E+03 .659 .303 19.28 .242
.900 .900 .906E+03 .685E+03 .833 .322 18.12 .290
1.000 1.000 1.062E+04 .891E+03\* 1.031 .340 17.14 .340
1.100 1.100 .122E+04 .113E+04\* 1.253 .358 16.29 .394
1.200 1.200 .140E+04 .141E+04\* 1.500 .375 15.55 .450
1.300 1.300 .159E+04 .172E+04\* 1.775 .392 14.89 .509
1.400 1.400 .178E+04 .210E+04\* 2.077 .408 14.31 .571
1.500 1.500 .199E+04 .251E+04\* 2.407 .423 13.78 .635
1.600 1.600 .221E+04 .297E+04\* 2.768 .439 13.30 .702
1.700 1.700 .244E+04 .348E+04\* 3.158 .453 12.87 .771
1.800 1.800 .268E+04 .405E+04\* 3.580 .468 12.46 .842
2.000 2.000 .102E+05 .171E+05\* 5.907 .203 28.69 .407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

050:0015
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002050 | Number of SEGMENTS = 3
| OUT< 01:002060 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000
LENGTH = 200.00 (m)

<----- DATA FOR SECTION ( 4.0 ) ----->
Distance Elevation Manning
.00 2.00 .2000
100.00 1.80 .1400 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

050:0009
| DESIGN NASHYD | Area (ha)= 10.43 Curve Number (CN)=72.00
| 02:202 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .970
Unit Hyd Qpeak (cms)= .411
PEAK FLOW (cms)= .411 (i)
TIME TO PEAK (hrs)= 6.918
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .331E+02 .486E+01 .016 .096 34.57 .010
.200 .200 .722E+02 .212E+02 .052 .144 23.13 .029
.300 .300 .118E+03 .518E+02 .106 .180 18.50 .054
.400 .400 .169E+03 .993E+02 .177 .210 15.86 .084
.500 .500 .226E+03 .166E+03 .268 .236 14.10 .118
.600 .600 .290E+03 .256E+03 .377 .260 12.81 .156
.700 .700 .360E+03 .370E+03 .507 .282 11.82 .197
.800 .800 .436E+03 .512E+03 .659 .303 11.02 .242
.900 .900 .518E+03 .685E+03 .833 .322 10.36 .290
1.000 1.000 .606E+03 .891E+03\* 1.031 .340 9.79 .340
1.100 1.100 .700E+03 .113E+04\* 1.253 .358 9.31 .394
1.200 1.200 .800E+03 .141E+04\* 1.500 .375 8.89 .450
1.300 1.300 .906E+03 .173E+04\* 1.775 .392 8.51 .509
1.400 1.400 .102E+04 .210E+04\* 2.077 .408 8.18 .571
1.500 1.500 .114E+04 .251E+04\* 2.407 .423 7.87 .635
1.600 1.600 .128E+04 .297E+04\* 2.768 .439 7.60 .702
1.700 1.700 .139E+04 .348E+04\* 3.158 .453 7.35 .771
1.800 1.800 .153E+04 .405E+04\* 3.580 .468 7.12 .842
2.000 2.000 .581E+04 .171E+05\* 6.114 .210 15.84 .421

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0010
| ADD HYD ( 2030 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (m) | (m/s)
---|---|---|---|---|---|---
ID1 01: 2020 107.59 3.785 7.75 49.35 .000
+ID2 02:202 10.43 .411 6.92 41.39 .000
SUM 03: 2030 118.02 4.104 7.65 48.64 .000

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLW : ID= 4:002010 107.59 3.916 7.30 49.348 1.829 .394
OUTFLOW: ID= 1:002020 107.59 3.785 7.75 49.348 1.818 .420

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0011
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002030 | Number of SEGMENTS = 3
| OUT< 01:002040 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000
LENGTH = 450.00 (m)

050:0016
| DESIGN NASHYD | Area (ha)= 4.78 Curve Number (CN)=72.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .890

Unit Hyd Qpeak (cms)= .205
PEAK FLOW (cms)= .200 (i)
TIME TO PEAK (hrs)= 6.834
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- DATA FOR SECTION ( 3.0 ) ----->
Distance Elevation Manning
.00 2.00 .2000
100.00 1.80 .2000 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

050:0017
| ADD HYD ( 2070 ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
| (ha) | (cms) | (hrs) | (mm) | (m) | (m/s)
---|---|---|---|---|---|---
ID1 01: 2060 144.19 4.640 8.33 48.64 .000
+ID2 02:206 4.78 .200 6.83 41.39 .000
SUM 03: 2070 148.97 4.729 8.33 48.41 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .744E+02 .486E+01 .016 .096 77.79 .010
.200 .200 .163E+03 .212E+02 .052 .144 52.05 .029
.300 .300 .264E+03 .518E+02 .106 .180 41.63 .054
.400 .400 .380E+03 .993E+02 .177 .210 35.68 .084
.500 .500 .509E+03 .166E+03 .268 .236 31.72 .118
.600 .600 .653E+03 .256E+03 .377 .260 28.82 .156
.700 .700 .809E+03 .370E+03 .507 .282 26.59 .197
.800 .800 .980E+03 .512E+03 .659 .303 24.79 .242
.900 .900 .116E+04 .685E+03\* .833 .322 23.30 .290
1.000 1.000 .136E+04 .891E+03\* 1.031 .340 22.04 .340
1.100 1.100 .157E+04 .113E+04\* 1.253 .358 20.93 .394
1.200 1.200 .180E+04 .141E+04\* 1.500 .375 19.99 .450
1.300 1.300 .204E+04 .173E+04\* 1.775 .392 19.15 .509
1.400 1.400 .229E+04 .210E+04\* 2.077 .408 18.40 .571
1.500 1.500 .256E+04 .251E+04\* 2.407 .423 17.72 .635
1.600 1.600 .284E+04 .297E+04\* 2.768 .439 17.10 .702
1.700 1.700 .313E+04 .348E+04\* 3.158 .453 16.54 .771

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 03:002070 | Number of SEGMENTS = 3
| OUT: 01:002080 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 500.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show elevation points from 200.00 to 407.00 and Manning values of 0.1400 and 0.0850.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show flow characteristics at various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph data: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL.
INFLOW: ID= 3:002070 148.97 4.729 8.33 48.409 1.959 .216
OUTFLOW: ID= 1:002080 148.97 4.317 9.02 48.409 1.942 .228

DESIGN NASHYD | Area (ha)= 14.96 Curve Number (CN)=72.00
| 02:207 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.330

Unit Hyd Qpeak (cms)= .430
PEAK FLOW (cms)= .465 (i)
TIME TO PEAK (hrs)= 7.334
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD | Area (ha)= 7.92 Curve Number (CN)=72.00
| 03:208 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110

Unit Hyd Qpeak (cms)= .273
PEAK FLOW (cms)= .282 (i)
TIME TO PEAK (hrs)= 7.084
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DESIGN NASHYD | Area (ha)= 14.96 Curve Number (CN)=82.00
| 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .389 (i)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 04:002090 | Number of SEGMENTS = 3
| OUT: 01:002100 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 130.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show elevation points from 200.00 to 407.00 and Manning values of 0.1400 and 0.0850.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show flow characteristics at various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph data: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL.
INFLOW: ID= 4:002090 171.85 4.715 8.78 47.475 1.965 .205
OUTFLOW: ID= 1:002100 171.85 4.675 9.05 47.475 1.962 .208

DESIGN NASHYD | Area (ha)= 4.95 Curve Number (CN)=73.00
| 02:212 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .480

Unit Hyd Qpeak (cms)= .394
PEAK FLOW (cms)= .325 (i)
TIME TO PEAK (hrs)= 6.351
RUNOFF VOLUME (mm)= 42.489
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .475

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD ( 2110 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2100 171.85 4.675 9.05 47.47 0.00
+ID2 02:212 4.95 3.25 6.35 42.49 0.00
SUM 03: 2110 176.80 4.713 9.05 47.33 0.00

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 03:002110 | Number of SEGMENTS = 3
| OUT: 01:002120 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 330.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show elevation points from 200.00 to 407.00 and Manning values of 0.1400 and 0.0850.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show flow characteristics at various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph data: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL.
INFLOW: ID= 3:002110 176.80 4.713 9.05 47.335 1.965 .206
OUTFLOW: ID= 1:002120 176.80 4.506 9.67 47.335 1.955 .213

DESIGN NASHYD | Area (ha)= 6.60 Curve Number (CN)=82.00
| 02:EXT8 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .820

Unit Hyd Qpeak (cms)= .307
PEAK FLOW (cms)= .389 (i)
TIME TO PEAK (hrs)= 6.734
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 04:002090 | Number of SEGMENTS = 3
| OUT: 01:002100 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 130.00 (m)

Table with columns: Distance, Elevation, Manning. Rows show elevation points from 200.00 to 407.00 and Manning values of 0.1400 and 0.0850.

TRAVEL TIME TABLE with columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Rows show flow characteristics at various depths from 0.112 to 2.200.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

DESIGN NASHYD | Area (ha)= 12.75 Curve Number (CN)=72.00
| 01:203 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .970

Unit Hyd Qpeak (cms)= .502
PEAK FLOW (cms)= .502 (i)
TIME TO PEAK (hrs)= 6.918
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

IND 01:203	Number of SEGMENTS = 3
OUT< 02:002140	Slopes (%), CHANNEL= .3500 FLOODPLAIN= .2000
	LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 8.0) ----->

Distance	Elevation	Manning	Flow Rate	Velocity	Trav Time	D x V
.00	1.40	.1400				
200.00	1.00	.1400 / .1000	Main Channel			
201.50	.00	.1000	Main Channel			
203.50	.00	.1000	Main Channel			
205.00	1.00	.1000 / .2000	Main Channel			
405.00	1.40	.2000				

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV TIME (min)	D x V (m2/s)
.071	.071	.753E+02	.154E+01	.015	.097	85.67	.007
.143	.143	.138E+03	.646E+01	.047	.149	56.11	.021
.214	.214	.249E+03	.135E+02	.094	.188	44.28	.040
.286	.286	.347E+03	.283E+02	.154	.221	37.63	.063
.357	.357	.453E+03	.462E+02	.227	.250	33.27	.089
.429	.429	.566E+03	.693E+02	.313	.276	30.14	.118
.500	.500	.687E+03	.982E+02	.413	.300	27.75	.150
.571	.571	.816E+03	.133E+03	.526	.322	25.85	.184
.643	.643	.953E+03	.175E+03	.654	.343	24.30	.220
.714	.714	.110E+04	.224E+03	.795	.362	22.99	.259
.786	.786	.128E+04	.280E+03	.952	.381	21.87	.299
.857	.857	.141E+04	.345E+03	1.123	.399	20.90	.342
.929	.929	.158E+04	.418E+03	1.310	.416	20.04	.386
1.000	1.000	.175E+04	.500E+03	1.513	.432	19.28	.432
1.080	1.080	1.913E+04	.629E+03	1.629	.449	18.62	.491
1.160	1.160	.855E+04	.283E+04	2.777	.162	51.31	.188
1.240	1.240	.167E+05	.593E+04	4.375	.131	63.81	.162
1.320	1.320	.281E+05	.106E+05	6.931	.123	67.70	.162
1.400	1.400	.427E+05	.171E+05	10.642	.124	66.95	.174

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

INFLOW : ID= 1:203	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
OUTFLOW : ID= 2:002140	12.75	.448	7.28	41.389	.522	.307

050:0030-----

DESIGN NASHYD	Area (ha)= 12.89	Curve Number (CN)=72.00
01:205 DT= 1.00	Ia (mm)= 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .860	

Unit Hyd Qpeak (cms)= .572

PEAK FLOW (cms)= .554 (i)

TIME TO PEAK (hrs)= 6.801

RUNOFF VOLUME (mm)= 41.389

TOTAL RAINFALL (mm)= 89.400

RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0031-----

ADD HYD ( 2150)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:205	12.89	.554	6.80	41.39	.000
+ID2 02: 2140	12.75	.448	7.28	41.39	.000
SUM 03:	2150	25.64	.961	7.02	41.39 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0032-----

ROUTE CHANNEL   Routing time step (min) = 1.00	
IND 03:002150   Number of SEGMENTS = 3	
OUT< 01:002160   Slopes (%), CHANNEL= .0500 FLOODPLAIN= .2000	
	LENGTH = 360.00 (m)

<----- DATA FOR SECTION ( 9.0) ----->

Distance	Elevation	Manning	Flow Rate	Velocity	Trav Time	D x V
.00	1.40	.1400				
200.00	1.00	.1400 / .1000	Main Channel			
201.50	.00	.1000	Main Channel			
203.50	.00	.1000	Main Channel			
205.00	1.00	.1000 / .2000	Main Channel			
405.00	1.40	.2000				

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV TIME (min)	D x V (m2/s)
.071	.071	.542E+02	.108E+02	.006	.037	163.19	.003
.143	.143	.114E+03	.452E+02	.018	.056	106.89	.008
.214	.214	.179E+03	.107E+03	.035	.071	84.35	.015
.286	.286	.250E+03	.198E+03	.058	.084	71.69	.024
.357	.357	.326E+03	.323E+03	.086	.095	63.38	.034
.429	.429	.408E+03	.485E+03	.118	.105	57.41	.045
.500	.500	.495E+03	.687E+03	.156	.113	52.87	.057
.571	.571	.588E+03	.933E+03	.199	.122	49.25	.070
.643	.643	.686E+03	.123E+04	.247	.130	46.29	.083
.714	.714	.790E+03	.157E+04	.301	.137	43.80	.098
.786	.786	.899E+03	.196E+04	.360	.144	41.67	.113
.857	.857	.101E+04	.241E+04	.424	.151	39.81	.129
.929	.929	.113E+04	.293E+04	.495	.157	38.18	.146
1.000	1.000	.126E+04	.350E+04	.572	.163	36.73	.163
1.080	1.080	.256E+04	.767E+04	.786	.111	54.17	.120
1.160	1.160	.616E+04	.198E+05	1.451	.085	70.71	.098
1.240	1.240	.121E+05	.415E+05	2.837	.085	70.85	.105
1.320	1.320	.203E+05	.743E+05	5.168	.092	65.36	.121
1.400	1.400	.308E+05	.120E+06	8.644	.101	59.35	.142

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

INFLOW : ID= 3:002150	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
OUTFLOW : ID= 1:002160	25.64	.961	7.02	41.389	1.101	.103
						1.052

050:0033-----

DESIGN NASHYD	Area (ha)= 15.50	Curve Number (CN)=72.00
02:209 DT= 1.00	Ia (mm)= 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .970	

Unit Hyd Qpeak (cms)= .610

PEAK FLOW (cms)= .610 (i)

TIME TO PEAK (hrs)= 6.918

RUNOFF VOLUME (mm)= 41.389

TOTAL RAINFALL (mm)= 89.400

RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0034-----

ADD HYD ( 2170)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01: 2160	25.64	.709	7.75	41.39	.000
+ID2 02:209	15.50	.610	6.92	41.39	.000
SUM 03:	2170	41.14	1.232	7.22	41.39 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0035-----

ROUTE CHANNEL   Routing time step (min) = 1.00	
IND 03:002170   Number of SEGMENTS = 3	
OUT< 01:002180   Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000	
	LENGTH = 250.00 (m)

<----- DATA FOR SECTION ( 10.0) ----->

Distance	Elevation	Manning	Flow Rate	Velocity	Trav Time	D x V
.00	1.40	.2000				
200.00	1.00	.2000 / .1000	Main Channel			
201.50	.00	.1000	Main Channel			
203.50	.00	.1000	Main Channel			
205.00	1.00	.1000 / .2000	Main Channel			
405.00	1.40	.2000				

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV TIME (min)	D x V (m2/s)
.071	.071	.376E+02	.358E+01	.010	.064	65.43	.005
.143	.143	.791E+02	.151E+02	.031	.097	42.85	.014
.214	.214	.124E+03	.355E+02	.061	.123	33.82	.026
.286	.286	.173E+03	.661E+02	.101	.145	28.74	.041
.357	.357	.226E+03	.108E+03	.148	.164	25.41	.059
.429	.429	.283E+03	.162E+03	.205	.181	23.02	.078
.500	.500	.344E+03	.229E+03	.270	.197	21.20	.098
.571	.571	.408E+03	.311E+03	.344	.211	19.75	.121
.643	.643	.476E+03	.408E+03	.428	.225	18.56	.144
.714	.714	.548E+03	.522E+03	.521	.237	17.56	.169
.786	.786	.624E+03	.654E+03	.623	.249	16.71	.196
.857	.857	.704E+03	.805E+03	.735	.261	15.96	.224
.929	.929	.788E+03	.975E+03	.858	.272	15.31	.253
1.000	1.000	.875E+03	.117E+04	.990	.283	14.73	.283
1.080	1.080	.177E+04	.256E+04	1.270	.179	23.30	.193
1.160	1.160	.427E+04	.661E+04	1.927	.113	36.97	.131
1.240	1.240	.837E+04	.138E+05	3.185	.095	43.82	.118
1.320	1.320	.141E+05	.248E+05	5.229	.093	44.86	.123
1.400	1.400	.214E+05	.399E+05	8.222	.096	43.33	.135

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

INFLOW : ID= 3:002170	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
OUTFLOW : ID= 1:002180	41.14	1.151	7.85	41.389	1.046	.212

050:0036-----

DESIGN NASHYD	Area (ha)= 7.27	Curve Number (CN)=82.00
02:210 DT= 1.00	Ia (mm)= 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= .820	

Unit Hyd Qpeak (cms)= .339

PEAK FLOW (cms)= .428 (i)

TIME TO PEAK (hrs)= 6.734

RUNOFF VOLUME (mm)= 53.784

TOTAL RAINFALL (mm)= 89.400

RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0037-----

DESIGN NASHYD	Area (ha)= 21.08	Curve Number (CN)=80.00
03:EXT4 DT= 1.00	Ia (mm)= 1.500	# of Linear Res. (N)= 3.00
	U.H. Tp(hrs)= 1.830	

Unit Hyd Qpeak (cms)= .440

PEAK FLOW (cms)= .642 (i)

TIME TO PEAK (hrs)= 7.901

RUNOFF VOLUME (mm)= 51.033

TOTAL RAINFALL (mm)= 89.400

RUNOFF COEFFICIENT = .571

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0038-----

#####  
# McGill Drain - Total Flow at Jefferson Boulevard  
#####

ADD HYD ( 2190)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01: 2180	41.14	1.151	7.85	41.39	.000
+ID2 02:210	7.27	.428	6.73	53.78	.000
+ID3 03:EXT4	21.08	.642	7.90	51.03	.000
SUM 04:	2190	69.49	2.034	7.63	45.61 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0039-----

ROUTE CHANNEL   Routing time step (min) = 1.00	
IND 04:002190   Number of SEGMENTS = 3	
OUT< 01:002200   Slopes (%), CHANNEL= .3000 FLOODPLAIN= .2000	
	LENGTH = 280.00 (m)

<----- DATA FOR SECTION ( 11.0) ----->

Distance	Elevation	Manning	Flow Rate	Velocity	Trav Time	D x V
.00	1.40	.2000				
200.00	1.00	.2000 / .1000	Main Channel			
201.50	.00	.1000	Main Channel			
203.50	.00	.1000	Main Channel			
205.00	1.00	.1000 / .2000	Main Channel			
405.00	1.40	.2000				

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV TIME (min)	D x V (m2/s)
.071	.071	.421E+02	.179E+01	.014	.090	51.82	.006
.143	.143	.886E+02	.753E+01	.043	.138	33.94	.020
.214	.214	.139E+03	.178E+02	.087	.174	26.78	.037
.286	.286	.194E+03	.330E+02	.142	.205	22.76	.059
.357	.357	.254E+03	.539E+02	.210	.232	20.12	.083
.429	.429	.317E+03	.809E+02	.290	.256	18.23	.110
.500	.500	.385E+03	.115E+03	.382	.278	16.79	.139
.571	.571	.457E+03	.155E+03	.487	.298	15.64	.171
.643	.643	.534E+03	.204E+03	.605	.318	14.70	.204
.714	.714	.614E+03	.261E+03	.736	.336	13.91	.240

Table with 7 columns of numerical data, likely representing flow or volume metrics at different points.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0046----- ROUTE CHANNEL | Routing time step (min) = 1.00 | IN< 03:002240 | Number of SEGMENTS = 3 | OUT< 01:002250 | Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000 LENGTH= 170.00 (m)

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- DATA FOR SECTION ( 13.0 ) ----->

Table with 4 columns: Distance, Elevation, Manning, and Channel Name. Shows data for a main channel at various elevations.

<--- hydrograph ---> <-pipe / channel->

Table with 6 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Shows peak flow characteristics for different inflow/outflow scenarios.

<----- TRAVEL TIME TABLE ----->

Large table with 8 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Provides detailed travel time and volume data for various depths and elevations.

050:0040----- | DESIGN NASHYD | Area (ha)= 14.81 Curve Number (CN)=82.00 | 02:EXT5 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00 U.H. Tp(hrs)= 1.520

Unit Hyd Qpeak (cms)= .372 PEAK FLOW (cms)= .550 (i) TIME TO PEAK (hrs)= 7.518 RUNOFF VOLUME (mm)= 53.785 TOTAL RAINFALL (mm)= 89.400 RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0041----- | ADD HYD ( 2210 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) (cms) (cms) ID1 01: 2200 69.49 1.955 8.45 45.61 .000 +ID2 02:EXT5 14.81 .550 7.52 53.78 .000 SUM 03: 2210 84.30 2.430 8.23 47.05 .000

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph ---> <-pipe / channel->

Table with 6 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Shows peak flow characteristics for a different inflow/outflow scenario.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0042----- | ADD HYD ( 2220 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) (cms) (cms) ID1 03: 2210 84.30 2.430 8.23 47.05 .000 +ID2 02: 2130 183.40 4.572 9.65 47.57 .000 SUM 01: 2220 267.70 6.598 8.88 47.40 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0047----- | DESIGN NASHYD | Area (ha)= 24.11 Curve Number (CN)=80.00 | 02:EXT6 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00 U.H. Tp(hrs)= 1.520

Unit Hyd Qpeak (cms)= .606 PEAK FLOW (cms)= .847 (i) TIME TO PEAK (hrs)= 7.534 RUNOFF VOLUME (mm)= 51.033 TOTAL RAINFALL (mm)= 89.400 RUNOFF COEFFICIENT = .571

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0043----- | ROUTE CHANNEL | Routing time step (min) = 1.00 | IN< 01:002220 | Number of SEGMENTS = 3 | OUT< 02:002230 | Slopes (%), CHANNEL= .1500 FLOODPLAIN= .2000 LENGTH= 200.00 (m)

<----- DATA FOR SECTION ( 12.0 ) ----->

Table with 4 columns: Distance, Elevation, Manning, and Channel Name. Shows data for a main channel at various elevations.

<----- TRAVEL TIME TABLE ----->

Large table with 8 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Provides detailed travel time and volume data for various depths and elevations.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION. (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<--- hydrograph ---> <-pipe / channel->

Table with 6 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Shows peak flow characteristics for different inflow/outflow scenarios.

050:0044----- | DESIGN NASHYD | Area (ha)= 16.88 Curve Number (CN)=72.00 | 01:213 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00 U.H. Tp(hrs)= .770

Unit Hyd Qpeak (cms)= .837 PEAK FLOW (cms)= .785 (i) TIME TO PEAK (hrs)= 6.701 RUNOFF VOLUME (mm)= 41.389 TOTAL RAINFALL (mm)= 89.400 RUNOFF COEFFICIENT = .463

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0045----- | ADD HYD ( 2240 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF (ha) (cms) (hrs) (mm) (cms) (cms) ID1 01:213 16.88 .785 6.70 41.39 .000 +ID2 02: 2230 267.70 6.429 9.37 47.40 .000 SUM 03: 2240 284.58 6.581 9.28 47.05 .000

050:0048----- | DESIGN NASHYD | Area (ha)= 14.49 Curve Number (CN)=82.00 | 03:211 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00 U.H. Tp(hrs)= 1.070

Unit Hyd Qpeak (cms)= .517 PEAK FLOW (cms)= .703 (i) TIME TO PEAK (hrs)= 7.001 RUNOFF VOLUME (mm)= 53.784 TOTAL RAINFALL (mm)= 89.400 RUNOFF COEFFICIENT = .602

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0049----- | ROUTE CHANNEL | Routing time step (min) = 1.00 | IN< 03:211 | Number of SEGMENTS = 3 | OUT< 04:002280 | Slopes (%), CHANNEL= .2000 FLOODPLAIN= .2000 LENGTH= 500.00 (m)

<----- DATA FOR SECTION ( 15.0 ) ----->

Table with 4 columns: Distance, Elevation, Manning, and Channel Name. Shows data for a main channel at various elevations.

<----- TRAVEL TIME TABLE ----->

Large table with 8 columns: DEPTH, ELEV, X-VOLUME, S-VOLUME, FLOW RATE, VELOCITY, TRAV. TIME, D x V. Provides detailed travel time and volume data for various depths and elevations.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH. S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

<--- hydrograph ---> <-pipe / channel->

Table with 6 columns: AREA, QPEAK, TPEAK, R.V., MAX DEPTH, MAX VEL. Shows peak flow characteristics for different inflow/outflow scenarios.

050:0050----- | DESIGN NASHYD | Area (ha)= 10.57 Curve Number (CN)=72.00 | 03:216 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00 U.H. Tp(hrs)= 1.210



Unit Hyd Qpeak (cms)= .334
PEAK FLOW (cms)= .353 (i)
TIME TO PEAK (hrs)= 7.201
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090

Table with columns: NHYD, AREA (ha), QPEAK (cms), TpeakDate\_hh:mm, R.V. (mm), NFE WetHrs (hrs). Rows include IDin=01:002300, IDout=02:002310, IDout=03:002320.

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
050:0051
| ADD HYD ( 2290 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 03:216 10.57 .353 7.20 41.39 .000
+ID2 04: 2280 14.49 .672 7.25 53.78 .000
SUM 05: 2290 25.06 1.025 7.23 48.56 .000

050:0057
| DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=72.00
| 01:215 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .860

Unit Hyd Qpeak (cms)= .237
PEAK FLOW (cms)= .230 (i)
TIME TO PEAK (hrs)= 6.801
RUNOFF VOLUME (mm)= 41.389
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .463

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
050:0052
| ADD HYD ( 2260 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01: 2250 284.58 6.479 9.62 47.05 .000
+ID2 02:EXT6 24.11 .847 7.53 51.03 .000
+ID3 05: 2290 25.06 1.025 7.23 48.56 .000
SUM 03: 2260 333.75 7.372 9.10 47.45 .000

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0058
| ADD HYD ( 2330 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01:215 5.34 .230 6.80 41.39 .000
+ID2 02: 2310 15.35 .692 6.97 45.99 .000
SUM 04: 2330 20.69 .920 6.85 44.80 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0053
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002260 | Number of SEGMENTS = 3
| OUT< 10:002295 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000
LENGTH = 370.00 (m)

050:0059
| DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
| 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.470

Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .709 (i)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 53.784
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .602

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

DATA FOR SECTION ( 14.0 )
Distance Elevation Manning
.00 1.80 1.400
200.00 1.40 .1400 / .0850 Main Channel
202.60 .00 .0850 Main Channel
204.40 .00 .0850 Main Channel
207.00 1.40 .0850 / .2000 Main Channel
407.00 1.80 .2000

050:0060
#\*\*\*\*\*
# McGill Drain - Total Flow at Eastern WSP
#\*\*\*\*\*
| ADD HYD ( 2340 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 01:EXT7 18.59 .709 7.45 53.78 .000
+ID2 05: 2330 20.69 .920 6.85 44.80 .000
+ID3 10: 2295 333.75 6.903 10.12 47.45 .000
SUM 05: 2340 373.03 7.506 9.77 47.62 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

hydrograph <-> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
INFLOW : ID= 3:002260 333.75 7.372 9.10 47.448 1.724 1.119
OUTFLOW: ID=10:002295 333.75 6.903 10.12 47.448 1.713 1.119

050:0061
# AREA CHECK
#\*\*\*\*\*
| ADD HYD ( 2350 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 03: 2320 2.12 .143 6.97 45.99 .000
+ID2 05: 2340 373.03 7.506 9.77 47.62 .000
SUM 01: 2350 375.15 7.524 9.77 47.61 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0054
| DESIGN NASHYD | Area (ha)= 17.47 Curve Number (CN)=76.00
| 03:214 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .600
Unit Hyd Qpeak (cms)= 1.112
PEAK FLOW (cms)= 1.077 (i)
TIME TO PEAK (hrs)= 6.484
RUNOFF VOLUME (mm)= 45.961
TOTAL RAINFALL (mm)= 89.400
RUNOFF COEFFICIENT = .514
(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0062
| ADD HYD ( 2350 ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
ID1 03: 2320 2.12 .143 6.97 45.99 .000
+ID2 05: 2340 373.03 7.506 9.77 47.62 .000
SUM 01: 2350 375.15 7.524 9.77 47.61 .000

\*\* END OF RUN : 99

050:0055
# Calculate culvert routing and flow split near eastern site boundary
# - Storage volumes calculated based on site survey
# - Discharges calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03: (214 ) |
| OUT<01: (002300) |
===== OUTFLOW STORAGE TABLE =====
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | 1.130 .4600E+00
.150 .0000E+00 | 5.470 .8100E+00
.450 .0000E+00 | 83.090 .3400E+01
.820 .6500E-01 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm) (m)
INFLOW >03: (214 ) 17.47 1.077 6.484 45.961
OUTFLOW<01: (002300) 17.47 .835 6.968 45.987
PEAK FLOW REDUCTION [Qout/Qin] (%) = 77.491
TIME SHIFT OF PEAK FLOW (min) = 29.00
MAXIMUM STORAGE USED (ha.m.) = .8405E-01

050:0062
| START | Project dir.: F:\WSP\
Rainfall dir.: F:\WSP\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 100
NSTORM= 1
# 1=12scs100.stm
100:0002
# Project Name: [Windsor Solar Project] Project Number: [1335-60106]
# Date : 02-10-2016
# Modeller : [ME]
# Company : Stantec Consulting Ltd. (London)
# License # : 4730904
# Proposed Conditions
# 25 mm Water Quality Event
# 2, 5, 10, 25, 50, 100, 250-year 3-Hour Chicago Design Storm
100:0002
| READ STORM | Filename: 100-yr scs 12 hr windsor
| Ptotal= 98.00 mm | Comments: 100-yr scs 12 hr windsor
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.50 1.960 | 3.50 3.920 | 6.50 17.640 | 9.50 3.920
1.00 1.960 | 4.00 3.920 | 7.00 7.840 | 10.00 1.960
1.50 1.960 | 4.50 5.880 | 7.50 5.880 | 10.50 1.960
2.00 1.960 | 5.00 7.840 | 8.00 5.880 | 11.00 1.960
2.50 3.920 | 5.50 11.760 | 8.50 3.920 | 11.50 1.960

3.00 3.920 | 6.00 88.200 | 9.00 3.920 | 12.00 1.960

-----  
 100:0003-----  
 \*\*\*\*\*  
 # LAPPAN DRAIN  
 \*\*\*\*\*  
 | DESIGN NASHYD | Area (ha)= 42.26 Curve Number (CN)=73.00  
 | 01:EXT1 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= 1.110
 Unit Hyd Qpeak (cms)= 1.454  
 PEAK FLOW (cms)= 1.788 (i)  
 TIME TO PEAK (hrs)= 7.068  
 RUNOFF VOLUME (mm)= 48.897  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .499  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100	.100	.578E+02	.486E+01	.016	.096	60.50	.010
200	.200	.126E+03	.212E+02	.052	.144	40.48	.029
300	.300	.206E+03	.513E+02	.106	.180	32.38	.054
400	.400	.296E+03	.993E+02	.177	.210	27.75	.084
500	.500	.396E+03	1.66E+03	.268	.236	24.67	.118
600	.600	.508E+03	2.56E+03	.377	.260	22.42	.156
700	.700	.630E+03	3.70E+03	.507	.282	20.68	.197
800	.800	.762E+03	5.12E+03	.659	.303	19.28	.242
900	.900	.906E+03	6.85E+03	.833	.322	18.12	.290
1000	1.000	1.062E+04	8.91E+03	1.031	.340	17.14	.340
1100	1.100	1.222E+04	1.13E+04	1.253	.358	16.29	.394
1200	1.200	1.402E+04	1.41E+04	1.500	.375	15.55	.450
1300	1.300	1.592E+04	1.73E+04	1.775	.392	14.89	.509
1400	1.400	1.782E+04	2.10E+04	2.077	.408	14.31	.571
1500	1.500	1.982E+04	2.51E+04	2.407	.423	13.78	.635
1600	1.600	2.212E+04	2.97E+04	2.768	.439	13.30	.702
1700	1.700	2.442E+04	3.48E+04	3.158	.453	12.87	.771
1800	1.800	2.682E+04	4.05E+04	3.580	.468	12.46	.842
2000	2.000	3.02E+05	4.71E+05	5.907	.203	28.69	.407

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

100:0004-----  
 -----  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN: 01:EXT1 | Number of SEGMENTS = 3  
 | OUT: 02:002000 | Slopes (%), CHANNEL= 1000 FLOODPLAIN= .2000  
LENGTH = 700.00 (m)
 <----- DATA FOR SECTION ( 1.0) ----->  
 Distance Elevation Manning  
 .00 1.40 .2000  
 100.00 1.20 .2000 / .0850 Main Channel  
 101.80 .00 .0850 Main Channel  
 103.00 .00 .0850 Main Channel  
 104.80 1.20 .0850 / .2000 Main Channel  
 204.80 1.40 .2000

----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID = 4:002010 107.59 4.402 7.23 56.344 1.871 .321  
 OUTFLOW : ID = 1:002020 107.59 4.173 7.83 56.344 1.849 .356

100:0009-----  
 -----  
 | DESIGN NASHYD | Area (ha)= 10.43 Curve Number (CN)=72.00  
 | 02:202 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= .970
 Unit Hyd Qpeak (cms)= .411  
 PEAK FLOW (cms)= .475 (i)  
 TIME TO PEAK (hrs)= 6.918  
 RUNOFF VOLUME (mm)= 47.169  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .487  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .071 .071 .64E+03 .32E+03 .005 .059 197.27 .004  
 .141 .141 .140E+03 .141E+02 .018 .089 131.37 .013  
 .212 .212 .225E+03 .340E+02 .036 .111 104.80 .024  
 .282 .282 .321E+03 .647E+02 .060 .130 89.71 .037  
 .353 .353 .427E+03 .108E+03 .089 .146 79.68 .052  
 .424 .424 .544E+03 .168E+03 .128 .161 72.40 .068  
 .494 .494 .671E+03 .237E+03 .168 .175 66.79 .086  
 .565 .565 .809E+03 .326E+03 .217 .187 62.29 .106  
 .635 .635 .957E+03 .434E+03 .272 .199 58.56 .127  
 .706 .706 .112E+04 .563E+03 .336 .211 55.41 .149  
 .776 .776 .129E+04 .713E+03 .407 .221 52.69 .172  
 .847 .847 .146E+04 .886E+03 .485 .232 50.32 .196  
 .918 .918 .166E+04 .108E+04 .572 .242 48.22 .222  
 .988 .988 .186E+04 .131E+04 .657 .252 46.35 .249  
 1.059 1.059 .207E+04 .156E+04 .771 .261 44.66 .277  
 1.129 1.129 .229E+04 .185E+04 .884 .271 43.13 .306  
 1.200 1.200 .252E+04 .216E+04 .1006 .280 41.73 .335  
 1.300 1.300 .332E+04 .290E+04 .1392 .313 36.12 .199  
 1.400 1.400 .472E+05 .172E+05 .2456 .400 116.67 .140

100:0010-----  
 -----  
 | ADD HYD ( 2030) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (m)  
 ID1 01: 2020 107.59 4.173 7.83 56.34 .000  
 +ID2 02:202 10.43 .475 6.92 47.69 .000  
 -----  
 SUM 03: 2030 118.02 4.506 7.63 55.58 .000  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID = 1:EXT1 42.26 1.788 7.07 48.897 1.337 .128  
 OUTFLOW : ID = 2:002000 42.26 1.336 8.50 48.897 1.285 .164

100:0011-----  
 -----  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN: 03:002030 | Number of SEGMENTS = 3  
 | OUT: 01:002040 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000  
LENGTH = 450.00 (m)
 <----- DATA FOR SECTION ( 3.0) ----->  
 Distance Elevation Manning  
 .00 2.00 .2000  
 100.00 1.80 .2000 / .0850 Main Channel  
 102.75 .00 .0850 Main Channel  
 104.25 .00 .0850 Main Channel  
 107.00 1.80 .0850 / .1400 Main Channel  
 207.00 2.00 .1400

100:0005-----  
 -----  
 | DESIGN NASHYD | Area (ha)= 22.52 Curve Number (CN)=82.00  
 | 01:EXT2 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= 1.270
 Unit Hyd Qpeak (cms)= .677  
 PEAK FLOW (cms)= 1.094 (i)  
 TIME TO PEAK (hrs)= 7.218  
 RUNOFF VOLUME (mm)= 61.161  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .624  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .100 .100 .744E+02 4.86E+01 .016 .096 77.79 .010  
 .200 .200 .163E+03 2.12E+02 .052 .144 52.05 .029  
 .300 .300 .264E+03 5.18E+02 .106 .180 41.63 .054  
 .400 .400 .380E+03 9.93E+02 .177 .210 35.68 .084  
 .500 .500 .509E+03 1.66E+03 .268 .236 31.72 .118  
 .600 .600 .653E+03 2.56E+03 .377 .260 28.82 .156  
 .700 .700 .809E+03 3.70E+03 .507 .282 26.59 .197  
 .800 .800 .980E+03 5.12E+03 .659 .303 24.79 .242  
 .900 .900 .116E+04 6.85E+03 .833 .322 23.30 .290  
 1.000 1.000 .136E+04 8.91E+03 1.031 .340 22.04 .340  
 1.100 1.100 .157E+04 1.13E+04 1.253 .358 20.95 .394  
 1.200 1.200 .180E+04 1.41E+04 1.500 .375 19.99 .450  
 1.300 1.300 .204E+04 1.73E+04 1.775 .392 19.15 .509  
 1.400 1.400 .229E+04 2.10E+04 2.077 .408 18.40 .571  
 1.500 1.500 .256E+04 2.51E+04 2.407 .423 17.72 .635  
 1.600 1.600 .284E+04 2.97E+04 2.768 .439 17.10 .702  
 1.700 1.700 .313E+04 3.48E+04 3.158 .453 16.54 .771  
 1.800 1.800 .344E+04 4.05E+04 3.580 .468 16.03 .842  
 2.000 2.000 .471E+05 4.71E+05 5.907 .203 36.88 .407

100:0006-----  
 -----  
 | DESIGN NASHYD | Area (ha)= 42.81 Curve Number (CN)=82.00  
 | 03:EXT3 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= 1.110
 Unit Hyd Qpeak (cms)= 1.473  
 PEAK FLOW (cms)= 2.302 (i)  
 TIME TO PEAK (hrs)= 7.051  
 RUNOFF VOLUME (mm)= 61.161  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .624  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID = 3:002030 118.02 4.506 7.63 55.579 1.880 .308  
 OUTFLOW : ID = 1:002040 118.02 4.294 8.35 55.579 1.863 .332

100:0007-----  
 -----  
 # Lappan Drain - Total Flow at Pilette Road  
 \*\*\*\*\*  
 | ADD HYD ( 2010) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (m)  
 ID1 01:EXT2 22.52 1.094 7.22 61.16 .000  
 +ID2 02: 2000 42.26 1.336 8.50 48.90 .000  
 +ID3 03:EXT3 42.81 2.302 7.05 61.16 .000  
 -----  
 SUM 04: 2010 107.59 4.402 7.23 56.34 .000  
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0012-----  
 -----  
 | DESIGN NASHYD | Area (ha)= 15.29 Curve Number (CN)=82.00  
 | 02:201 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= 1.290
 Unit Hyd Qpeak (cms)= .453  
 PEAK FLOW (cms)= .734 (i)  
 TIME TO PEAK (hrs)= 7.251  
 RUNOFF VOLUME (mm)= 61.161  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .624  
 (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0008-----  
 -----  
 | ROUTE CHANNEL | Routing time step (min) = 1.00  
 | IN: 04:002010 | Number of SEGMENTS = 3  
 | OUT: 01:002020 | Slopes (%), CHANNEL= 1700 FLOODPLAIN= .2000  
LENGTH = 350.00 (m)
 <----- DATA FOR SECTION ( 2.0) ----->  
 Distance Elevation Manning  
 .00 2.00 .2000  
 100.00 1.80 .2000 / .0850 Main Channel  
 102.75 .00 .0850 Main Channel  
 104.25 .00 .0850 Main Channel  
 107.00 1.80 .0850 / .1400 Main Channel  
 207.00 2.00 .1400

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
 S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
 (\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<----- hydrograph -----> <-pipe / channel->  
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL  
 (ha) (cms) (hrs) (mm) (m) (m/s)  
 INFLOW : ID = 3:002030 118.02 4.506 7.63 55.579 1.880 .308  
 OUTFLOW : ID = 1:002040 118.02 4.294 8.35 55.579 1.863 .332

<----- TRAVEL TIME TABLE ----->  
 DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V  
 (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)  
 .071 .071 .64E+03 .32E+03 .005 .059 197.27 .004  
 .141 .141 .140E+03 .141E+02 .018 .089 131.37 .013  
 .212 .212 .225E+03 .340E+02 .036 .111 104.80 .024  
 .282 .282 .321E+03 .647E+02 .060 .130 89.71 .037  
 .353 .353 .427E+03 .108E+03 .089 .146 79.68 .052  
 .424 .424 .544E+03 .168E+03 .128 .161 72.40 .068  
 .494 .494 .671E+03 .237E+03 .168 .175 66.79 .086  
 .565 .565 .809E+03 .326E+03 .217 .187 62.29 .106  
 .635 .635 .957E+03 .434E+03 .272 .199 58.56 .127  
 .706 .706 .112E+04 .563E+03 .336 .211 55.41 .149  
 .776 .776 .129E+04 .713E+03 .407 .221 52.69 .172  
 .847 .847 .146E+04 .886E+03 .485 .232 50.32 .196  
 .918 .918 .166E+04 .108E+04 .572 .242 48.22 .222  
 .988 .988 .186E+04 .131E+04 .657 .252 46.35 .249  
 1.059 1.059 .207E+04 .156E+04 .771 .261 44.66 .277  
 1.129 1.129 .229E+04 .185E+04 .884 .271 43.13 .306  
 1.200 1.200 .252E+04 .216E+04 .1006 .280 41.73 .335  
 1.300 1.300 .332E+04 .290E+04 .1392 .313 36.12 .199  
 1.400 1.400 .472E+05 .172E+05 .2456 .400 116.67 .140

100:0013-----  
 -----  
 | DESIGN NASHYD | Area (ha)= 10.88 Curve Number (CN)=72.00  
 | 03:204 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00  
U.H. Tp(hrs)= .850
 Unit Hyd Qpeak (cms)= .489  
 PEAK FLOW (cms)= .545 (i)  
 TIME TO PEAK (hrs)= 6.784  
 RUNOFF VOLUME (mm)= 47.687  
 TOTAL RAINFALL (mm)= 98.000  
 RUNOFF COEFFICIENT = .487

Windsor Solar Energy Project

Proposed Conditions SWMHYMO

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

OUTFLOW: ID= 1:002080 148.97 4.737 9.22 55.322 1.958 .217

100:0014---
| ADD HYD ( 2050) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| IN> 04:002050 | ID1 01: 2040 118.02 4.294 8.35 55.58 .000
+ID2 02:201 15.29 .734 7.25 61.16 .000
+ID3 03:204 10.88 .545 6.78 47.69 .000
SUM 04: 2050 144.19 5.065 8.08 55.58 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0019---
| DESIGN NASHYD | Area (ha)= 14.96 Curve Number (CN)=72.00
| 02:207 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.330
Unit Hyd Qpeak (cms)= .430
PEAK FLOW (cms)= .538 (1)
TIME TO PEAK (hrs)= 7.334
RUNOFF VOLUME (mm)= 47.687
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .487

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0015---
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002050 | Number of SEGMENTS = 3
| OUT< 01:002060 | Slopes (%), CHANNEL= .1700 FLOODPLAIN= .2000
LENGTH = 200.00 (m)

<----- DATA FOR SECTION ( 4.0) ----->
Distance Elevation Manning
.00 2.00 .1400
1.80 1.80 .1400 / .0850 Main Channel
102.75 .00 .0850 Main Channel
104.25 .00 .0850 Main Channel
107.00 1.80 .0850 / .1400 Main Channel
207.00 2.00 .1400

100:0020---
| DESIGN NASHYD | Area (ha)= 7.92 Curve Number (CN)=72.00
| 03:208 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.110
Unit Hyd Qpeak (cms)= .273
PEAK FLOW (cms)= .326 (1)
TIME TO PEAK (hrs)= 7.084
RUNOFF VOLUME (mm)= 47.687
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .487

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE

DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.100 .100 .331E+02 .486E+01 .016 .096 34.37 .010
.200 .200 .722E+02 .212E+02 .052 .144 23.13 .029
.300 .300 .118E+03 .518E+02 .106 .180 18.50 .054
.400 .400 .169E+03 .993E+02 .177 .210 15.86 .084
.500 .500 .226E+03 .166E+03\* .268 .236 14.10 .118
.600 .600 .290E+03 .256E+03\* .377 .260 12.81 .156
.700 .700 .360E+03 .370E+03\* .507 .282 11.82 .197
.800 .800 .436E+03 .512E+03\* .659 .303 11.02 .242
.900 .900 .518E+03 .685E+03\* .833 .322 10.36 .290
1.000 1.000 .606E+03 .891E+03\* 1.031 .340 9.79 .340
1.100 1.100 .700E+03 .113E+04\* 1.253 .358 9.31 .394
1.200 1.200 .800E+03 .141E+04\* 1.500 .375 8.89 .450
1.300 1.300 .906E+03 .172E+04\* 1.775 .392 8.51 .509
1.400 1.400 .102E+04 .210E+04\* 2.077 .408 8.18 .571
1.500 1.500 .114E+04 .251E+04\* 2.407 .423 7.87 .635
1.600 1.600 .126E+04 .297E+04\* 2.768 .439 7.60 .702
1.700 1.700 .139E+04 .348E+04\* 3.158 .453 7.35 .771
1.800 1.800 .153E+04 .405E+04\* 3.580 .468 7.12 .842
2.000 2.000 .581E+04 .171E+05\* 6.114 .210 15.84 .421

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 4:002050 144.19 5.065 8.08 55.575 1.917 .273
OUTFLOW: ID= 1:002060 144.19 4.987 8.33 55.575 1.913 .277

100:0021---
| ADD HYD ( 2090) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| IN> 04:002090 | ID1 01: 2080 148.97 4.737 9.22 55.32 .000
+ID2 02:207 14.96 .538 7.33 47.69 .000
+ID3 03:208 7.92 .276 7.08 47.69 .000
SUM 04: 2090 171.85 5.152 9.00 54.31 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0022---
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 04:002090 | Number of SEGMENTS = 3
| OUT< 01:002100 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 130.00 (m)

<----- DATA FOR SECTION ( 6.0) ----->
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
407.00 2.20 .1400

100:0016---
| DESIGN NASHYD | Area (ha)= 4.78 Curve Number (CN)=72.00
| 02:206 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .890
Unit Hyd Qpeak (cms)= .205
PEAK FLOW (cms)= .232 (1)
TIME TO PEAK (hrs)= 6.818
RUNOFF VOLUME (mm)= 47.687
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .487

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .245E+02 .882E+01 .016 .087 24.94 .010
.225 .225 .539E+02 .389E+02\* .054 .129 16.76 .029
.337 .337 .845E+02 .957E+02\* .110 .161 13.43 .054
.450 .450 .128E+03 .185E+03\* .185 .188 11.53 .085
.562 .562 .173E+03 .311E+03\* .280 .211 10.25 .119
.675 .675 .222E+03 .481E+03\* .397 .233 9.32 .157
.788 .788 .272E+03 .698E+03\* .537 .252 8.59 .199
.900 .900 .336E+03 .970E+03\* .700 .270 8.01 .243
1.013 1.013 .401E+03 .130E+04\* .888 .288 7.53 .291
1.125 1.125 .471E+03 .170E+04\* 1.102 .304 7.12 .343
1.238 1.238 .545E+03 .216E+04\* 1.344 .320 6.76 .397
1.350 1.350 .625E+03 .271E+04\* 1.615 .336 6.45 .453
1.463 1.463 .710E+03 .333E+04\* 1.916 .351 6.18 .513
1.575 1.575 .800E+03 .404E+04\* 2.247 .365 5.93 .575
1.688 1.688 .895E+03 .484E+04\* 2.611 .379 5.71 .640
1.800 1.800 .994E+03 .574E+04\* 3.008 .393 5.51 .708
1.933 1.933 .1.093E+04 .671E+04\* 3.431 .407 5.33 .787
2.067 2.067 .1.206E+04 .786E+04\* 3.900 .421 5.16 .874
2.200 2.200 .1.336E+04 .919E+04\* 4.421 .435 5.00 .967

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

100:0017---
| ADD HYD ( 2070) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| IN> 03:002070 | ID1 01: 2060 144.19 4.987 8.33 55.58 .000
+ID2 02:206 4.78 .232 6.82 47.69 .000
SUM 03: 2070 148.97 5.088 8.33 55.32 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0018---
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002070 | Number of SEGMENTS = 3
| OUT< 01:002080 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 500.00 (m)

<----- DATA FOR SECTION ( 5.0) ----->
Distance Elevation Manning
.00 2.20 .1400
200.00 1.80 .1400 / .0850 Main Channel
202.75 .00 .0850 Main Channel
204.25 .00 .0850 Main Channel
207.00 1.80 .0850 / .1400 Main Channel
407.00 2.20 .1400

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x v
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
.112 .112 .940E+02 .882E+01 .016 .087 95.91 .010
.225 .225 .207E+03 .389E+02 .054 .129 64.45 .029
.337 .337 .340E+03 .957E+02 .110 .161 51.67 .054
.450 .450 .492E+03 .185E+03 .185 .188 44.34 .085
.562 .562 .664E+03 .311E+03 .280 .211 39.43 .119
.675 .675 .854E+03 .481E+03 .397 .233 35.84 .157
.788 .788 .1.06E+04 .698E+03\* .537 .252 33.06 .199
.900 .900 .1.29E+04 .970E+03\* .700 .270 30.81 .243
1.013 1.013 .1.54E+04 .1.30E+04\* .888 .288 28.95 .291
1.125 1.125 .1.81E+04 .1.70E+04\* 1.102 .304 27.37 .343
1.238 1.238 .2.10E+04 .2.16E+04\* 1.344 .320 26.01 .397
1.350 1.350 .2.40E+04 .2.71E+04\* 1.615 .336 24.81 .453
1.463 1.463 .2.73E+04 .3.33E+04\* 1.916 .351 23.76 .513
1.575 1.575 .3.08E+04 .4.04E+04\* 2.247 .365 22.82 .575
1.688 1.688 .3.44E+04 .4.84E+04\* 2.611 .379 21.97 .640
1.800 1.800 .3.82E+04 .5.74E+04\* 3.008 .393 21.19 .708
1.933 1.933 .4.23E+04 .6.71E+04\* 3.431 .407 20.52 .787
2.067 2.067 .4.67E+04 .7.86E+04\* 3.900 .421 19.96 .874
2.200 2.200 .5.14E+04 .9.19E+04\* 4.421 .435 19.50 .967

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 3:002070 148.97 5.088 8.33 55.322 1.974 .206

100:0023---
| DESIGN NASHYD | Area (ha)= 4.95 Curve Number (CN)=73.00
| 02:212 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .480
Unit Hyd Qpeak (cms)= .394
PEAK FLOW (cms)= .376 (1)
TIME TO PEAK (hrs)= 6.334
RUNOFF VOLUME (mm)= 48.897
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .499

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0024---
| ADD HYD ( 2110) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| IN> 03:002110 | ID1 01: 2100 171.85 5.103 9.18 54.31 .000
+ID2 02:212 4.95 .376 6.33 48.90 .000
SUM 03: 2110 176.80 5.145 9.18 54.15 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0025---
| ROUTE CHANNEL | Routing time step (min) = 1.00
| IN> 03:002110 | Number of SEGMENTS = 3
| OUT< 01:002120 | Slopes (%), CHANNEL= .1200 FLOODPLAIN= .2000
LENGTH = 330.00 (m)

<----- DATA FOR SECTION ( 7.0) ----->
Distance Elevation Manning

200.00	2.20	1.400	
202.75	1.80	.1400 / .0850	Main Channel
204.25	.00	.0850	Main Channel
207.00	1.80	.0850 / .2000	Main Channel
407.00	2.20	.2000	

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.112	.112	.621E+02	.882E+01	.016	.087	63.30	.010
.225	.225	.137E+03	.389E+02	.054	.129	42.54	.029
.337	.337	.224E+03	.957E+02	.110	.161	34.10	.054
.450	.450	.325E+03	.185E+03*	.185	.188	29.26	.085
.562	.562	.438E+03	.311E+03*	.280	.211	26.02	.119
.675	.675	.564E+03	.481E+03*	.397	.233	23.65	.157
.788	.788	.702E+03	.698E+03*	.537	.252	21.82	.199
.900	.900	.854E+03	.970E+03*	.700	.270	20.34	.243
1.013	1.013	1.013E+04	.130E+04*	.888	.288	19.11	.291
1.125	1.125	.119E+04	.170E+04*	1.102	.304	18.06	.343
1.238	1.238	.138E+04	.216E+04*	1.344	.320	17.16	.397
1.350	1.350	.159E+04	.271E+04*	1.615	.336	16.38	.453
1.463	1.463	.180E+04	.333E+04*	1.916	.351	15.68	.513
1.575	1.575	.203E+04	.404E+04*	2.247	.365	15.06	.575
1.688	1.688	.227E+04	.484E+04*	2.611	.379	14.50	.640
1.800	1.800	.252E+04	.574E+04*	3.008	.393	13.99	.708
1.933	1.933	.277E+04	.671E+04*	4.041	.415	13.28	.788
2.067	2.067	.149E+05	.388E+05*	6.848	.452	12.62	.875
2.200	2.200	.298E+05	.829E+05*	12.488	.488	12.00	.975

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.  
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 3:002110	176.80	5.145	9.18	54.154	1.986	.192
OUTFLOW : ID= 1:002120	176.80	4.956	9.97	54.154	1.975	.199

100:0026					
DESIGN NASHYD	Area (ha)	6.60	Curve Number (CN)	#82.00	
02:EXTB DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)	3.00	
	U.H. Tp (hrs)	.820			

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.071	.071	.542E+02	.108E+02	.006	.037	163.19	.003
.143	.143	.114E+03	.452E+02	.018	.056	106.89	.008
.214	.214	.179E+03	.107E+03*	.035	.071	84.35	.015
.286	.286	.250E+03	.198E+03*	.058	.084	71.69	.024
.357	.357	.326E+03	.323E+03*	.086	.095	63.38	.034
.429	.429	.408E+03	.485E+03*	.118	.105	57.41	.045
.500	.500	.495E+03	.687E+03*	.156	.113	52.87	.057
.571	.571	.588E+03	.933E+03*	.199	.122	49.25	.070
.643	.643	.686E+03	.123E+04*	.247	.130	46.29	.083
.714	.714	.790E+03	.157E+04*	.301	.137	43.80	.098
.786	.786	.898E+03	.196E+04*	.360	.144	41.67	.120
.857	.857	.101E+04	.241E+04*	.424	.151	39.81	.129
.929	.929	.113E+04	.293E+04*	.495	.157	38.18	.146
1.000	1.000	.126E+04	.350E+04*	.572	.163	36.73	.163
1.080	1.080	.140E+04	.417E+04*	.656	.168	35.41	.181
1.160	1.160	.161E+04	.498E+04*	.747	.173	34.21	.198
1.240	1.240	.182E+04	.595E+04*	.845	.177	33.15	.215
1.320	1.320	.203E+04	.708E+04*	.950	.181	32.22	.231
1.400	1.400	.224E+04	.838E+04*	1.062	.185	31.41	.247

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0027					
DESIGN NASHYD	Area (ha)	6.60	Curve Number (CN)	#82.00	
02:EXTB DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)	3.00	
	U.H. Tp (hrs)	.820			
Unit Hyd Qpeak (cms)		.307			
PEAK FLOW (cms)		.443 (1)			
TIME TO PEAK (hrs)		6.718			
RUNOFF VOLUME (mm)		61.161			
TOTAL RAINFALL (mm)		98.000			
RUNOFF COEFFICIENT		.624			

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0028					
DESIGN NASHYD	Area (ha)	12.75	Curve Number (CN)	#72.00	
01:203 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)	3.00	
	U.H. Tp (hrs)	.970			
Unit Hyd Qpeak (cms)		.502			
PEAK FLOW (cms)		.580 (1)			
TIME TO PEAK (hrs)		6.918			
RUNOFF VOLUME (mm)		47.687			
TOTAL RAINFALL (mm)		98.000			
RUNOFF COEFFICIENT		.487			

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0029					
ROUTE CHANNEL	Routing time step (min)	= 1.00			
IN> 01:203	Number of SEGMENTS	= 3			
OUT< 02:002140	Slopes (%), CHANNEL= 3500 FLOODPLAIN= .2000				
	LENGTH = 500.00 (m)				

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 1:203	12.75	.580	6.92	47.687	.602	.331
OUTFLOW : ID= 2:002140	12.75	.522	7.27	47.687	.566	.321

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.071	.071	.753E+02	.154E+01	.015	.097	85.67	.007
.143	.143	.158E+03	.646E+01	.047	.149	56.11	.021
.214	.214	.249E+03	.152E+02	.094	.188	44.28	.040
.286	.286	.347E+03	.283E+02	.154	.221	37.83	.063
.357	.357	.453E+03	.462E+02	.227	.250	33.27	.089
.429	.429	.566E+03	.693E+02	.313	.276	30.14	.118
.500	.500	.687E+03	.982E+02	.413	.300	27.75	.150
.571	.571	.818E+03	.133E+03	.526	.322	25.85	.184
.643	.643	.953E+03	.175E+03	.654	.343	24.30	.220
.714	.714	.110E+04	.224E+03	.795	.362	22.99	.259
.786	.786	.125E+04	.280E+03	.952	.381	21.87	.299
.857	.857	.141E+04	.345E+03	1.123	.399	20.90	.342
.929	.929	.158E+04	.418E+03	1.310	.416	20.04	.386
1.000	1.000	.175E+04	.500E+03	1.513	.432	19.28	.432
1.080	1.080	.195E+04	.600E+03	1.733	.449	18.62	.481
1.160	1.160	.217E+04	.717E+03	2.000	.467	18.04	.534
1.240	1.240	.242E+04	.853E+03	2.327	.485	17.53	.591
1.320	1.320	.269E+04	.100E+04	2.720	.503	17.08	.652
1.400	1.400	.298E+04	.117E+04	3.180	.521	16.69	.717

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 1:203	12.75	.580	6.92	47.687	.602	.331
OUTFLOW : ID= 2:002140	12.75	.522	7.27	47.687	.566	.321

100:0030					
DESIGN NASHYD	Area (ha)	12.89	Curve Number (CN)	#72.00	
01:205 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)	3.00	
	U.H. Tp (hrs)	.860			

Unit Hyd Qpeak (cms)		.572			
PEAK FLOW (cms)		.640 (1)			
TIME TO PEAK (hrs)		6.784			
RUNOFF VOLUME (mm)		47.687			
TOTAL RAINFALL (mm)		98.000			
RUNOFF COEFFICIENT		.487			

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0031							
ADD HYD ( 2150 )	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)	
	ID1 01:205	2140	12.75	522	7.27	47.69	.000
	ID2 02: 2140	12.75	522	7.27	47.69	.000	
SUM 03:	2150	25.64	1.116	7.00	47.69	.000	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0032					
ROUTE CHANNEL	Routing time step (min)	= 1.00			
IN> 03:002150	Number of SEGMENTS	= 3			
OUT< 01:002160	Slopes (%), CHANNEL= .0500 FLOODPLAIN= .2000				
	LENGTH = 360.00 (m)				

Distance	Elevation	Manning
.00	1.40	.1400
200.00	1.00	.1000 / .1000
201.50	.00	.1000
203.50	.00	.1000
205.00	1.00	.1000 / .2000
405.00	1.40	.2000

DEPTH (m)	ELEV (m)	X-VOLUME (cu.m.)	S-VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)	D x V (m2/s)
.071	.071	.542E+02	.108E+02	.006	.037	163.19	.003
.143	.143	.114E+03	.452E+02	.018	.056	106.89	.008
.214	.214	.179E+03	.107E+03*	.035	.071	84.35	.015
.286	.286	.250E+03	.198E+03*	.058	.084	71.69	.024
.357	.357	.326E+03	.323E+03*	.086	.095	63.38	.034
.429	.429	.408E+03	.485E+03*	.118	.105	57.41	.045
.500	.500	.495E+03	.687E+03*	.156	.113	52.87	.057
.571	.571	.588E+03	.933E+03*	.199	.122	49.25	.070
.643	.643	.686E+03	.123E+04*	.247	.130	46.29	.083
.714	.714	.790E+03	.157E+04*	.301	.137	43.80	.098
.786	.786	.898E+03	.196E+04*	.360	.144	41.67	.120
.857	.857	.101E+04	.241E+04*	.424	.151	39.81	.129
.929	.929	.113E+04	.293E+04*	.495	.157	38.18	.146
1.000	1.000	.126E+04	.350E+04*	.572	.163	36.73	.163
1.080	1.080	.140E+04	.417E+04*	.656	.168	35.41	.181
1.160	1.160	.161E+04	.498E+04*	.747	.173	34.21	.198
1.240	1.240	.182E+04	.595E+04*	.845	.177	33.15	.215
1.320	1.320	.203E+04	.708E+04*	.950	.181	32.22	.231
1.400	1.400	.224E+04	.838E+04*	1.062	.185	31.41	.247

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.  
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)	
INFLOW : ID= 3:002150	25.64	1.116	7.00	47.687	1.120	.096
OUTFLOW : ID= 1:002160	25.64	.786	7.87	47.687	1.079	.111

100:0033					
DESIGN NASHYD	Area (ha)	15.50	Curve Number (CN)	#72.00	
02:209 DT= 1.00	Ia (mm)	1.500	# of Linear Res. (N)	3.00	
	U.H. Tp (hrs)	.970			
Unit Hyd Qpeak (cms)		.610			
PEAK FLOW (cms)		.705 (1)			
TIME TO PEAK (hrs)		6.918			
RUNOFF VOLUME (mm)		47.687			
TOTAL RAINFALL (mm)		98.000			
RUNOFF COEFFICIENT		.487			

100:0034						
ADD HYD ( 2170 )	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
	ID1 01: 2160	25.64	.786	7.87	47.69	.000
	ID2 02:209					





AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
INFLOW : ID= 3:002240 284.58 7.257 9.58 53.841 1.695 .140
OUTFLOW: ID= 1:002250 284.58 7.128 9.95 53.841 1.690 .141

.00 1.80 .1400
.1400 / .0850 Main Channel
.0850 Main Channel
.204.40 .00 .0850 Main Channel
.207.00 1.40 .0850 / .2000 Main Channel
.407.00 1.80 .2000

100:0047-----
DESIGN NASHYD | Area (ha)= 24.11 Curve Number (CN)=80.00
| 02:EXT6 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.520
Unit Hyd Qpeak (cms)= .606
PEAK FLOW (cms)= .968 (l)
TIME TO PEAK (hrs)= 7.518 (m)
RUNOFF VOLUME (mm)= 58.211
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .594
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

100:0048-----
DESIGN NASHYD | Area (ha)= 14.49 Curve Number (CN)=82.00
| 03:211 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.070
Unit Hyd Qpeak (cms)= .517
PEAK FLOW (cms)= .801 (l)
TIME TO PEAK (hrs)= 7.001 (m)
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
(\*) Actual value may be less due to limited CHANNEL LENGTH for given SLOPE.

AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
INFLOW : ID= 3:002260 333.75 8.040 9.25 54.279 1.739 .119
OUTFLOW: ID=10:002295 333.75 7.637 10.28 54.279 1.729 .119

100:0049-----
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 03:211 | Number of SEGMENTS = 3
| OUT: 04:002280 | Slopes (%), CHANNEL= .2000 FLOODPLAIN= .2000
LENGTH = 500.00 (m)
DATA FOR SECTION ( 15.0) -----
Distance Elevation Manning
.00 .62 .1400
10.00 .60 .0400 Main Channel
11.80 .00 .0400 Main Channel
12.80 .00 .0400 Main Channel
14.60 .62 .0400 / .2000 Main Channel
24.60 .60 .2000

100:0054-----
DESIGN NASHYD | Area (ha)= 17.47 Curve Number (CN)=76.00
| 03:214 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .600
Unit Hyd Qpeak (cms)= 1.112
PEAK FLOW (cms)= 1.239 (l)
TIME TO PEAK (hrs)= 6.484 (m)
RUNOFF VOLUME (mm)= 52.697
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .538
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TRAVEL TIME TABLE
DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV TIME D x V
(m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

100:0055-----
# Calculate culvert routing and flow split near eastern site boundary
# Storage volumes calculated based on site survey
# Discharge calculated based on the 600 mm diameter CSP and 1500 mm diameter CSP capacities
ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03:(214) |
| OUT<01:(002300) |
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | 1.130 .4600E+00
.150 .0000E+00 | 5.470 .8100E+00
.450 .0000E+00 | 83.090 .3400E+01
.820 .6500E-01 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW>03:(214) 17.47 1.239 6.484 52.697
OUTFLOW<01:(002300) 17.47 .866 7.068 52.728
PEAK FLOW REDUCTION [Qout/Qin] (%) = 69.883
TIME SPLIT OF PEAK FLOW (min) = 35.00
MAXIMUM STORAGE USED (ha.m.) = 1235E+00

X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
INFLOW : ID= 3:211 14.49 8.01 7.00 61.161 .562 .536
OUTFLOW: ID= 4:002280 14.49 .768 7.23 61.161 .549 .529

100:0050-----
DESIGN NASHYD | Area (ha)= 10.57 Curve Number (CN)=72.00
| 03:216 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= 1.210
Unit Hyd Qpeak (cms)= .334
PEAK FLOW (cms)= 4.08 (l)
TIME TO PEAK (hrs)= 7.184 (m)
RUNOFF VOLUME (mm)= 47.687
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .487
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0056-----
DIVERT HYD |
| INID=01 (002300) |
Outflow / Inflow Relationships
Flow 02 + Flow 03 = Total
(cms) (cms) (cms)
.000 .000 .000
.150 .000 .150
.400 .050 .450
.680 .140 .820
.930 .200 1.130
1.040 4.430 5.470
1.460 81.630 83.090

100:0051-----
ADD HYD ( 2290) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| 03:216 DT= 1.00 | ID1 03:216 14.49 8.01 7.00 61.161 .000
+ID2 04: 2280 14.49 .768 7.23 61.16 .000
SUM 05: 2290 25.06 1.176 7.22 55.48 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0057-----
DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=72.00
| 01:215 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00
U.H. Tp(hrs)= .860
Unit Hyd Qpeak (cms)= .237
PEAK FLOW (cms)= .265 (l)
TIME TO PEAK (hrs)= 6.784 (m)
RUNOFF VOLUME (mm)= 47.687
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .487
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0052-----
ADD HYD ( 2260) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| 01: 2250 284.58 7.128 9.95 53.84 .000
+ID2 02:EXT6 24.11 .968 7.52 58.20 .000
+ID3 05: 2290 25.06 1.176 7.22 55.48 .000
SUM 03: 2260 333.75 8.040 9.25 54.28 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0058-----
ADD HYD ( 2330) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| 01:215 DT= 1.00 | ID1 01:215 5.34 .265 6.78 47.69 .000
+ID2 02: 2310 15.22 .717 7.07 52.73 .000
SUM 04: 2330 20.56 .977 6.88 51.42 .000
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100:0053-----
ROUTE CHANNEL | Routing time step (min) = 1.00
| IN: 03:002260 | Number of SEGMENTS = 3
| OUT< 10:002295 | Slopes (%), CHANNEL= .0800 FLOODPLAIN= .2000
LENGTH = 370.00 (m)
DATA FOR SECTION ( 14.0) -----
Distance Elevation Manning

100:0059-----
DESIGN NASHYD | Area (ha)= 18.59 Curve Number (CN)=82.00
| 01:EXT7 DT= 1.00 | Ia (mm)= 1.500 # of Linear Res. (N)= 3.00

```

----- U.H. Tp(hrs)= 1.470
Unit Hyd Qpeak (cms)= .483
PEAK FLOW (cms)= .807 (i)
TIME TO PEAK (hrs)= 7.451
RUNOFF VOLUME (mm)= 61.161
TOTAL RAINFALL (mm)= 98.000
RUNOFF COEFFICIENT = .624

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
100:0060-----
*#*****
*# McGill Drain - Total Flow at Eastern WSP
*#*****
-----
| ADD HYD ( 2340) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
----- (ha) (cms) (hrs) (mm) (cms)
ID1 01:EXT7 18.59 .807 7.45 61.16 .000
+ID2 04: 2330 20.56 .977 6.88 51.42 .000
+ID3 10: 2295 332.75 7.637 10.28 54.28 .000
-----
SUM 05: 2340 372.90 8.272 9.87 54.46 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
-----
100:0061-----
*#*****
*# AREA CHECK
*#*****
-----
| ADD HYD ( 2350) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
----- (ha) (cms) (hrs) (mm) (cms)
ID1 03: 2320 2.25 .149 7.07 52.73 .000
+ID2 05: 2340 372.90 8.272 9.87 54.46 .000
-----
SUM 01: 2350 375.15 8.294 9.87 54.45 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
-----
100:0062-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
100:0002-----
FINISH
-----
*****
WARNINGS / ERRORS / NOTES
-----
Simulation ended on 2016-02-15 at 14:15:22
-----

```

# Hydrologic Response of Solar Farms

Lauren M. Cook, S.M.ASCE<sup>1</sup>; and Richard H. McCuen, M.ASCE<sup>2</sup>

**Abstract:** Because of the benefits of solar energy, the number of solar farms is increasing; however, their hydrologic impacts have not been studied. The goal of this study was to determine the hydrologic effects of solar farms and examine whether or not storm-water management is needed to control runoff volumes and rates. A model of a solar farm was used to simulate runoff for two conditions: the pre- and postpaneled conditions. Using sensitivity analyses, modeling showed that the solar panels themselves did not have a significant effect on the runoff volumes, peaks, or times to peak. However, if the ground cover under the panels is gravel or bare ground, owing to design decisions or lack of maintenance, the peak discharge may increase significantly with storm-water management needed. In addition, the kinetic energy of the flow that drains from the panels was found to be greater than that of the rainfall, which could cause erosion at the base of the panels. Thus, it is recommended that the grass beneath the panels be well maintained or that a buffer strip be placed after the most downgradient row of panels. This study, along with design recommendations, can be used as a guide for the future design of solar farms. DOI: 10.1061/(ASCE)HE.1943-5584.0000530. © 2013 American Society of Civil Engineers.

**CE Database subject headings:** Hydrology; Land use; Solar power; Floods; Surface water; Runoff; Stormwater management.

**Author keywords:** Hydrology; Land use change; Solar energy; Flooding; Surface water runoff; Storm-water management.

## Introduction

Storm-water management practices are generally implemented to reverse the effects of land-cover changes that cause increases in volumes and rates of runoff. This is a concern posed for new types of land-cover change such as the solar farm. Solar energy is a renewable energy source that is expected to increase in importance in the near future. Because solar farms require considerable land, it is necessary to understand the design of solar farms and their potential effect on erosion rates and storm runoff, especially the impact on offsite properties and receiving streams. These farms can vary in size from 8 ha (20 acres) in residential areas to 250 ha (600 acres) in areas where land is abundant.

The solar panels are impervious to rain water; however, they are mounted on metal rods and placed over pervious land. In some cases, the area below the panel is paved or covered with gravel. Service roads are generally located between rows of panels. Although some panels are stationary, others are designed to move so that the angle of the panel varies with the angle of the sun. The angle can range, depending on the latitude, from 22° during the summer months to 74° during the winter months. In addition, the angle and direction can also change throughout the day. The issue posed is whether or not these rows of impervious panels will change the runoff characteristics of the site, specifically increase runoff volumes or peak discharge rates. If the increases are hydrologically significant, storm-water management facilities may be needed. Additionally, it is possible that the velocity of water

draining from the edge of the panels is sufficient to cause erosion of the soil below the panels, especially where the maintenance roadways are bare ground.

The outcome of this study provides guidance for assessing the hydrologic effects of solar farms, which is important to those who plan, design, and install arrays of solar panels. Those who design solar farms may need to provide for storm-water management. This study investigated the hydrologic effects of solar farms, assessed whether or not storm-water management might be needed, and if the velocity of the runoff from the panels could be sufficient to cause erosion of the soil below the panels.

## Model Development

Solar farms are generally designed to maximize the amount of energy produced per unit of land area, while still allowing space for maintenance. The hydrologic response of solar farms is not usually considered in design. Typically, the panels will be arrayed in long rows with separations between the rows to allow for maintenance vehicles. To model a typical layout, a unit width of one panel was assumed, with the length of the downgradient strip depending on the size of the farm. For example, a solar farm with 30 rows of 200 panels each could be modeled as a strip of 30 panels with space between the panels for maintenance vehicles. Rainwater that drains from the upper panel onto the ground will flow over the land under the 29 panels on the downgradient strip. Depending on the land cover, infiltration losses would be expected as the runoff flows to the bottom of the slope.

To determine the effects that the solar panels have on runoff characteristics, a model of a solar farm was developed. Runoff in the form of sheet flow without the addition of the solar panels served as the prepaneled condition. The paneled condition assumed a downgradient series of cells with one solar panel per ground cell. Each cell was separated into three sections: wet, dry, and spacer.

The dry section is that portion directly underneath the solar panel, unexposed directly to the rainfall. As the angle of the panel from the horizontal increases, more of the rain will fall directly onto

<sup>1</sup>Research Assistant, Dept. of Civil and Environmental Engineering, Univ. of Maryland, College Park, MD 20742-3021.

<sup>2</sup>The Ben Dyer Professor, Dept. of Civil and Environmental Engineering, Univ. of Maryland, College Park, MD 20742-3021 (corresponding author). E-mail: rhmccuen@eng.umd.edu

Note. This manuscript was submitted on August 12, 2010; approved on October 20, 2011; published online on October 24, 2011. Discussion period open until October 1, 2013; separate discussions must be submitted for individual papers. This paper is part of the *Journal of Hydrologic Engineering*, Vol. 18, No. 5, May 1, 2013. © ASCE, ISSN 1084-0699/2013/5-536-541/\$25.00.

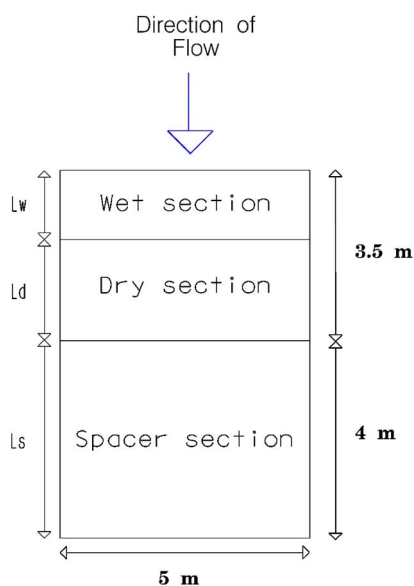


the ground; this section of the cell is referred to as the wet section. The spacer section is the area between the rows of panels used by maintenance vehicles. Fig. 1 is an image of two solar panels and the spacer section allotted for maintenance vehicles. Fig. 2 is a schematic of the wet, dry, and spacer sections with their respective dimensions. In Fig. 1, tracks from the vehicles are visible on what is modeled within as the spacer section. When the solar panel is horizontal, then the length longitudinal to the direction that runoff will occur is the length of the dry and wet sections combined. Runoff from a dry section drains onto the downgradient spacer section. Runoff from the spacer section flows to the wet section of the next downgradient cell. Water that drains from a solar panel falls directly onto the spacer section of that cell.

The length of the spacer section is constant. During a storm event, the loss rate was assumed constant for the 24-h storm because a wet antecedent condition was assumed. The lengths of the wet and dry sections changed depending on the angle of the solar panel. The total length of the wet and dry sections was set



**Fig. 1.** Maintenance or “spacer” section between two rows of solar panels (photo by John E. Showler, reprinted with permission)



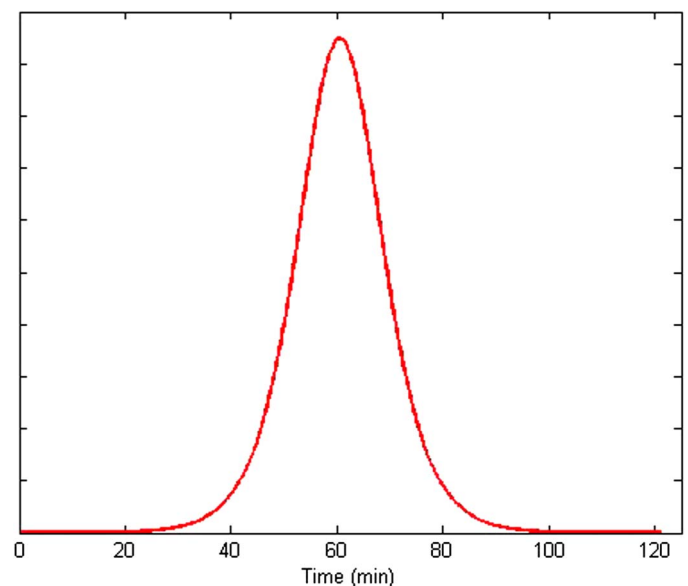
**Fig. 2.** Wet, dry, and spacer sections of a single cell with lengths  $L_w$ ,  $L_s$ , and  $L_d$  with the solar panel covering the dry section

equal to the length of one horizontal solar panel, which was assumed to be 3.5 m. When a solar panel is horizontal, the dry section length would equal 3.5 m and the wet section length would be zero. In the paneled condition, the dry section does not receive direct rainfall because the rain first falls onto the solar panel then drains onto the spacer section. However, the dry section does infiltrate some of the runoff that comes from the upgradient wet section. The wet section was modeled similar to the spacer section with rain falling directly onto the section and assuming a constant loss rate.

For the presolar panel condition, the spacer and wet sections are modeled the same as in the paneled condition; however, the cell does not include a dry section. In the prepaneled condition, rain falls directly onto the entire cell. When modeling the prepaneled condition, all cells receive rainfall at the same rate and are subject to losses. All other conditions were assumed to remain the same such that the prepaneled and paneled conditions can be compared.

Rainfall was modeled after a natural resources conservation service (NRCS) Type II Storm (McCuen 2005) because it is an accurate representation of actual storms of varying characteristics that are imbedded in intensity-duration-frequency (IDF) curves. For each duration of interest, a dimensionless hyetograph was developed using a time increment of 12 s over the duration of the storm (see Fig. 3). The depth of rainfall that corresponds to each storm magnitude was then multiplied by the dimensionless hyetograph. For a 2-h storm duration, depths of 40.6, 76.2, and 101.6 mm were used for the 2-, 25-, and 100-year events. The 2- and 6-h duration hyetographs were developed using the center portion of the 24-h storm, with the rainfall depths established with the Baltimore IDF curve. The corresponding depths for a 6-h duration were 53.3, 106.7, and 132.1 mm, respectively. These magnitudes were chosen to give a range of storm conditions.

During each time increment, the depth of rain is multiplied by the cell area to determine the volume of rain added to each section of each cell. This volume becomes the storage in each cell. Depending on the soil group, a constant volume of losses was subtracted from the storage. The runoff velocity from a solar panel was calculated using Manning’s equation, with the hydraulic radius for sheet flow assumed to equal the depth of the storage on the panel (Bedient and Huber 2002). Similar assumptions were made to compute the velocities in each section of the surface sections.



**Fig. 3.** Dimensionless hyetograph of 2-h Type II storm

Runoff from one section to the next and then to the next downgradient cell was routed using the continuity of mass. The routing coefficient depended on the depth of flow in storage and the velocity of runoff. Flow was routed from the wet section to the dry section to the spacer section, with flow from the spacer section draining to the wet section of the next cell. Flow from the most downgradient cell was assumed to be the outflow. Discharge rates and volumes from the most downgradient cell were used for comparisons between the prepaneled and paneled conditions.

### Alternative Model Scenarios

To assess the effects of the different variables, a section of 30 cells, each with a solar panel, was assumed for the base model. Each cell was separated individually into wet, dry, and spacer sections. The area had a total ground length of 225 m with a ground slope of 1% and width of 5 m, which was the width of an average solar panel. The roughness coefficient (Engman 1986) for the silicon solar panel was assumed to be that of glass, 0.01. Roughness coefficients of 0.15 for grass and 0.02 for bare ground were also assumed. Loss rates of 0.5715 cm/h (0.225 in./h) and 0.254 cm/h (0.1 in./h) for B and C soils, respectively, were assumed.

The prepaneled condition using the 2-h, 25-year rainfall was assumed for the base condition, with each cell assumed to have a good grass cover condition. All other analyses were made assuming a paneled condition. For most scenarios, the runoff volumes and peak discharge rates from the paneled model were not significantly greater than those for the prepaneled condition. Over a total length of 225 m with 30 solar panels, the runoff increased by 0.26 m<sup>3</sup>, which was a difference of only 0.35%. The slight increase in runoff volume reflects the slightly higher velocities for the paneled condition. The peak discharge increased by 0.0013 m<sup>3</sup>, a change of only 0.31%. The time to peak was delayed by one time increment, i.e., 12 s. Inclusion of the panels did not have a significant hydrologic impact.

### Storm Magnitude

The effect of storm magnitude was investigated by changing the magnitude from a 25-year storm to a 2-year storm. For the 2-year storm, the rainfall and runoff volumes decreased by approximately 50%. However, the runoff from the paneled watershed condition increased compared to the prepaneled condition by approximately the same volume as for the 25-year analysis, 0.26 m<sup>3</sup>. This increase represents only a 0.78% increase in volume. The peak discharge and the time to peak did not change significantly. These results reflect runoff from a good grass cover condition and indicated that the general conclusion of very minimal impacts was the same for different storm magnitudes.

### Ground Slope

The effect of the downgradient ground slope of the solar farm was also examined. The angle of the solar panels would influence the velocity of flows from the panels. As the ground slope was increased, the velocity of flow over the ground surface would be closer to that on the panels. This could cause an overall increase in discharge rates. The ground slope was changed from 1 to 5%, with all other conditions remaining the same as the base conditions.

With the steeper incline, the volume of losses decreased from that for the 1% slope, which is to be expected because the faster velocity of the runoff would provide less opportunity for infiltration. However, between the prepaneled and paneled conditions, the increase in runoff volume was less than 1%. The peak discharge

and the time to peak did not change. Therefore, the greater ground slope did not significantly influence the response of the solar farm.

### Soil Type

The effect of soil type on the runoff was also examined. The soil group was changed from B soil to C soil by varying the loss rate. As expected, owing to the higher loss rate for the C soil, the depths of runoff increased by approximately 7.5% with the C soil when compared with the volume for B soils. However, the runoff volume for the C soil condition only increased by 0.17% from the prepaneled condition to the paneled condition. In comparison with the B soil, a difference of 0.35% in volume resulted between the two conditions. Therefore, the soil group influenced the actual volumes and rates, but not the relative effect of the paneled condition when compared to the prepaneled condition.

### Panel Angle

Because runoff velocities increase with slope, the effect of the angle of the solar panel on the hydrologic response was examined. Analyses were made for angles of 30° and 70° to test an average range from winter to summer. The hydrologic response for these angles was compared to that of the base condition angle of 45°. The other site conditions remained the same. The analyses showed that the angle of the panel had only a slight effect on runoff volumes and discharge rates. The lower angle of 30° was associated with an increased runoff volume, whereas the runoff volume decreased for the steeper angle of 70° when compared with the base condition of 45°. However, the differences (~0.5%) were very slight. Nevertheless, these results indicate that, when the solar panel was closer to horizontal, i.e., at a lower angle, a larger difference in runoff volume occurred between the prepaneled and paneled conditions. These differences in the response result are from differences in loss rates.

The peak discharge was also lower at the lower angle. At an angle of 30°, the peak discharge was slightly lower than at the higher angle of 70°. For the 2-h storm duration, the time to peak of the 30° angle was 2 min delayed from the time to peak of when the panel was positioned at a 70° angle, which reflects the longer travel times across the solar panels.

### Storm Duration

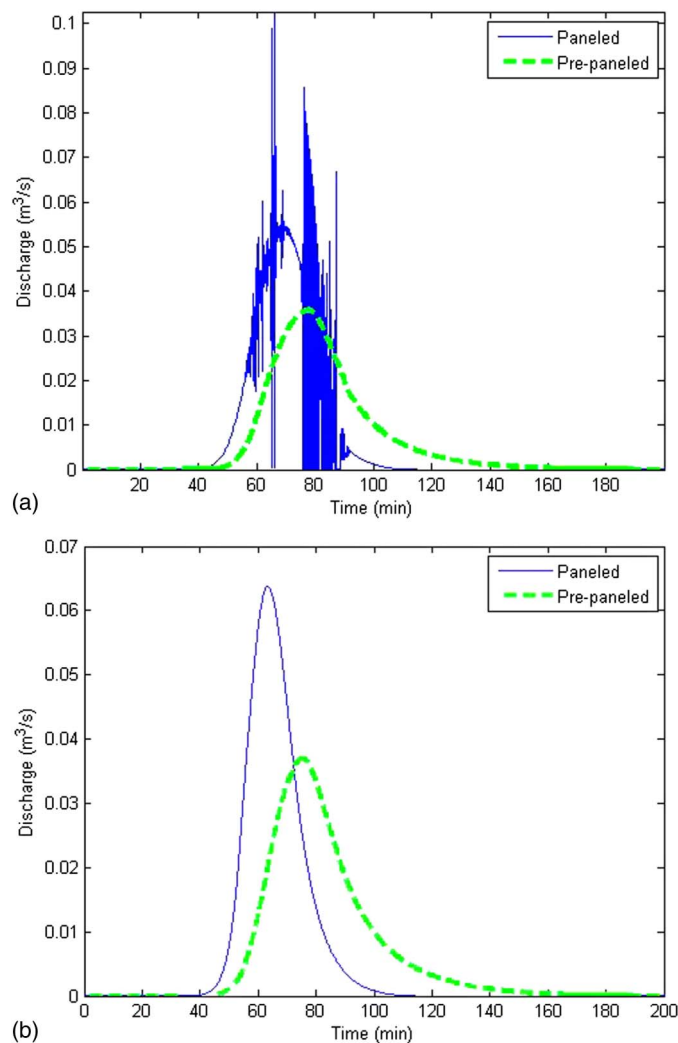
To assess the effect of storm duration, analyses were made for 6-h storms, testing magnitudes for 2-, 25-, and 100-year return periods, with the results compared with those for the 2-h rainfall events. The longer storm duration was tested to determine whether a longer duration storm would produce a different ratio of increase in runoff between the prepaneled and paneled conditions. When compared to runoff volumes from the 2-h storm, those for the 6-h storm were 34% greater in both the paneled and prepaneled cases. However, when comparing the prepaneled to the paneled condition, the increase in the runoff volume with the 6-h storm was less than 1% regardless of the return period. The peak discharge and the time-to-peak did not differ significantly between the two conditions. The trends in the hydrologic response of the solar farm did not vary with storm duration.

### Ground Cover

The ground cover under the panels was assumed to be a native grass that received little maintenance. For some solar farms, the area beneath the panel is covered in gravel or partially paved because the panels prevent the grass from receiving sunlight. Depending on the

volume of traffic, the spacer cell could be grass, patches of grass, or bare ground. Thus, it was necessary to determine whether or not these alternative ground-cover conditions would affect the runoff characteristics. This was accomplished by changing the Manning's  $n$  for the ground beneath the panels. The value of  $n$  under the panels, i.e., the dry section, was set to 0.015 for gravel, with the value for the spacer or maintenance section set to 0.02, i.e., bare ground. These can be compared to the base condition of a native grass ( $n = 0.15$ ). A good cover should promote losses and delay the runoff.

For the smoother surfaces, the velocity of the runoff increased and the losses decreased, which resulted in increasing runoff volumes. This occurred both when the ground cover under the panels was changed to gravel and when the cover in the spacer section was changed to bare ground. Owing to the higher velocities of the flow, runoff rates from the cells increased significantly such that it was necessary to reduce the computational time increment. Fig. 4(a) shows the hydrograph from a 30-panel area with a time increment of 12 s. With a time increment of 12 s, the water in each cell is discharged at the end of every time increment, which results in no attenuation of the flow; thus, the undulations shown in Fig. 4(a) result. The time increment was reduced to 3 s for the 2-h storm, which resulted in watershed smoothing and a rational hydrograph shape [Fig. 4(b)]. The results showed that the storm runoff



**Fig. 4.** Hydrograph with time increment of (a) 12 s; (b) 3 s with Manning's  $n$  for bare ground

increased by 7% from the grass-covered scenario to the scenario with gravel under the panel. The peak discharge increased by 73% for the gravel ground cover when compared with the grass cover without the panels. The time to peak was 10 min less with the gravel than with the grass, which reflects the effect of differences in surface roughness and the resulting velocities.

If maintenance vehicles used the spacer section regularly and the grass cover was not adequately maintained, the soil in the spacer section would be compacted and potentially the runoff volumes and rates would increase. Grass that is not maintained has the potential to become patchy and turn to bare ground. The grass under the panel may not get enough sunlight and die. Fig. 1 shows the result of the maintenance trucks frequently driving in the spacer section, which diminished the grass cover.

The effect of the lack of solar farm maintenance on runoff characteristics was modeled by changing the Manning's  $n$  to a value of 0.02 for bare ground. In this scenario, the roughness coefficient for the ground under the panels, i.e., the dry section, as well as in the spacer cell was changed from grass covered to bare ground ( $n = 0.02$ ). The effects were nearly identical to that of the gravel. The runoff volume increased by 7% from the grass-covered to the bare-ground condition. The peak discharge increased by 72% when compared with the grass-covered condition. The runoff for the bare-ground condition also resulted in an earlier time to peak by approximately 10 min. Two other conditions were also modeled, showing similar results. In the first scenario, gravel was placed directly under the panel, and healthy grass was placed in the spacer section, which mimics a possible design decision. Under these conditions, the peak discharge increased by 42%, and the volume of runoff increased by 4%, which suggests that storm-water management would be necessary if gravel is placed anywhere.

Fig. 5 shows two solar panels from a solar farm in New Jersey. The bare ground between the panels can cause increased runoff rates and reductions in time of concentration, both of which could necessitate storm-water management. The final condition modeled involved the assumption of healthy grass beneath the panels and bare ground in the spacer section, which would simulate the condition of unmaintained grass resulting from vehicles that drive over the spacer section. Because the spacer section is 53% of the cell, the change in land cover to bare ground would reduce losses and decrease runoff travel times, which would cause runoff to amass as it



**Fig. 5.** Site showing the initiation of bare ground below the panels, which increases the potential for erosion (photo by John Showler, reprinted with permission)



moves downgradient. With the spacer section as bare ground, the peak discharge increased by 100%, which reflected the increases in volume and decrease in timing. These results illustrate the need for maintenance of the grass below and between the panels.

## Design Suggestions

With well-maintained grass underneath the panels, the solar panels themselves do not have much effect on total volumes of the runoff or peak discharge rates. Although the panels are impervious, the rainwater that drains from the panels appears as runoff over the downgradient cells. Some of the runoff infiltrates. If the grass cover of a solar farm is not maintained, it can deteriorate either because of a lack of sunlight or maintenance vehicle traffic. In this case, the runoff characteristics can change significantly with both runoff rates and volumes increasing by significant amounts. In addition, if gravel or pavement is placed underneath the panels, this can also contribute to a significant increase in the hydrologic response.

If bare ground is foreseen to be a problem or gravel is to be placed under the panels to prevent erosion, it is necessary to counteract the excess runoff using some form of storm-water management. A simple practice that can be implemented is a buffer strip (Dabney et al. 2006) at the downgradient end of the solar farm. The buffer strip length must be sufficient to return the runoff characteristics with the panels to those of runoff experienced before the gravel and panels were installed. Alternatively, a detention basin can be installed.

A buffer strip was modeled along with the panels. For approximately every 200 m of panels, or 29 cells, the buffer must be 5 cells long (or 35 m) to reduce the runoff volume to that which occurred before the panels were added. Even if a gravel base is not placed under the panels, the inclusion of a buffer strip may be a good practice when grass maintenance is not a top funding priority. Fig. 6 shows the peak discharge from the graveled surface versus the length of the buffer needed to keep the discharge to prepaneled peak rate.

Water draining from a solar panel can increase the potential for erosion of the spacer section. If the spacer section is bare ground, the high kinetic energy of water draining from the panel can cause soil detachment and transport (Garde and Raju 1977; Beuselinck et al. 2002). The amount and risk of erosion was modeled using the velocity of water coming off a solar panel compared with the velocity and intensity of the rainwater. The velocity of panel

runoff was calculated using Manning's equation, and the velocity of falling rainwater was calculated using the following:

$$V_t = 120 d_r^{0.35} \quad (1)$$

where  $d_r$  = diameter of a raindrop, assumed to be 1 mm. The relationship between kinetic energy and rainfall intensity is

$$K_e = 916 + 330 \log_{10} i \quad (2)$$

where  $i$  = rainfall intensity (in./h) and  $K_e$  = kinetic energy (ft-tons per ac-in. of rain) of rain falling onto the wet section and the panel, as well as the water flowing off of the end of the panel (Wischmeier and Smith 1978). The kinetic energy (Salles et al. 2002) of the rainfall was greater than that coming off the panel, but the area under the panel (i.e., the product of the length, width, and cosine of the panel angle) is greater than the area under the edge of the panel where the water drains from the panel onto the ground. Thus, dividing the kinetic energy by the respective areas gives a more accurate representation of the kinetic energy experienced by the soil. The energy of the water draining from the panel onto the ground can be nearly 10 times greater than the rain itself falling onto the ground area. If the solar panel runoff falls onto an unsealed soil, considerable detachment can result (Motha et al. 2004). Thus, because of the increased kinetic energy, it is possible that the soil is much more prone to erosion with the panels than without. Where panels are installed, methods of erosion control should be included in the design.

## Conclusions

Solar farms are the energy generators of the future; thus, it is important to determine the environmental and hydrologic effects of these farms, both existing and proposed. A model was created to simulate storm-water runoff over a land surface without panels and then with solar panels added. Various sensitivity analyses were conducted including changing the storm duration and volume, soil type, ground slope, panel angle, and ground cover to determine the effect that each of these factors would have on the volumes and peak discharge rates of the runoff.

The addition of solar panels over a grassy field does not have much of an effect on the volume of runoff, the peak discharge, nor the time to peak. With each analysis, the runoff volume increased slightly but not enough to require storm-water management facilities. However, when the land-cover type was changed under the panels, the hydrologic response changed significantly. When gravel or pavement was placed under the panels, with the spacer section left as patchy grass or bare ground, the volume of the runoff increased significantly and the peak discharge increased by approximately 100%. This was also the result when the entire cell was assumed to be bare ground.

The potential for erosion of the soil at the base of the solar panels was also studied. It was determined that the kinetic energy of the water draining from the solar panel could be as much as 10 times greater than that of rainfall. Thus, because the energy of the water draining from the panels is much higher, it is very possible that soil below the base of the solar panel could erode owing to the concentrated flow of water off the panel, especially if there is bare ground in the spacer section of the cell. If necessary, erosion control methods should be used.

Bare ground beneath the panels and in the spacer section is a realistic possibility (see Figs. 1 and 5). Thus, a good, well-maintained grass cover beneath the panels and in the spacer section is highly recommended. If gravel, pavement, or bare ground is

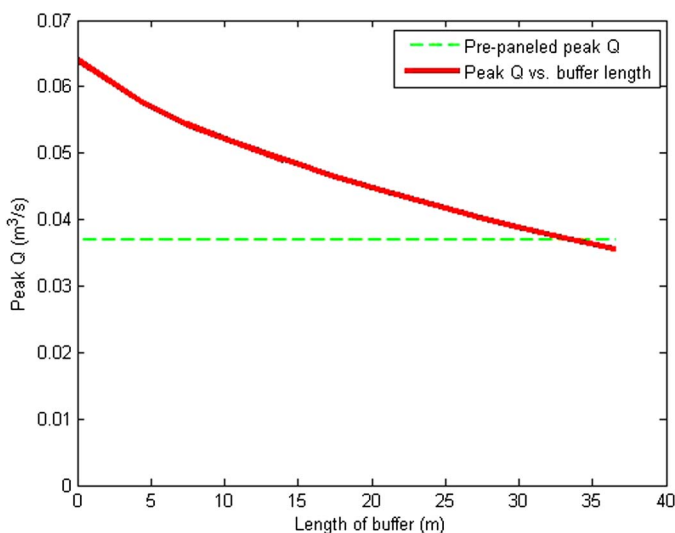


Fig. 6. Peak discharge over gravel compared with buffer length



deemed unavoidable below the panels or in the spacer section, it may necessary to add a buffer section to control the excess runoff volume and ensure adequate losses. If these simple measures are taken, solar farms will not have an adverse hydrologic impact from excess runoff or contribute eroded soil particles to receiving streams and waterways.

## Acknowledgments

The authors appreciate the photographs (Figs. 1 and 5) of Ortho Clinical Diagnostics, 1001 Route 202, North Raritan, New Jersey, 08869, provided by John E. Showler, Environmental Scientist, New Jersey Department of Agriculture. The extensive comments of reviewers resulted in an improved paper.

## References

- Bedient, P. B., and Huber, W. C. (2002). *Hydrology and floodplain analysis*, Prentice-Hall, Upper Saddle River, NJ.
- Beuselinck, L., Govers, G., Hairsince, P. B., Sander, G. C., and Breynaert, M. (2002). "The influence of rainfall on sediment transport by overland flow over areas of net deposition." *J. Hydrol.*, 257(1–4), 145–163.
- Dabney, S. M., Moore, M. T., and Locke, M. A. (2006). "Integrated management of in-field, edge-of-field, and after-field buffers." *J. Amer. Water Resour. Assoc.*, 42(1), 15–24.
- Engman, E. T. (1986). "Roughness coefficients for routing surface runoff." *J. Irrig. Drain. Eng.*, 112(1), 39–53.
- Garde, R. J., and Raju, K. G. (1977). *Mechanics of sediment transportation and alluvial stream problems*, Wiley, New York.
- McCuen, R. H. (2005). *Hydrologic analysis and design*, 3rd Ed., Pearson/Prentice-Hall, Upper Saddle River, NJ.
- Motha, J. A., Wallbrink, P. J., Hairsine, P. B., and Grayson, R. B. (2004). "Unsealed roads as suspended sediment sources in agricultural catchment in south-eastern Australia." *J. Hydrol.*, 286(1–4), 1–18.
- Salles, C., Poesen, J., and Sempere-Torres, D. (2002). "Kinetic energy of rain and its functional relationship with intensity." *J. Hydrol.*, 257(1–4), 256–270.
- Wischmeier, W. H., and Smith, D. D. (1978). *Predicting rainfall erosion losses: A guide to conservation planning*, USDA Handbook 537, U.S. Government Printing Office, Washington, DC.

Copyright of Journal of Hydrologic Engineering is the property of American Society of Civil Engineers and its content may not be copied or emailed to multiple sites or posted to a listserv without the copyright holder's express written permission. However, users may print, download, or email articles for individual use.

# **APPENDIX E**

## **RUNOFF QUALITY**

## CONTROL OF SOIL EROSION

(Revision of Factsheet "Control of Soil Erosion", January 1979)

N. Moore, Soil & Water Management Branch, Lindsay

P. Fish, Upper Thames River Conservation Authority, London

J. Arnold, Soil & Water Management Branch, Guelph

While protecting and improving land investment, controlling soil erosion will sustain or improve crop yields; reduce drainage costs; retain nutrients and chemicals where applied; reduce hazards when working on eroding soil, and help improve water quality.

Management of soil for water and wind erosion control is based on sensible soil conservation practices. The majority of these practices are not new. They are recognized components of good soil, crop, and water management. For effective erosion control, the following factors are involved:

- maintaining good soil structure
- protecting the soil surface by adequate crop and residue cover; and
- using special structural erosion control practices where necessary.

These factors are often interrelated in controlling both water and wind erosion. Not all erosion control practices will fit into every farm management scheme. However, each erosion problem can be remedied by choosing one or more of the remedial practices available. The choice of any such practice should be appropriate to the problem and also be a practical and economical solution.

### Soil Structure

Good soil structure is a consequence of management systems that include the regular use of soil improving crops such as forages; the frequent return of organic matter in residues and manure; and include tillage practices which avoid unnecessary breakdown of soil structure.

A forage crop, such as grass-legume hay, in a rotation improves soil structure as reflected by an increased degree of aggregate stability (Table 1). Corn stover residue, when not removed, also improves soil structure and reduces soil

**Table 1. Effect of forage crops in rotation on aggregate stability — Haldimand Clay.**

Cropping System	Water-stable aggregation %	Corn yield %
Corn, oats, hay, hay rotation	74*	100
Continuous corn	22	90

\* Measured in the second hay crop of the rotation.

**Table 2. Effect of corn stover residue on aggregate stability and erosion control with a continuous corn cropping system — Guelph loam with 8% slope**

Residue management	Water-stable aggregation %	Soil loss in runoff t/ha*
Stover removed —		
— plowed in fall	18	54
Stover not removed —		
— plowed in fall	32	35
— not plowed	—	4

\* Metric tonnes per hectare (15 t/ha = 1 mm depth of soil)

erosion (Table 2). However, soil losses from plowed soil — even where the stover is not removed — can exceed the limit (7 tonnes per hectare), considered tolerable for most field situations. By leaving corn stover residue at the soil surface as with no till or mulch tillage, soil losses may be reduced below tolerable limits. (Figure 1).



**Figure 1. Crop residue cover reduces erosion**

Tillage practices also affect soil structure. Proper tillage reduces soil aggregates to the most effective size for a favorable seedbed. Excess tillage, however, can break down soil aggregates to primary particles, destroying the soil structure formed previously by good crop and residue management, contribute to undesirable compaction, accelerate erosion, and waste time and energy. Timeliness of tillage operations is also important. For example, working



finely-textured soils when wet should be avoided in order to prevent compaction, puddling, and the resulting formation of hard clods when dry. Timely tillage will help maintain soil structure and reduce its erosion potential. See OMAF Factsheets. *Tillage for Crop Production on Ontario Soils — Practices*, Agdex 100/5/6, *Tillage for Crop Production on Ontario Soils — Principles*, Agdex 110/632, and *Tillage Practices for Residue Management and Erosion control*, Agdex 100/ 516.

#### Crop & Residue Cover

The benefits of growing the appropriate crops on specific soils must be recognized. Crops help reduce the erosive forces of water and wind by means of their canopy intercepting rain, and acting as a windbreak. Root systems stabilize the soil and reduce losses. Crop residues perform similar functions and, in addition, form small dams that help retain runoff water, thereby reducing erosion.

#### Crop Rotations

Fallow land has the highest erosion potential in any cropping system. Row crops such as corn or beans reduce this potential by half, which is still considered to be excessive. Sod crops such as hay and permanent pasture keep soil erosion to a minimum and should, therefore, be used in rotation with other crops where erosion is a problem. Compared to continuous corn, hay or pasture crops reduce soil loss by about 90% (Table 3). A rotation involving row crops and grain crops, while not as effective as a sod-based rotation, may reduce soil losses by 30% compared to continuous row crops.

**Table 3. Reduction in soil loss compared to continuous corn or beans\***

	%
Mixed grain or winter wheat	40
Rotation of 1 year corn, 1 year grain	
2 years hay-pasture or	
3 years corn, 3 years hay pasture	60
Rotation of 2 years corn, 4 years hay pasture	70
Hay-pasture	87
Permanent pasture	93

\* Values from parameters used in Universal Soil Loss Equation.

A crop rotation that includes forages can reduce soil loss by water erosion and, at the same time, slow the buildup of insect and disease problems encountered with a continuous cropping program. On farms where crop rotations are not adequate to control soil erosion, other management factors should be considered.

#### Tillage Practices

Proper tillage practices, employed separately or in combination with crop rotations, can be very effective in reducing soil erosion losses. Compared to conventional fall plowing, a mulch tiller used in the fall can reduce soil loss by up to 40% (Table 4). On sandy soils, planting can be done without any previous tillage or following discing only. Compared to fall plowing, water related soil losses can be reduced by up to 80% by these methods. The objective with any tillage practice is to leave the soil surface in a rough condition, and where practical protected with crop residues. These conditions facilitate easier infiltra-

tion of water by slowing surface water runoff, and minimize soil erosion. Choice of a tillage program depends on many factors which are described in other OMAF factsheets on Tillage.

**Table 4. Reduction in soil losses compared to fall plowing\***

	%
Spring plowing	15
Spring chisel	30
Fall mulch tiller	40
Disk-plant	70
No-till plant	80

\* Values from parameters used in Universal Soil Loss Equation.

#### Contour and Strip Cropping

Tillage and planting of the crop across, rather than with the slope, can reduce soil loss by 25%. (Value from parameters used in Universal Soil Loss Equation.) Strip cropping — alternative hay and grain strips — is an erosion control measure that can be used on long, smooth slopes where forages are part of the rotation. Strip cropping across the slope can reduce soil losses by 50% when compared to up-down slope cropping. Contour strip cropping will reduce soil losses even further. Small grains, with red clover plow-down, should also be highly effective in place of the hay strips on some slopes.

#### Wind Erosion Control

Management practices to control wind erosion are a must on sandy, muck, or peat soils, and should also be considered on clayey or silty soils. The maintenance of good soil structure and residue cover provides good resistance to wind erosion. Where little or no residue is left on the soil surface, (e.g. corn silage), a cover crop of winter rye may be sown to protect the surface of wind susceptible soils until spring. Fencerows and snowfencing also provide good protection. Strip cropping, or even planting crops at right angles to prevailing winds is a method of controlling wind erosion on land susceptible to strong winds.

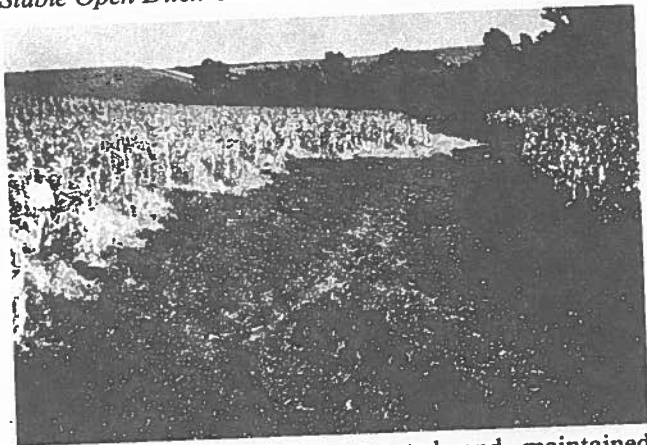
#### Special practices

Tree windbreaks should be planted along the north and west boundaries of fields, and may be planted all around fields where wind erosion is a particular problem. On very steep slopes or areas where blowouts or rills/gullies frequently occur, permanent sod or tree cover should be maintained, and may in fact provide better financial returns.

When surface runoff concentrates, rills develop. If these rills are not addressed with appropriate control practices, a gully may result. Runoff will continue to be a problem on some areas even after conservation tillage and cropping practices are followed. A properly prepared and maintained waterway with good grass cover may be a practical way to prevent this type of water erosion problem. Often, a diversion terrace can be constructed across the slope to divert surface water from affecting soil further down the slope. Diversion terraces can be used as a short-term solution while correcting erosion problems and constructing grassed waterways, or may be permanently grassed to direct water flow to stable outlets. Waterways must have a smoothly contoured channel with a constant grade and a hard-wearing grass sod cover to

carry water safely. Usually, they can be designed to be wide and shallow to facilitate equipment crossing. See OMAF Factsheet *Grassed Waterways*, Agdex 573.

Buffer strips along the banks of drainage ditches and streams should be maintained with grass cover. These buffer strips will help stabilize ditch banks by preventing slumping and wash-outs as well as subsequent siltation. Maintenance costs in cleaning will also be reduced. Ditch or stream banks should have proper side slopes according to recommendations for each soil type. The banks must be smoothly contoured so that a good grass sod can be maintained. See OMAF Factsheet *Considerations for Stable Open Ditch Constructions*, Agdex 751.



**Figure 2.** A properly constructed and maintained grassed waterway

Water and sediment control basins, or channel terraces, can be employed to temporarily pond surface runoff from relatively small upland areas and direct these flows into subsurface tile systems. These types of structures effectively reduce the peak flows of surface runoff and can sometimes reduce the need for elaborate structural measures further downslope.

Tile drainage systems can also prove to be an effective means of reducing surface runoff. They can be designed to complement surface water control measures such as water and sediment control basins, catch basins, blind inlets or terracing. These structures require design by qualified specialists.

Controlling livestock access to ditches and streams with fencing and low level crossings can be a cost effective means of maintaining bank stability, decreasing sedimentation, and reducing water quality problems.

Tile outlet protection is one of the most important practices that can be used in drainage ditches. Proper use of rip rap stone, and rodent guard outlet pipes, will discharge water safely into ditches and streams.

In summary, management for wind and water erosion control involves several alternative practices that are based on maintaining good soil structure, protection of the soil surfaces and the use of special practices. Adherence to these practices will do much to enable farmers to continue to maximize crop yields, minimize soil erosion, and enhance the quality of surface water.